
Design Example Report

| | |
|------------------------|---|
| Title | <i>15.3 W, Isolated Flyback, Dimmable, Power Factor Corrected LED Driver Using LinkSwitchTM-PH LNK406EG</i> |
| Specification | 185 VAC – 265 VAC Input 36 V, 425 mA Output |
| Application | LED Driver for PAR30 / PAR38 |
| Author | Application Engineering Department |
| Document Number | DER-314 |
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| Revision | 1.1 |

Summary and Features

- High efficiency, $\geq 87\%$ at 230 VAC
- Low cost
 - Single-stage converter
 - Single sided PCB
 - Low component count
- Enhanced user experience
 - Flicker free, fast monotonic start-up (<300 ms) – no perceptible delay
 - Broad dimmer compatibility
 - Flicker-free
 - Tested with common types from Australia, China, Korea and Germany
- Integrated protection and reliability features
 - Output open circuit / output short-circuit protected with auto-recovery
 - Line input overvoltage shutdown extends voltage withstand during line faults
 - Auto-recovering thermal shutdown with large hysteresis protects both components and printed circuit board
- IEC 61000-4-5 ring wave, IEC 61000-3-2 C and EN55015 B conducted EMI compliant

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PATENT INFORMATION

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Important Note: Although this board is designed to satisfy safety isolation requirements, the engineering prototype has not been agency approved. Therefore, all testing should be performed using an isolation transformer to provide the AC input to the prototype board.



1 Introduction

The document describes an isolated high power factor (PF) TRIAC dimmable LED driver designed to drive a nominal LED string voltage of 36 V at 425 mA from an input voltage range of 185 VAC to 265 VAC. The LED driver utilizes the LNK406EG from the LinkSwitch-PH family of ICs.

Key goals for this design were:

- Lowest cost
- Small size
- Efficiency
- Demonstration of (optional) thermal fold back (output current reduces above temperature threshold)

The topology used is a single-stage power factor corrected flyback, that delivers high efficiency, high power factor, low THD, isolation, low component count, and meets the stringent space limits for this design.

High power factor and low THD is achieved by employing the LinkSwitch-PH IC which also provides a sophisticated range of protection features including auto-restart for open control loop and output short-circuit conditions. Line overvoltage provides extended line fault and surge withstand, and accurate hysteretic thermal shutdown that ensures safe average PCB temperatures under all conditions.

This document contains the LED driver specification, schematic, PCB diagram, bill of materials, transformer documentation and typical performance characteristics.

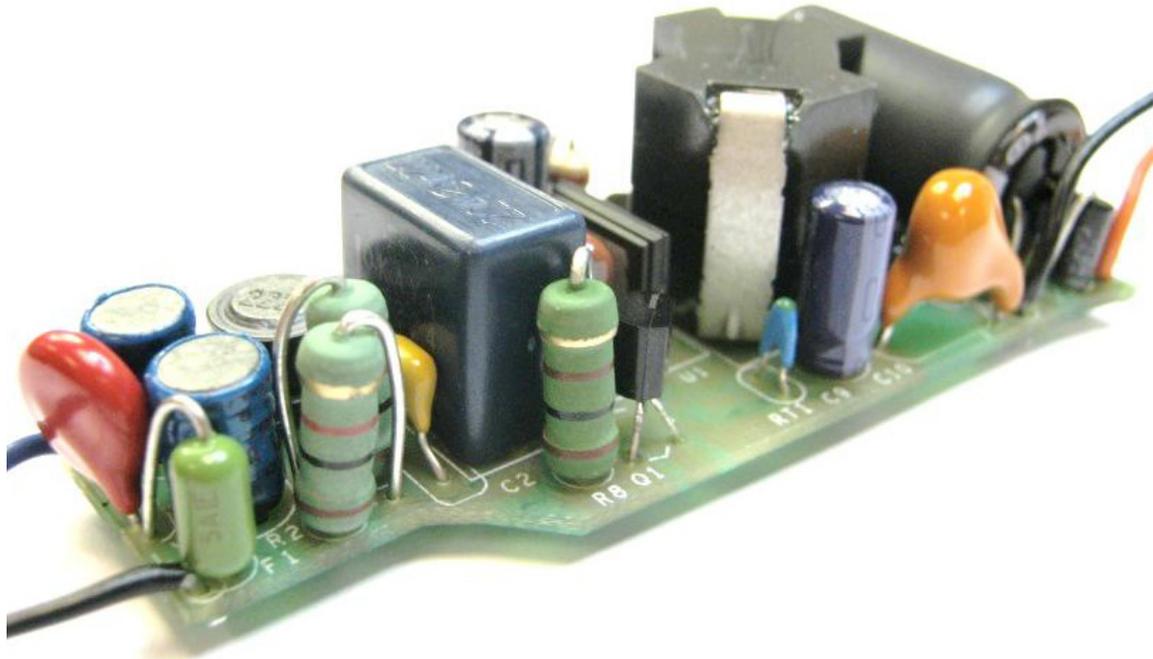


Figure 1 – Populated Circuit Board Photograph.





Figure 2 – Populated Circuit Board Photograph (Top View).



Figure 3 – Populated Circuit Board Photograph (Bottom View).



2 Power Supply Specification

The table below represents the minimum acceptable performance of the design. Actual performance is listed in the results section.

| Description | Symbol | Min | Typ | Max | Units | Comment |
|---|-------------------------------------|-----|--------------------------|-----|------------------|--|
| Input Voltage Frequency | V_{IN} f_{LINE} | 185 | 230 50 | 265 | VAC Hz | 2 Wire – no P.E. |
| Output Output Voltage Output Current Total Output Power Continuous Output Power | V_{OUT} I_{OUT} P_{OUT} | | 36 425 15.3 | | V mA W | $V_{OUT} = 36, V_{IN} = 230 \text{ VAC}, 25^\circ\text{C}$ |
| Efficiency Full Load | η | 86 | | | % | Measured at $P_{OUT} 25^\circ\text{C}$ |
| Environmental Conducted EMI Safety Ring Wave (100 kHz) Differential Mode (L1-L2) Common mode (L1/L2-PE) Differential Surge (1.2/50 μs) | | | | | | CISPR 15B / EN55015B Isolated 2.5 kV 500 V |
| Power Factor | | | 0.9 | | | Measured at $V_{OUT(TYP)}, I_{OUT(TYP)}$ and 230 VAC, 50 Hz |
| Harmonic Currents | | | EN 61000-3-2 Class D (C) | | | Class C specifies Class D Limits when $P_{IN} < 25 \text{ W}$ |
| Ambient Temperature | T_{AMB} | | 50 | | $^\circ\text{C}$ | Free convection, sea level |



3 Schematic

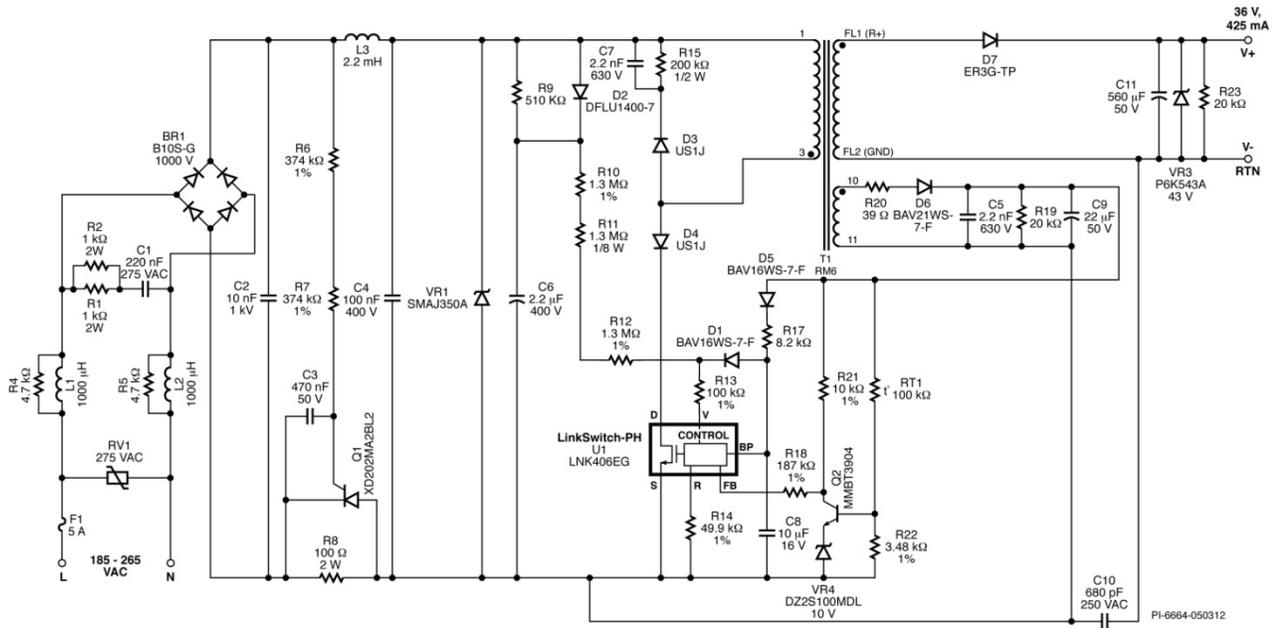


Figure 4 – Schematic.

The following components were not populated

- 500 V to 1 kV differential surge withstand: VR1



4 Circuit Description

The LinkSwitch-PH device is a controller with an integrated 725 V power MOSFET for use in LED driver applications. The LinkSwitch-PH is configured for use in a single-stage flyback topology which provides a primary side regulated constant current output while maintaining high power factor from the AC input.

4.1 Input Filtering

Fuse F1 provides protection from component failure. A relatively high current rating was selected to prevent failure during 1 kV differential (1.2 μ s /50 μ s) line surge. If 500 V withstand is sufficient, a lower rated device may be substituted. Varistor RV1 provides a clamp to limit the maximum voltage during differential line surges. A 275 VAC rated part was selected, being slightly above the maximum specified operating voltage of 265 VAC. Diode bridge BR1 rectifies the AC line voltage with capacitor C4 providing a low impedance path (decoupling) for the primary switching current. Capacitor C2 and differential choke L3 are used for additional differential filtering of noise associated with SCR Q1 switching. A low value of capacitance (sum of C4 and C2) is necessary to maintain a power factor of greater than 0.9.

EMI filtering is provided by inductors L1, L2, and L3, and capacitors C4, C2, and C10. Resistor R4 and R5 across L1 and L2 damp any LC resonances due to the filter components and the AC line impedance which would otherwise cause increased conducted EMI measurements.

4.2 LinkSwitch-PH Primary

One side of the transformer (T1) is connected to the DC bus and the other to the DRAIN (D) pin of the LinkSwitch-PH via blocking diode D4. During the on-time of the power MOSFET, current ramps through the primary, storing energy which is then delivered to the output during the power MOSFET off-time. An RM8 core size was selected to meet the power processing and size requirements of the design. One advantage of the low component count is the ability to use larger core sizes for increased efficiency whilst still meeting the size constraint.

To provide peak line voltage information to U1 the incoming rectified AC peak charges C6 via D2. This is then fed into the VOLTAGE MONITOR (V) pin of U1 as a current via R10, R11, R12 and R13. Resistor R9 provides a discharge path for C6 with a time constant much longer than that of the rectified AC to prevent the V pin current being modulated at the line frequency (which would degrade power factor).

To extend the dimming range R13 disables the line brown-out function of the V pin by supplying a current $>I_{UV}$ into the V pin. The current is determined by the BYPASS (BP) pin, V pin voltages and the value of R13 and is $\sim 30 \mu$ A for this design.

The line overvoltage shutdown function extends the rectified line voltage withstand (during surges and line swells) to the 725 BV_{DSS} rating of the internal power MOSFET.



The V pin current and the FEEDBACK (FB) pin current are used internally to control the average output LED current. For phase angle dimming applications a 49.9 k Ω resistor is used on the REFERENCE (R) pin (R14) and 4 M Ω (R10+R11+R12+R13) on the V pin to provide a linear relationship between input voltage and the output current. This maximizes the dimming range when used with TRIAC dimmers. The value of R14 is used to select between two values of internal line input brown-in and brown-out thresholds.

During the power MOSFET off-time, D3, R15, and C7 clamp the drain voltage to a safe level due to the effects of leakage inductance. Diode D4 is necessary to prevent reverse current from flowing through U1 while the voltage across C5 (rectified input AC) falls to below the reflected output voltage (parameter V_{OR} in the design spreadsheet).

Diode D6, C9, and R20 generate a primary bias supply from an auxiliary winding on the transformer. Capacitor C5 is used to minimize the loop on the bias winding circuit for reduced EMI. Resistor R20 provides filtering so that the bias voltage tracks the output voltage closely (to maintain constant output current with changes in LED voltage). Capacitor C8 provides local decoupling for the BP pin of U1 which is the supply pin for the internal controller. During start-up, C8 is charged to ~6 V from an internal high-voltage current source connected to the D pin. Once charged U1 starts switching at which point the operating supply current is provided from the bias supply via R17.

The use of an external bias supply (via D5 and R17) is recommended to give the lowest device dissipation and highest efficiency however these components may be omitted if desired. The ability to be self-powered provides improved phase angle dimming performance as the IC is able to maintain operation even when the input conduction phase angle is very small (the equivalent to a low AC input voltage).

Capacitor C8 also selects the output power mode, 10 μ F was selected (reduced power mode) to minimize the device dissipation and minimize heat sinking requirements.

4.3 Feedback

The bias winding voltage is used to sense the output voltage indirectly, eliminating secondary side feedback components. The voltage on the bias winding is proportional to the output voltage (set by the turn ratio between the bias and secondary windings). Resistors R18 and R21 converts the bias voltage into a current which is fed into the FB pin of U1. The internal engine within U1 combines the FB pin current, the V pin current, and internal drain current information to provide a constant output current whilst maintaining high input power factor.

4.4 Temperature Fold Back Circuit

The board also caters for an optional temperature compensation circuit that can enable LinkSwitch-PH to operate with temperature compensation to increase the maximum operating ambient temperature of a given LED driver by reducing the output power linearly as the driver temperature increases.



Zener diode VR4 and the voltage across the node of resistor R22 and thermistor (NTC) RT1 dictate the start of temperature fold back. As the monitored temperature rises, so does the base voltage of Q2. Once this exceeds the voltage of VR4 plus a V_{BE} drop, Q2 is biased on. Further increases in temperature will start diverting current from the FB pin, which will cause a reduction in output current / power.

Resistor R22 can be adjusted to vary the temperature trip point at which output power reduction starts desired.

The circuit is ideal for applications in extending the operating ambient temperature of a given LinkSwitch-PH LED driver, or protecting the LED array from excess temperature when installed incorrectly by the end user.

4.5 Output Rectification

The transformer secondary winding is rectified by D7 and filtered by C11. Capacitor C11 was selected to give an LED ripple current equal to $\sim\pm 30\%$ of the mean value. For designs where higher ripple is acceptable, the output capacitance value can be reduced (and for lower ripple increased).

4.6 Disconnected Load Protection

In case of open (disconnected) load fault, Zener diode VR3 will fail short circuit and the unit will enter auto-restart condition. This is a non-recovering protection scheme, for self-recovering protection the bias voltage rise can be sensed via a Zener diode connected from C9 to the base of Q2. The value would be selected to be above the maximum bias voltage when driving the maximum LED load voltage. For this design 39 V or 43 V would be a suitable starting value.

4.7 TRIAC Phase Dimming Control Compatibility

The requirement to provide output dimming with low cost, TRIAC based, leading edge phase dimmers introduced a number of tradeoffs in the design.

Due to the much lower power consumed by LED based lighting the current drawn by the lamp can fall below the holding current of the TRIAC within the dimmer. This causes undesirable behavior such as the lamp turning off before the end of the dimmer control range and/or flickering as the TRIAC fires inconsistently. The relatively large impedance the LED lamp presents to the line allows significant ringing to occur due to the inrush current charging the input capacitance when the TRIAC turns on. This too can cause similar undesirable behavior as the ringing may cause the TRIAC current to fall to zero.

To overcome these issues, active damper and passive bleeder circuits were added. The drawback of these circuits is increased dissipation and therefore reduced efficiency of the supply. For non-dimming applications these components can simply be omitted.



The Active Damper consists of components R6, R7, Q1, C3 and R8. This circuit limits the inrush current that flows to charge C4 when the TRIAC turns on by placing R8 in series for the first 1 ms of the conduction period. After approximately 1 ms, Q1 turns on and shorts R8. This keeps the power dissipation on R8 low and allows a larger value to be used for more effective during current limiting. Resistor R6, R7 and C3 provide the 1 ms delay after the TRIAC conducts. The SCR selected for Q1 is a low current, low cost device in a TO-92 package.

The passive bleeder circuit is comprised of C1 and parallel combination of R1, and R2. This keeps the input current above the TRIAC holding current while the driver input current increases during each AC half-cycle preventing the TRIAC switch from oscillating at the start (and end) of each conduction angle period.

This arrangement provided flicker-free dimming operation with phase angle dimmers from Australia, Europe, China, Korea, both leading-edge and lagging-edge types.



5 PCB Layout

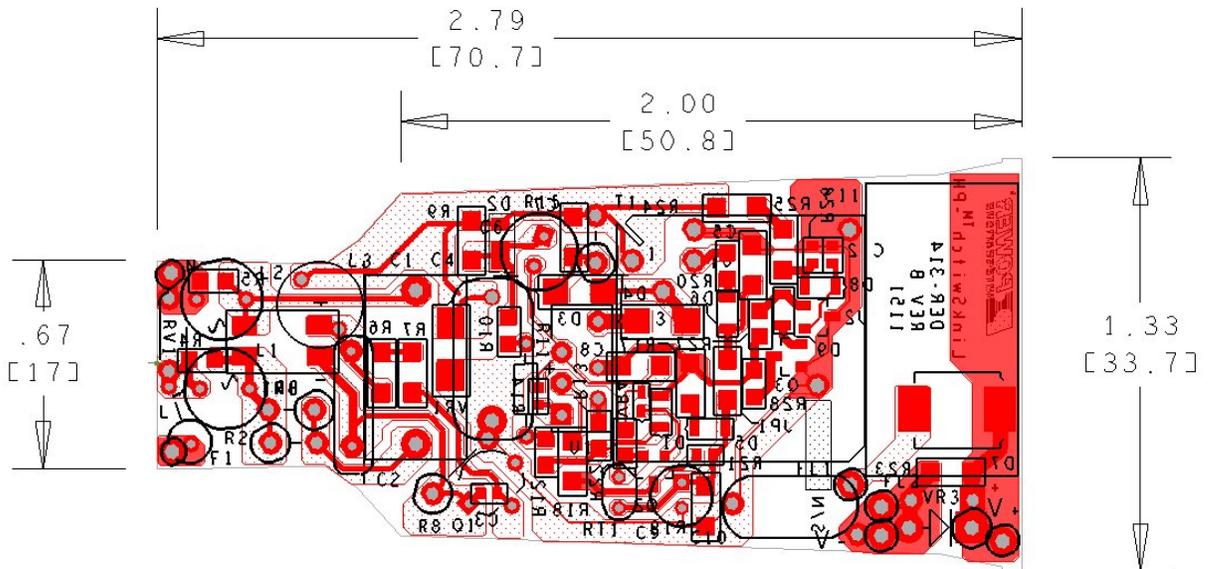


Figure 5 – PCB Layout and Outline.

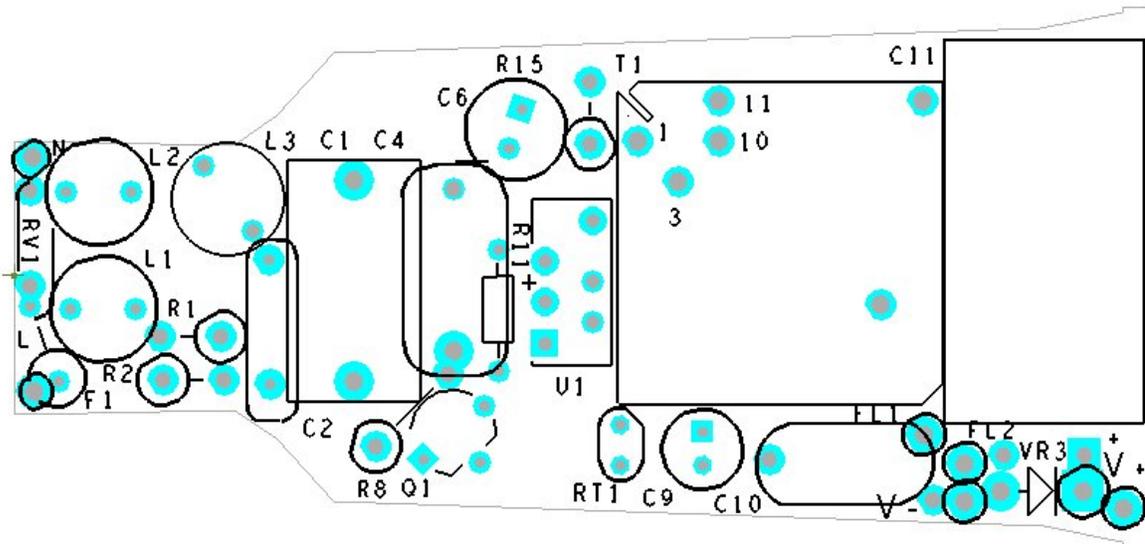


Figure 6 – Top Side.



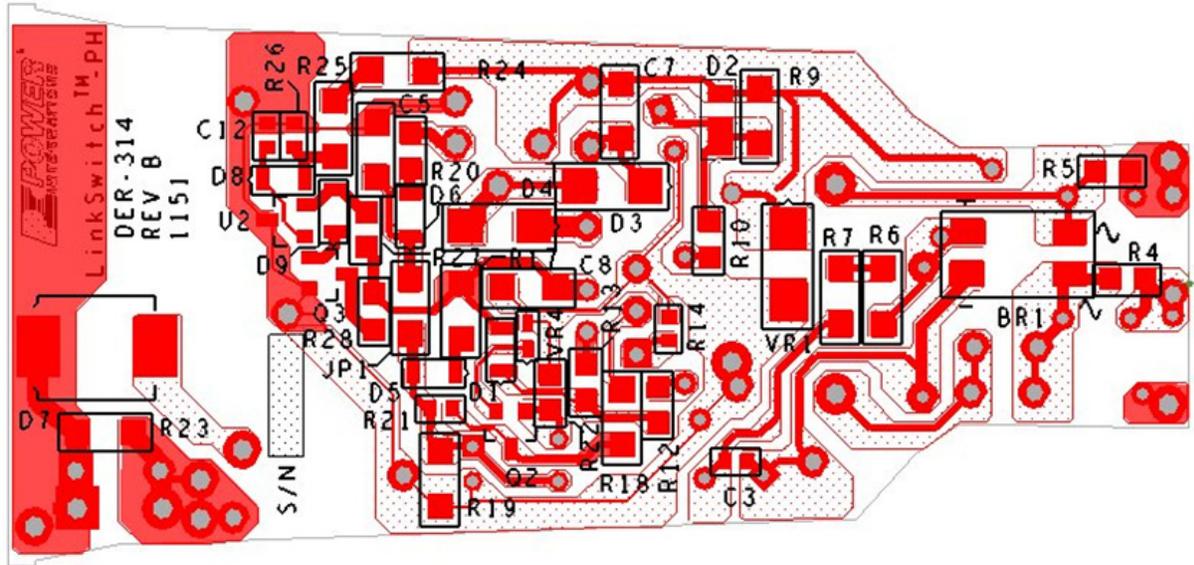


Figure 7 – Bottom Side.



6 Bill of Materials

| Item | Qty | Ref Des | Description | Mfg Part Number | Mfg |
|------|-----|---------|--|--------------------|--------------------|
| 1 | 1 | BR1 | 1000 V, 0.8 A, Bridge Rectifier, MBS-1, 4-SOIC | B10S-G | Comchip |
| 2 | 1 | C1 | 220 nF, 275 VAC, Film, X2 | LE224-M | OKAYA ELECT |
| 3 | 1 | C2 | 10 nF, 1 kV, Disc Ceramic, X7R | SV01AC103KAR | AVX |
| 4 | 1 | C3 | 470 nF, 50 V, Ceramic, Y5G, 0603 | C1608Y5V1H474Z | TDK |
| 5 | 1 | C4 | 100 nF, 400 V, Film | ECQ-E4104KF | Panasonic |
| 6 | 2 | C5 C7 | 2.2 nF, 630 V, Ceramic, X7R, 1206 | ECJ-3FBJ222K | Panasonic |
| 7 | 1 | C6 | 2.2 μ F, 400 V, Electrolytic, (6.3 x 11) | TAB2GM2R2E110 | Ltec |
| 8 | 1 | C8 | 10 μ F, 16 V, Ceramic, X7R, 1206 | C3216X7R1C106M | TDK |
| 9 | 1 | C9 | 22 μ F, 50 V, Electrolytic, (5 x 11.5) | ELXZ500ELL220MEB5D | Nippon Chemi-Con |
| 10 | 1 | C10 | 680 pF, Ceramic, Y1 | 440LT68-R | Vishay |
| 11 | 1 | C11 | 560 μ F, 50 V, Electrolytic, (12.5 x 25) | UPW1H561MHD | Nichicon |
| 12 | 2 | D1 D5 | 75 V, 0.15 A, Switching, SOD-323 | BAV16WS-7-F | Diodes, Inc. |
| 13 | 1 | D2 | 400 V, 1 A, Diode Sup Fast 1 A PWRDI 123 | DFLU1400-7 | Diodes, Inc. |
| 14 | 2 | D3 D4 | Diode Ultrafast, SW 600 V, 1 A, SMA | US1J-13-F | Diodes, Inc. |
| 15 | 1 | D6 | 250 V, 0.2 A, Fast Switching, 50 ns, SOD-323 | BAV21WS-7-F | Diodes, Inc. |
| 16 | 1 | D7 | 400 V, 3 A, SMC, DO-214AB | ER3G-TP | Micro Commercial |
| 17 | 1 | F1 | 5 A, 250 V, Fast, Microfuse, Axial | 0263005.MXL | Littlefuse |
| 18 | 1 | JP1 | 0 R, 5%, 1/4 W, Thick Film, 1206 | ERJ-8GEY0R00V | Panasonic |
| 19 | 2 | L1 L2 | 1000 μ H, 0.18 A, 7 x 10.5 mm | SBC2-102-181 | Tokin |
| 20 | 1 | L3 | 2.2 mH, 0.16 A, Ferrite Core | CTSCH875DF-222K | CT Parts |
| 21 | 1 | Q1 | SCR, 600 V, 1.25 A, TO-92 | X0202MA 2BL2 | ST Micro |
| 22 | 1 | Q2 | NPN, Small Signal BJT, 40 V, 0.2 A, SOT-23 | MMBT3904LT1G | On Semi |
| 23 | 2 | R1 R2 | 1.0 k Ω , 5%, 2 W, Metal Oxide | RSMF2JT1K00 | Stackpole |
| 24 | 2 | R4 R5 | 4.7 k Ω , 5%, 1/8 W, Thick Film, 0805 | ERJ-6GEYJ472V | Panasonic |
| 25 | 2 | R6 R7 | 374 k Ω , 1%, 1/4 W, Thick Film, 1206 | ERJ-8ENF3743V | Panasonic |
| 26 | 1 | R8 | 100 Ω , 5%, 2 W, Metal Oxide | RSMF2JT100R | Stackpole |
| 27 | 1 | R9 | 510 k Ω , 5%, 1/4 W, Thick Film, 1206 | ERJ-8GEYJ514V | Panasonic |
| 28 | 2 | R10 R12 | 1.3 M Ω , 1%, 1/8 W, Thick Film, 0805 | ERJ-6ENF1304V | Panasonic |
| 29 | 1 | R11 | 1.3 M Ω , 5%, 1/8 W, Carbon Film | CFR-12JB-1M3 | Yageo |
| 30 | 1 | R13 | 100 k Ω , 1%, 1/8 W, Thick Film, 0805 | ERJ-6ENF1003V | Panasonic |
| 31 | 1 | R14 | 49.9 k Ω , 1%, 1/16 W, Thick Film, 0603 | ERJ-3EKF4992V | Panasonic |
| 32 | 1 | R15 | 200 k Ω , 5%, 1/2 W, Carbon Film | CFR-50JB-200K | Yageo |
| 33 | 1 | R17 | 8.2 k Ω , 5%, 1/4 W, Thick Film, 1206 | ERJ-8GEYJ822V | Panasonic |
| 34 | 1 | R18 | 187 k Ω , 1%, 1/4 W, Thick Film, 1206 | ERJ-8ENF1873V | Panasonic |
| 35 | 2 | R19 R23 | 20 k Ω , 5%, 1/4 W, Thick Film, 1206 | ERJ-8GEYJ203V | Panasonic |
| 36 | 1 | R20 | 39 Ω , 5%, 1/8 W, Thick Film, 0805 | ERJ-6GEYJ390V | Panasonic |
| 37 | 1 | R21 | 10 k Ω , 1%, 1/16 W, Thick Film, 0603 | ERJ-3EKF1002V | Panasonic |
| 38 | 1 | R22 | 3.48 k Ω , 1%, 1/8 W, Thick Film, 0805 | ERJ-6ENF3481V | Panasonic |
| 39 | 1 | RT1 | NTC Thermistor, 100 k Ω , 0.00014 A | NTSA0WF104EE1B0 | Murata |
| 40 | 1 | RV1 | 275 V, 23 J, 7 mm, RADIAL | V275LA4P | Littlefuse |
| 41 | 1 | T1 | Bobbin, RM8, Vertical, 12 pins | RM8/12/1 | Schwartzpunkt |
| 42 | 1 | U1 | LinkSwitch-PH, eSIP | LNK406EG | Power Integrations |
| 43 | 1 | VR1 | 350 V, 400 W, 5%, DO214AC (SMA) | SMAJ350A | Littlefuse |
| 44 | 1 | VR3 | 43 V, 5 W, 5%, DO204AC (DO-15) | P6KE43AG | On Semi |
| 45 | 1 | VR4 | 10 V, 5%, 150 mW, SSMINI-2 | DZ2S100M0L | Panasonic |



7 Transformer Specification

7.1 Electrical Diagram

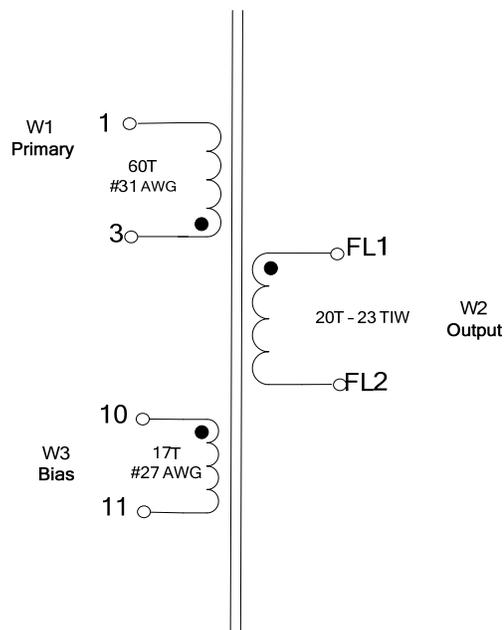


Figure 8 – Transformer Electrical Diagram.

7.2 Electrical Specifications

| | | |
|-----------------------------------|--|----------------|
| Electrical Strength | 1 second, 60 Hz, from pins 1, 10, 3, 11 to FL1, FL2 | 3000 VAC |
| Primary Inductance | Pins 1-3, all other windings open, measured at 100 kHz, 0.4 V _{RMS} | 1.15 mH ±2% |
| Resonant Frequency | Pins 1-3, all other windings open | 750 kHz (Min.) |
| Primary Leakage Inductance | Pins 1-3, with FL1-FL2 shorted, measured at 100 kHz, 0.4 V _{RMS} | 20 μH ±7% |

7.3 Materials

| Item | Description |
|------|--|
| [1] | Core: RM8/I, 3F3. |
| [2] | Bobbin, 12 pin vertical, CSV-RM8-1S-12P from Philips or equivalent With mounting clip, CLI/P-RM8. |
| [3] | Tape, Polyester film, 3M 1350F-1 or equivalent, 9 mm wide. |
| [4] | Wire: Magnet, 31 AWG, solderable double coated. |
| [5] | Wire: Magnet, 27 AWG, solderable double coated. |
| [6] | Wire: Triple Insulated, Furukawa TEX-E or Equivalent, 23 TIW. |
| [7] | Transformer Varnish, Dolph BC-359 or equivalent. |



7.4 Transformer Build Diagram

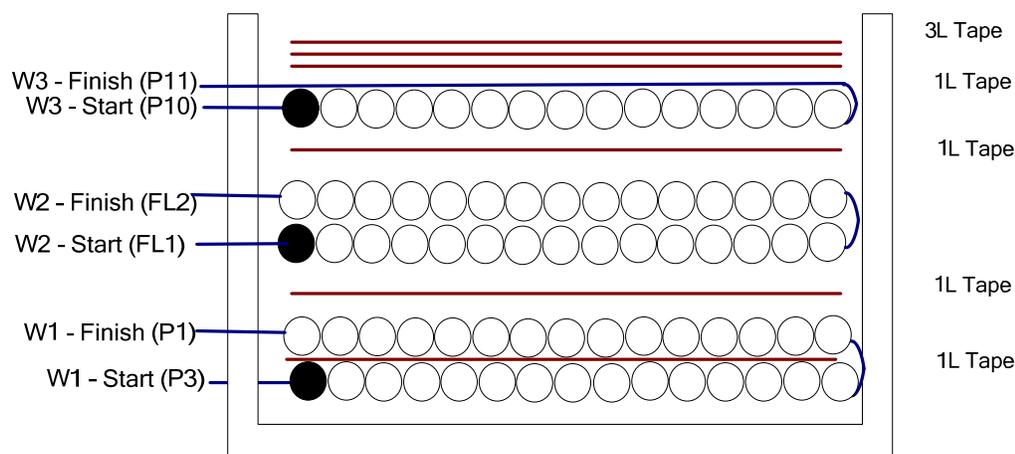


Figure 9 – Transformer Build Diagram.

7.5 Transformer Construction

| | |
|---------------------------|---|
| Bobbin Preparation | Place the bobbin item [2] on the mandrel such that pin side on the left side. Winding direction is the clockwise direction. |
| WDG 1 (Primary) | Starting at pin 3, wind 60 turns of wire item [4] in two layers. Apply one layer of tape item [3] between 1 st and 2 nd layer. Finish at pin 1. |
| Insulation | Apply one layer of tape item [3]. |
| WDG 2 (Secondary) | Leave about 1" of wire item [6], use small tape to mark as FL1, enter into slot of secondary side of bobbin, wind 20 turns in two layers. At the last turn exit the same slot, leave about 1", and mark as FL2. |
| Insulation | Apply one layer of tape item [3]. |
| WDG 3 (Bias) | Starting at pin 10, wind 17 turns of wire item [5], spreading the wire, and finish at pin 11. |
| Finish Wrap | Apply three layers of tape item [3] for finish wrap. |
| Final Assembly | Cut FL1 and FL2 to 0.75". Grind core to get 1.15 mH inductance. Assemble and secure core halves. Dip impregnate using varnish item [7]. |



8 Transformer Design Spreadsheet

| ACDC_LinkSwitch-PH_032511; Rev.1.3; Copyright Power Integrations 2011 | INPUT | INFO | OUTPUT | UNIT | LinkSwitch-PH_032511: Flyback Transformer Design Spreadsheet |
|---|--------|-------------|-----------|-----------|---|
| ENTER APPLICATION VARIABLES | | | | | |
| Dimming required | YES | <i>Info</i> | YES | | !!! Info. When configured for dimming, best output current line regulation is achieved over a single input voltage range. |
| VACMIN | 185 | | 185 | V | Minimum AC Input Voltage |
| VACMAX | 265 | | 265 | V | Maximum AC input voltage |
| fL | | | 50 | Hz | AC Mains Frequency |
| VO | 36.00 | | | V | Typical output voltage of LED string at full load |
| VO_MAX | | | 39.60 | V | Maximum expected LED string Voltage. |
| VO_MIN | | | 32.40 | V | Minimum expected LED string Voltage. |
| V_OVP | | | 43.56 | V | Over-voltage protection setpoint |
| IO | 0.43 | | | A | Typical full load LED current |
| PO | | | 15.5 | W | Output Power |
| n | 0.87 | | 0.87 | | Estimated efficiency of operation |
| VB | 30 | | 30 | V | Bias Voltage |
| ENTER LinkSwitch-PH VARIABLES | | | | | |
| LinkSwitch-PH | LNK406 | | | Universal | 115 Doubled/230V |
| Chosen Device | | LNK406 | Power Out | 10W | 4.5W |
| Current Limit Mode | RED | | RED | | Select "RED" for reduced Current Limit mode or "FULL" for Full current limit mode |
| ILIMITMIN | | | 1.19 | A | Minimum current limit |
| ILIMITMAX | | | 1.38 | A | Maximum current limit |
| fS | | | 66000 | Hz | Switching Frequency |
| fSmin | | | 62000 | Hz | Minimum Switching Frequency |
| fSmax | | | 70000 | Hz | Maximum Switching Frequency |
| IV | | | 80.6 | uA | V pin current |
| RV | | | 4 | M-ohms | Upper V pin resistor |
| RV2 | | | 1E+012 | M-ohms | Lower V pin resistor |
| IFB | 169.84 | | 169.8 | uA | FB pin current (85 uA < IFB < 210 uA) |
| RFB1 | | | 159.0 | k-ohms | FB pin resistor |
| VDS | | | 10 | V | LinkSwitch-PH on-state Drain to Source Voltage |
| VD | 0.50 | | | V | Output Winding Diode Forward Voltage Drop (0.5 V for Schottky and 0.8 V for PN diode) |
| VDB | 0.70 | | | V | Bias Winding Diode Forward Voltage Drop |
| Key Design Parameters | | | | | |
| KP | 1.24 | | 1.24 | | Ripple to Peak Current Ratio (For PF > 0.9, 0.4 < KP < 0.9) |
| LP | | | 1159 | uH | Primary Inductance |
| VOR | 109.50 | | 109.5 | V | Reflected Output Voltage. |
| Expected IO (average) | | | 0.42 | A | Expected Average Output Current |
| KP_VACMAX | | <i>Info</i> | 1.28 | | !!! Info. PF at high line may be less than 0.9. Decrease KP for higher PF |
| TON_MIN | | | 1.97 | us | Minimum on time at maximum AC input voltage |



| | | | | | |
|---|--------------|---|--------------|-------------------|---|
| PCLAMP | | | 0.13 | W | Estimated dissipation in primary clamp |
| ENTER TRANSFORMER CORE/CONSTRUCTION VARIABLES | | | | | |
| Core Type | RM8/I | | RM8/I | | |
| Bobbin | | <i>RM8/I_</i> <i>BOBBI</i> <i>N</i> | | <i>P/N:</i> | * |
| AE | | | 0.63 | cm ² | Core Effective Cross Sectional Area |
| LE | | | 3.84 | cm | Core Effective Path Length |
| AL | | | 3000 | nH/T ² | Ungapped Core Effective Inductance |
| BW | | | 8.6 | mm | Bobbin Physical Winding Width |
| M | | | 0 | mm | Safety Margin Width (Half the Primary to Secondary Creepage Distance) |
| L | 2.00 | | 2 | | Number of Primary Layers |
| NS | 20 | | 20 | | Number of Secondary Turns |
| DC INPUT VOLTAGE PARAMETERS | | | | | |
| VMIN | | | 262 | V | Peak input voltage at VACMIN |
| VMAX | | | 375 | V | Peak input voltage at VACMAX |
| CURRENT WAVEFORM SHAPE PARAMETERS | | | | | |
| DMAX | | | 0.26 | | Minimum duty cycle at peak of VACMIN |
| IAVG | | | 0.11 | A | Average Primary Current |
| IP | | | 0.95 | A | Peak Primary Current (calculated at minimum input voltage VACMIN) |
| IRMS | | | 0.24 | A | Primary RMS Current (calculated at minimum input voltage VACMIN) |
| TRANSFORMER PRIMARY DESIGN PARAMETERS | | | | | |
| LP | | | 1159 | uH | Primary Inductance |
| NP | | | 60 | | Primary Winding Number of Turns |
| NB | | | 17 | | Bias Winding Number of Turns |
| ALG | | | 322 | nH/T ² | Gapped Core Effective Inductance |
| BM | | | 2906 | Gauss | Maximum Flux Density at PO, VMIN (BM<3100) |
| BP | | | 3516 | Gauss | Peak Flux Density (BP<3700) |
| BAC | | | 1453 | Gauss | AC Flux Density for Core Loss Curves (0.5 X Peak to Peak) |
| ur | | | 1455 | | Relative Permeability of Ungapped Core |
| LG | | | 0.22 | mm | Gap Length (Lg > 0.1 mm) |
| BWE | | | 17.2 | mm | Effective Bobbin Width |
| OD | | | 0.29 | mm | Maximum Primary Wire Diameter including insulation |
| INS | | | 0.05 | mm | Estimated Total Insulation Thickness (= 2 * film thickness) |
| DIA | | | 0.24 | mm | Bare conductor diameter |
| AWG | | | 31 | AWG | Primary Wire Gauge (Rounded to next smaller standard AWG value) |
| CM | | | 81 | Cmils | Bare conductor effective area in circular mils |
| CMA | | | 341 | Cmils/Amp | Primary Winding Current Capacity (200 < CMA < 600) |
| LP_TOL | 10 | | 10 | | Tolerance of primary inductance |
| TRANSFORMER SECONDARY DESIGN PARAMETERS (SINGLE OUTPUT EQUIVALENT) | | | | | |
| Lumped parameters | | | | | |



| | | | | | |
|---|--|--|----------|--------|---|
| ISP | | | 2.84 | A | Peak Secondary Current |
| ISRMS | | | 1.05 | A | Secondary RMS Current |
| IRIPPLE | | | 0.96 | A | Output Capacitor RMS Ripple Current |
| CMS | | | 211 | Cmils | Secondary Bare Conductor minimum circular mils |
| AWGS | | | 26 | AWG | Secondary Wire Gauge (Rounded up to next larger standard AWG value) |
| DIAS | | | 0.41 | mm | Secondary Minimum Bare Conductor Diameter |
| ODS | | | 0.43 | mm | Secondary Maximum Outside Diameter for Triple Insulated Wire |
| VOLTAGE STRESS PARAMETERS | | | | | |
| VDRAIN | | | 599 | V | Estimated Maximum Drain Voltage assuming maximum LED string voltage (Includes Effect of Leakage Inductance) |
| PIVS | | | 168 | V | Output Rectifier Maximum Peak Inverse Voltage (calculated at VOVP, excludes leakage inductance spike) |
| PIVB | | | 141 | V | Bias Rectifier Maximum Peak Inverse Voltage (calculated at VOVP, excludes leakage inductance spike) |
| FINE TUNING (Enter measured values from prototype) | | | | | |
| V pin Resistor Fine Tuning | | | | | |
| RV1 | | | 4.00 | M-ohms | Upper V Pin Resistor Value |
| RV2 | | | 1.00E+12 | M-ohms | Lower V Pin Resistor Value |
| VAC1 | | | 115.0 | V | Test Input Voltage Condition1 |
| VAC2 | | | 230.0 | V | Test Input Voltage Condition2 |
| IO_VAC1 | | | 0.43 | A | Measured Output Current at VAC1 |
| IO_VAC2 | | | 0.43 | A | Measured Output Current at VAC2 |
| RV1 (new) | | | 4.00 | M-ohms | New RV1 |
| RV2 (new) | | | 20911.63 | M-ohms | New RV2 |
| V_OV | | | 319.6 | V | Typical AC input voltage at which OV shutdown will be triggered |
| V_UV | | | 66.3 | V | Typical AC input voltage beyond which power supply can startup |
| FB pin resistor Fine Tuning | | | | | |
| RFB1 | | | 159 | k-ohms | Upper FB Pin Resistor Value |
| RFB2 | | | 1E+012 | k-ohms | Lower FB Pin Resistor Value |
| VB1 | | | 27.0 | V | Test Bias Voltage Condition1 |
| VB2 | | | 33.0 | V | Test Bias Voltage Condition2 |
| IO1 | | | 0.43 | A | Measured Output Current at Vb1 |
| IO2 | | | 0.43 | A | Measured Output Current at Vb2 |
| RFB1 (new) | | | 159.0 | k-ohms | New RFB1 |
| RFB2(new) | | | 1.00E+12 | k-ohms | New RFB2 |



9 Performance Data

All measurements performed at room temperature using an LED load. The following data were measured using 3 sets of loads to represent a voltage of 35 V ~ 37 V. The table in Section 9.6 shows complete test data values.

9.1 Efficiency

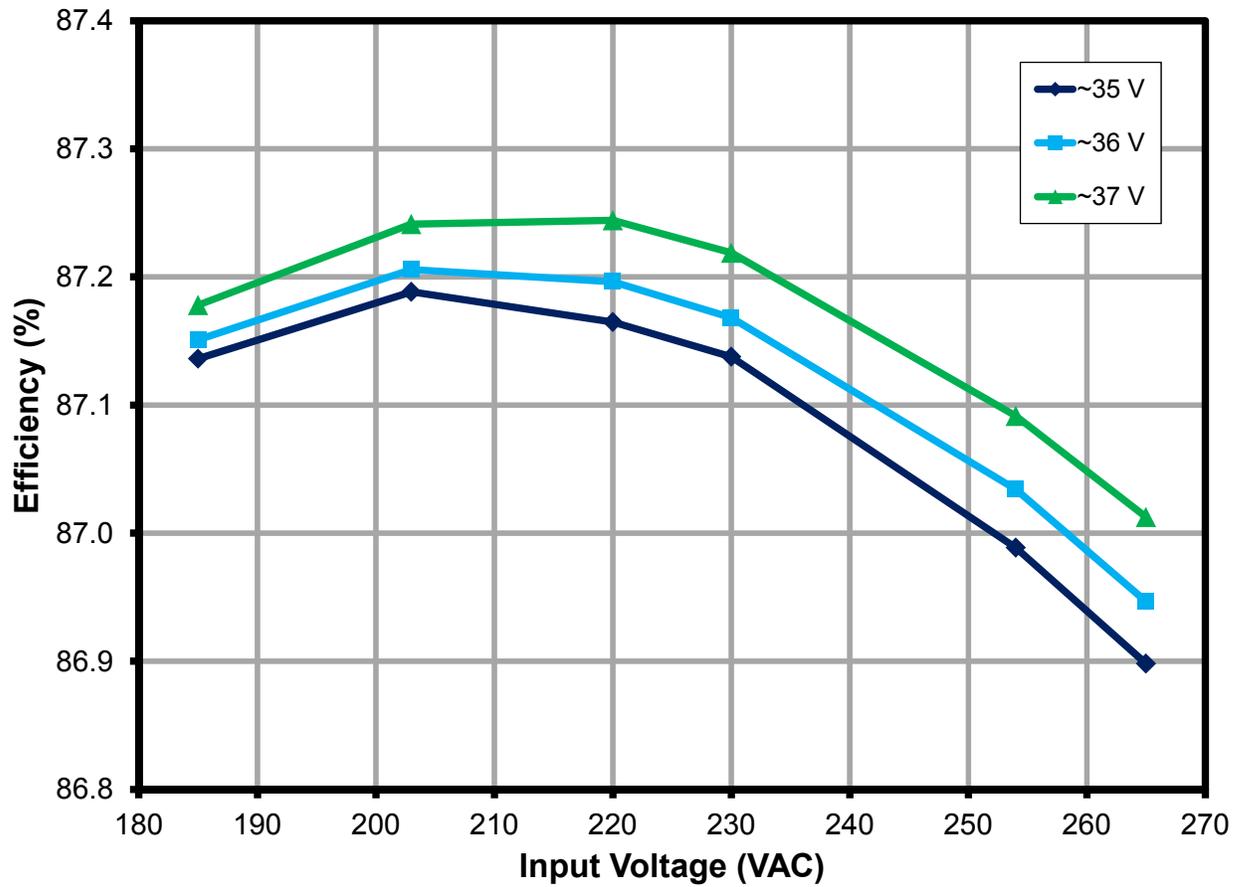


Figure 10 – Efficiency vs. Line and Load.



9.2 Line and Load Regulation

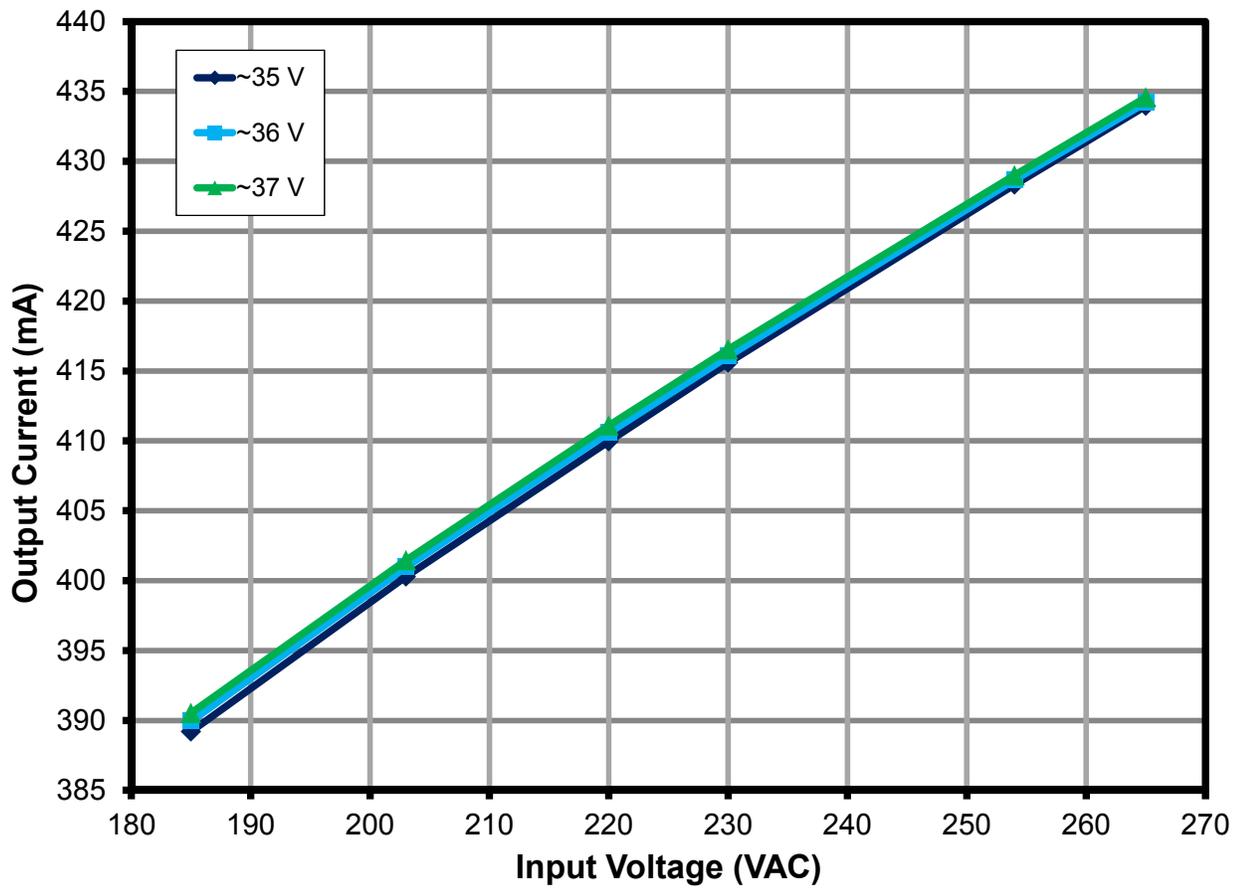


Figure 11 – Regulation vs. Line and Load.



9.3 Power Factor

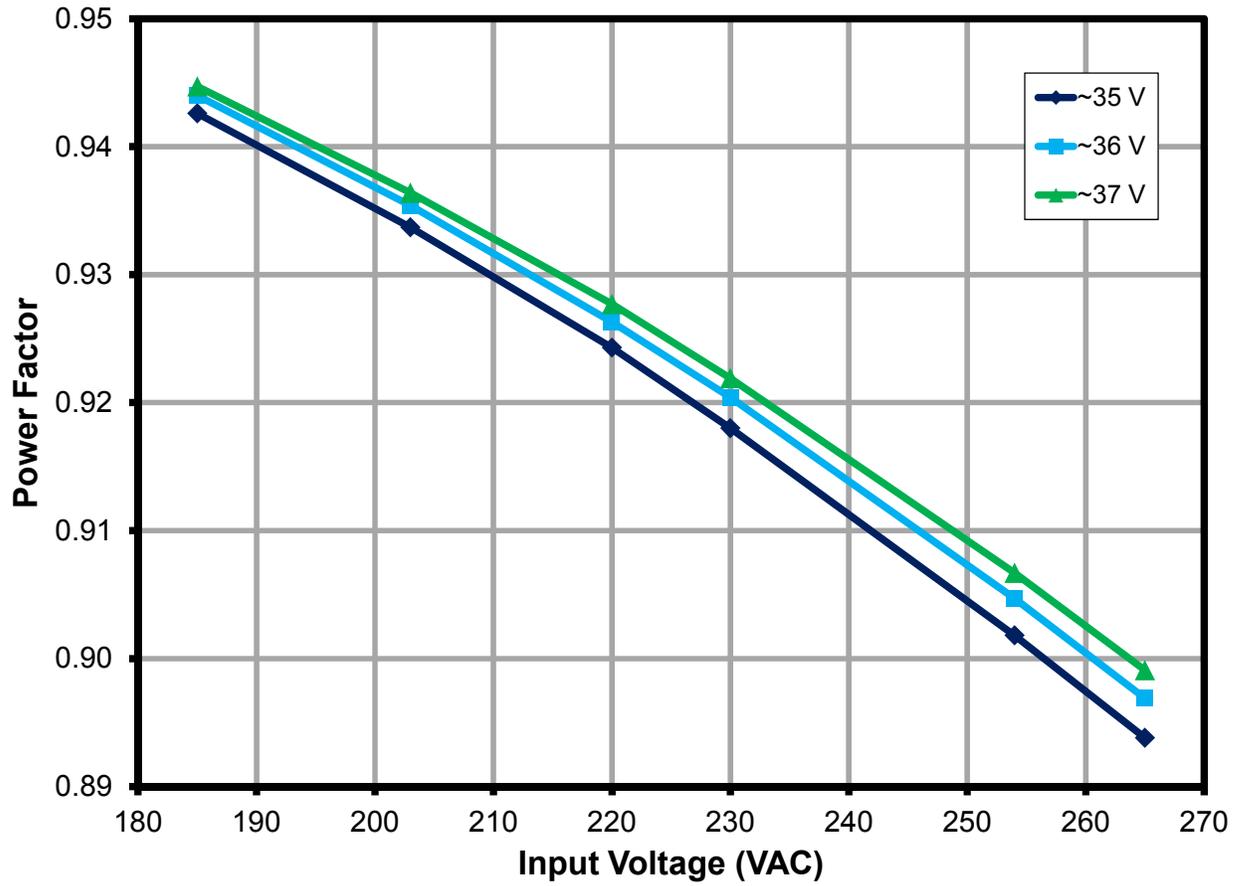


Figure 12 – Power Factor vs. Line and Load.



9.4 A-THD

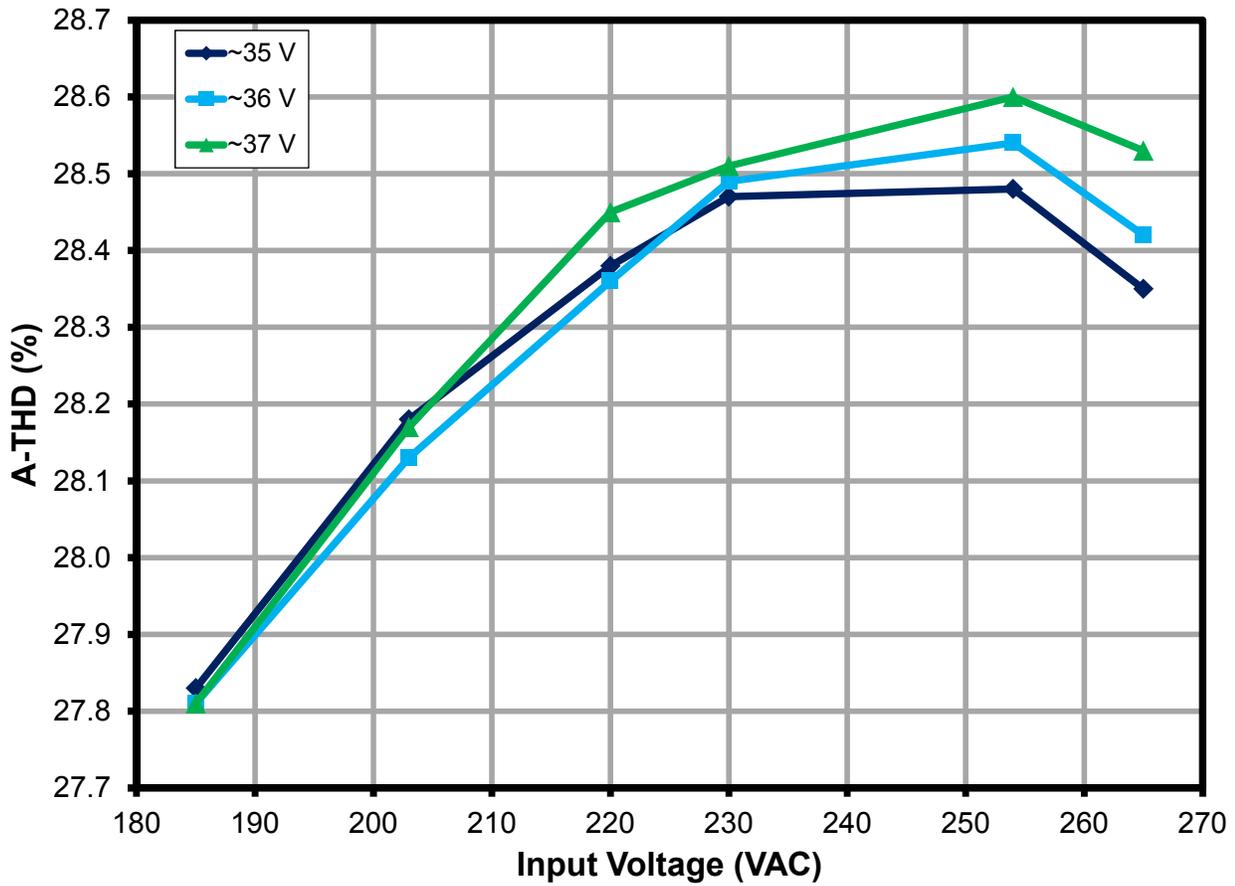


Figure 13 – A-THD vs. Line and Load.



9.5 Harmonic Currents

The design met the limits for Class C equipment for an active input power of <25 W. In this case IEC61000-3-2 specifies that harmonic currents shall not exceed the limits of Class D equipment¹. Therefore the limits shown in the charts below are Class D limits which must not be exceeded to meet Class C compliance.

9.5.1 35 V LED Load

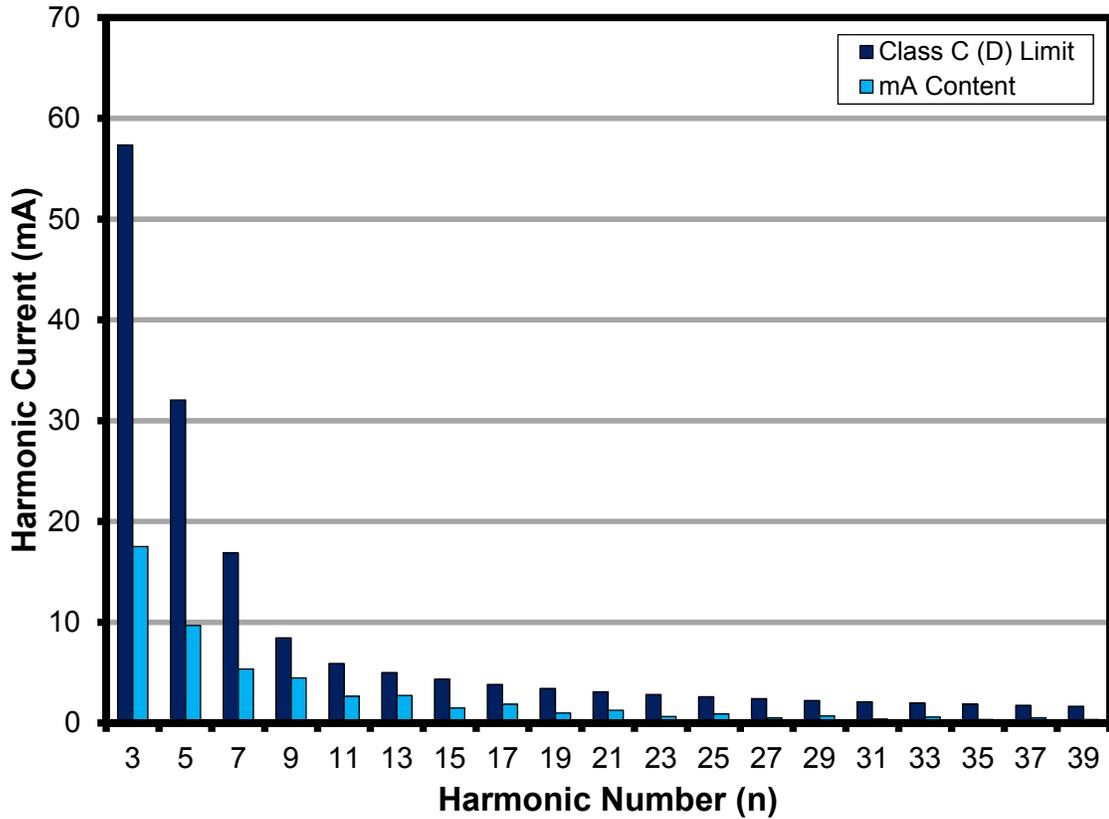


Figure 14 – 35 V LED Load Input Current Harmonics at 230 VAC, 50 Hz.

¹ IEC6000-3-2 Section 7.3, table 2, column 2.



9.5.3 36 V LED Load

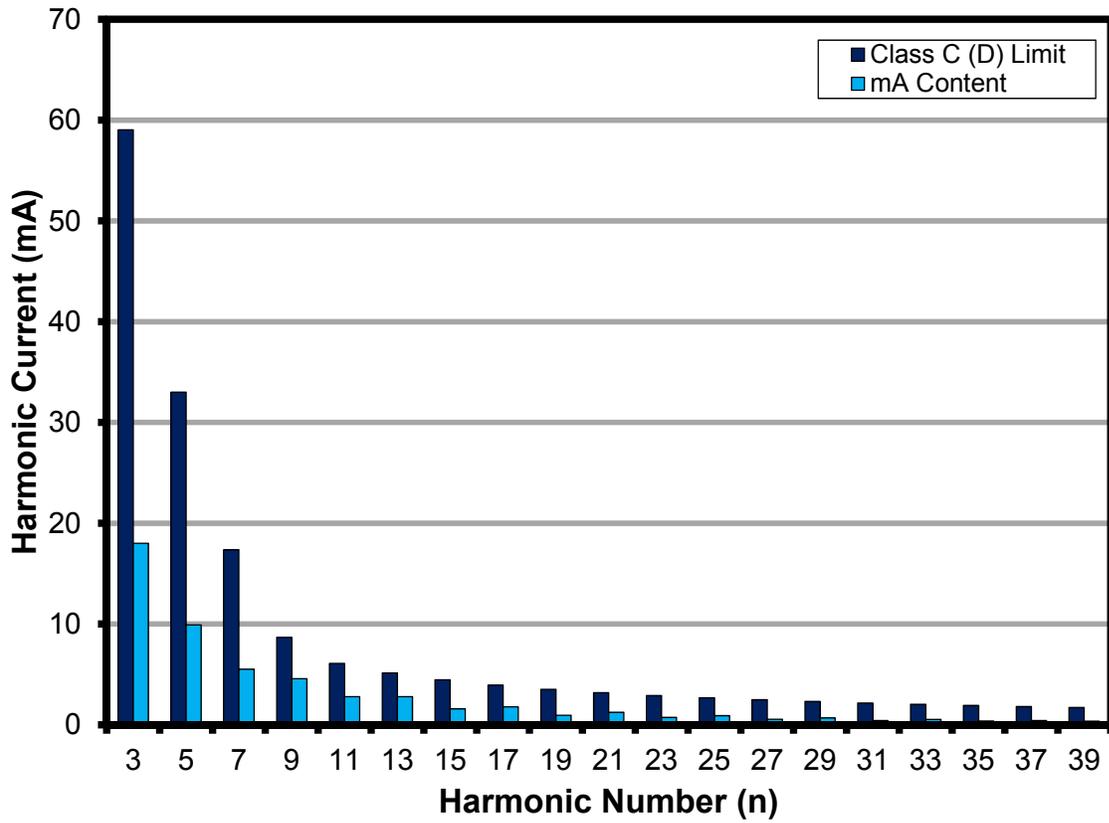


Figure 15 – 36 V LED Load Input Current Harmonics at 230 VAC, 50 Hz.



9.5.4 37 V LED Load

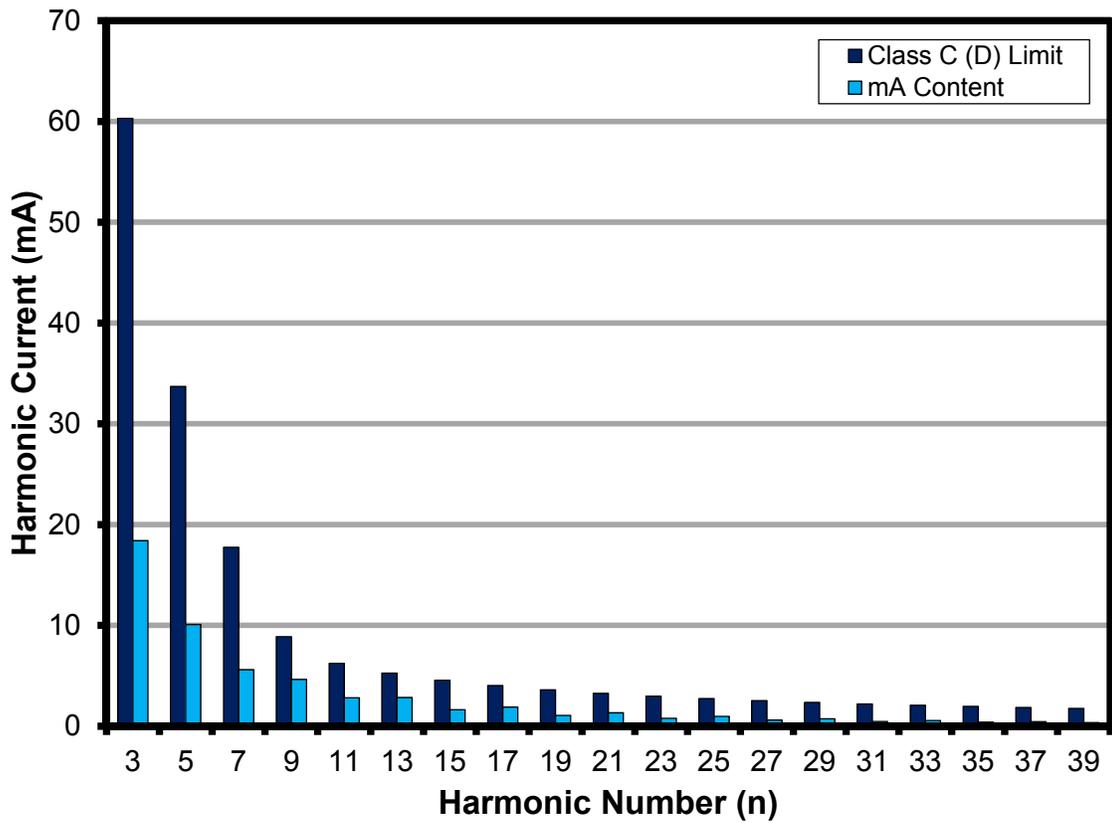


Figure 16 – 37 V LED Load Input Current Harmonics at 230 VAC, 50 Hz.



9.6 Test Data

All measurements were taken with the board at open frame, 25 °C ambient, and 50 Hz line frequency.

9.6.1 Test Data, 35 V LED Load

| Input Measurement | | | | | Load Measurement | | | Calculation | | |
|--|---|------------------------|-------|-------|--|---|-------------------------|-------------------------|-------------------|-------------|
| V _{IN} (V _{RMS}) | I _{IN} (mA _{RMS}) | P _{IN} (W) | PF | %ATHD | V _{OUT} (V _{DC}) | I _{OUT} (mA _{DC}) | P _{OUT} (W) | P _{CAL} (W) | Efficiency (%) | Loss (W) |
| 185.03 | 90.22 | 15.734 | 0.943 | 27.83 | 35.11 | 389.21 | 13.710 | 13.66 | 87.14 | 2.02 |
| 203.06 | 85.46 | 16.204 | 0.934 | 28.18 | 35.18 | 400.28 | 14.128 | 14.08 | 87.19 | 2.08 |
| 220.08 | 81.74 | 16.626 | 0.924 | 28.38 | 35.23 | 409.96 | 14.492 | 14.44 | 87.16 | 2.13 |
| 230.13 | 79.86 | 16.871 | 0.918 | 28.47 | 35.25 | 415.58 | 14.701 | 14.65 | 87.14 | 2.17 |
| 254.10 | 76.17 | 17.454 | 0.902 | 28.48 | 35.32 | 428.33 | 15.183 | 15.13 | 86.99 | 2.27 |
| 265.11 | 74.76 | 17.715 | 0.894 | 28.35 | 35.35 | 433.96 | 15.394 | 15.34 | 86.90 | 2.32 |

9.6.2 Test Data, 36 V LED Load

| Input Measurement | | | | | Load Measurement | | | Calculation | | |
|--|---|------------------------|-------|-------|--|---|-------------------------|-------------------------|-------------------|-------------|
| V _{IN} (V _{RMS}) | I _{IN} (mA _{RMS}) | P _{IN} (W) | PF | %ATHD | V _{OUT} (V _{DC}) | I _{OUT} (mA _{DC}) | P _{OUT} (W) | P _{CAL} (W) | Efficiency (%) | Loss (W) |
| 185.00 | 92.88 | 16.219 | 0.944 | 27.81 | 36.14 | 389.94 | 14.14 | 14.09 | 87.15 | 2.08 |
| 203.05 | 87.90 | 16.695 | 0.935 | 28.13 | 36.20 | 400.96 | 14.56 | 14.51 | 87.21 | 2.14 |
| 220.06 | 83.99 | 17.120 | 0.926 | 28.36 | 36.24 | 410.58 | 14.93 | 14.88 | 87.20 | 2.19 |
| 230.11 | 81.98 | 17.363 | 0.920 | 28.49 | 36.26 | 416.04 | 15.14 | 15.09 | 87.17 | 2.23 |
| 254.08 | 78.08 | 17.947 | 0.905 | 28.54 | 36.32 | 428.66 | 15.62 | 15.57 | 87.03 | 2.33 |
| 265.10 | 76.59 | 18.210 | 0.897 | 28.42 | 36.34 | 434.20 | 15.83 | 15.78 | 86.95 | 2.38 |

9.6.3 Test Data, 37 V LED Load

| Input Measurement | | | | | Load Measurement | | | Calculation | | |
|--|---|------------------------|-------|-------|--|---|-------------------------|-------------------------|-------------------|-------------|
| V _{IN} (V _{RMS}) | I _{IN} (mA _{RMS}) | P _{IN} (W) | PF | %ATHD | V _{OUT} (V _{DC}) | I _{OUT} (mA _{DC}) | P _{OUT} (W) | P _{CAL} (W) | Efficiency (%) | Loss (W) |
| 185.00 | 94.83 | 16.573 | 0.945 | 27.81 | 36.88 | 390.53 | 14.45 | 14.40 | 87.18 | 2.13 |
| 203.04 | 89.70 | 17.055 | 0.936 | 28.17 | 36.95 | 401.45 | 14.88 | 14.83 | 87.24 | 2.18 |
| 220.06 | 85.68 | 17.490 | 0.928 | 28.45 | 37.00 | 411.10 | 15.26 | 15.21 | 87.24 | 2.23 |
| 230.11 | 83.61 | 17.737 | 0.922 | 28.51 | 37.02 | 416.54 | 15.47 | 15.42 | 87.22 | 2.27 |
| 254.07 | 79.57 | 18.329 | 0.907 | 28.6 | 37.09 | 429.01 | 15.96 | 15.91 | 87.09 | 2.37 |
| 265.09 | 78.02 | 18.595 | 0.899 | 28.53 | 37.11 | 434.58 | 16.18 | 16.13 | 87.01 | 2.42 |



9.6.4 230 VAC 50 Hz, 35 V LED Load Harmonics Data

| V | Freq | I (mA) | P | PF | %THD |
|-----------|------------|-----------|-------------|-------------|---------|
| 230 | 50.00 | 79.86 | 16.8710 | 0.9180 | 28.47 |
| nth Order | mA Content | % Content | Limit <25 W | Limit >25 W | Remarks |
| 1 | 76.74 | | | | |
| 2 | 0.02 | 0.03% | | 2.00% | |
| 3 | 17.52 | 22.83% | 57.3614 | 27.54% | Pass |
| 5 | 9.67 | 12.60% | 32.0549 | 10.00% | Pass |
| 7 | 5.34 | 6.96% | 16.8710 | 7.00% | Pass |
| 9 | 4.46 | 5.81% | 8.4355 | 5.00% | Pass |
| 11 | 2.64 | 3.44% | 5.9049 | 3.00% | Pass |
| 13 | 2.73 | 3.56% | 4.9964 | 3.00% | Pass |
| 15 | 1.49 | 1.94% | 4.3302 | 3.00% | Pass |
| 17 | 1.85 | 2.41% | 3.8208 | 3.00% | Pass |
| 19 | 0.99 | 1.29% | 3.4186 | 3.00% | Pass |
| 21 | 1.26 | 1.64% | 3.0930 | 3.00% | Pass |
| 23 | 0.65 | 0.85% | 2.8241 | 3.00% | Pass |
| 25 | 0.90 | 1.17% | 2.5981 | 3.00% | Pass |
| 27 | 0.50 | 0.65% | 2.4057 | 3.00% | Pass |
| 29 | 0.69 | 0.90% | 2.2398 | 3.00% | Pass |
| 31 | 0.39 | 0.51% | 2.0953 | 3.00% | Pass |
| 33 | 0.58 | 0.76% | 1.9683 | 3.00% | Pass |
| 35 | 0.35 | 0.46% | 1.8558 | 3.00% | Pass |
| 37 | 0.49 | 0.64% | 1.7555 | 3.00% | Pass |
| 39 | 0.34 | 0.44% | 1.6655 | 3.00% | Pass |
| 41 | 0.37 | 0.48% | | | |
| 43 | 0.31 | 0.40% | | | |
| 45 | 0.32 | 0.42% | | | |
| 47 | 0.40 | 0.52% | | | |
| 49 | 0.30 | 0.39% | | | |



9.6.5 230 VAC 50 Hz, 36 V LED Load Harmonics Data

| V | Freq | I (mA) | P | PF | %THD |
|-----------|------------|-----------|-------------|-------------|---------|
| 230 | 50.00 | 81.98 | 17.3630 | 0.9204 | 28.49 |
| nth Order | mA Content | % Content | Limit <25 W | Limit >25 W | Remarks |
| 1 | 78.78 | | | | |
| 2 | 0.05 | 0.06% | | 2.00% | |
| 3 | 18.01 | 22.86% | 59.0342 | 27.61% | Pass |
| 5 | 9.91 | 12.58% | 32.9897 | 10.00% | Pass |
| 7 | 5.51 | 6.99% | 17.3630 | 7.00% | Pass |
| 9 | 4.57 | 5.80% | 8.6815 | 5.00% | Pass |
| 11 | 2.78 | 3.53% | 6.0771 | 3.00% | Pass |
| 13 | 2.80 | 3.55% | 5.1421 | 3.00% | Pass |
| 15 | 1.58 | 2.01% | 4.4565 | 3.00% | Pass |
| 17 | 1.77 | 2.25% | 3.9322 | 3.00% | Pass |
| 19 | 0.95 | 1.21% | 3.5183 | 3.00% | Pass |
| 21 | 1.24 | 1.57% | 3.1832 | 3.00% | Pass |
| 23 | 0.72 | 0.91% | 2.9064 | 3.00% | Pass |
| 25 | 0.91 | 1.16% | 2.6739 | 3.00% | Pass |
| 27 | 0.56 | 0.71% | 2.4758 | 3.00% | Pass |
| 29 | 0.69 | 0.88% | 2.3051 | 3.00% | Pass |
| 31 | 0.43 | 0.55% | 2.1564 | 3.00% | Pass |
| 33 | 0.52 | 0.66% | 2.0257 | 3.00% | Pass |
| 35 | 0.38 | 0.48% | 1.9099 | 3.00% | Pass |
| 37 | 0.42 | 0.53% | 1.8067 | 3.00% | Pass |
| 39 | 0.36 | 0.46% | 1.7140 | 3.00% | Pass |
| 41 | 0.38 | 0.48% | | | |
| 43 | 0.30 | 0.38% | | | |
| 45 | 0.32 | 0.41% | | | |
| 47 | 0.28 | 0.36% | | | |
| 49 | 0.22 | 0.28% | | | |



9.6.6 230 VAC 50 Hz, 37 V LED Load Harmonics Data

| V | Freq | I (mA) | P | PF | %THD |
|-----------|------------|-----------|-------------|-------------|---------|
| 230 | 50.00 | 83.61 | 17.7370 | 0.9219 | 28.51 |
| nth Order | mA Content | % Content | Limit <25 W | Limit >25 W | Remarks |
| 1 | 80.35 | | | | |
| 2 | 0.03 | 0.04% | | 2.00% | |
| 3 | 18.39 | 22.89% | 60.3058 | 27.66% | Pass |
| 5 | 10.09 | 12.56% | 33.7003 | 10.00% | Pass |
| 7 | 5.61 | 6.98% | 17.7370 | 7.00% | Pass |
| 9 | 4.64 | 5.77% | 8.8685 | 5.00% | Pass |
| 11 | 2.82 | 3.51% | 6.2080 | 3.00% | Pass |
| 13 | 2.84 | 3.53% | 5.2529 | 3.00% | Pass |
| 15 | 1.63 | 2.03% | 4.5525 | 3.00% | Pass |
| 17 | 1.89 | 2.35% | 4.0169 | 3.00% | Pass |
| 19 | 1.06 | 1.32% | 3.5941 | 3.00% | Pass |
| 21 | 1.32 | 1.64% | 3.2518 | 3.00% | Pass |
| 23 | 0.77 | 0.96% | 2.9690 | 3.00% | Pass |
| 25 | 0.96 | 1.19% | 2.7315 | 3.00% | Pass |
| 27 | 0.59 | 0.73% | 2.5292 | 3.00% | Pass |
| 29 | 0.72 | 0.90% | 2.3547 | 3.00% | Pass |
| 31 | 0.46 | 0.57% | 2.2028 | 3.00% | Pass |
| 33 | 0.55 | 0.68% | 2.0693 | 3.00% | Pass |
| 35 | 0.40 | 0.50% | 1.9511 | 3.00% | Pass |
| 37 | 0.44 | 0.55% | 1.8456 | 3.00% | Pass |
| 39 | 0.35 | 0.44% | 1.7510 | 3.00% | Pass |
| 41 | 0.37 | 0.46% | | | |
| 43 | 0.32 | 0.40% | | | |
| 45 | 0.28 | 0.35% | | | |
| 47 | 0.27 | 0.34% | | | |
| 49 | 0.20 | 0.25% | | | |



10 Dimming Performance Data

TRIAC dimming results were taken at an input voltage of 230 VAC, 50 Hz line frequency, room temperature, and a nominal 36 V LED load.

The output current High Limit I_{OUT} (HL) and Low Limit I_{OUT} (LL) were incorporated based on the USA NEMA Publication SSL6-2010 Section 4 page 9 for dimming performance system requirements for reference. The standard however refers to 120 VAC operating input voltage and pertains to the limits as relative light output. The limits incorporated on the succeeding graphs assumes that 100% relative light output falls on the maximum operating output current of 425 mA and 0 mA as 0% light output, and input line of 230 VAC, 50 Hz.

10.1 Performance with Clipsal Brand (Australian market) Dimmers

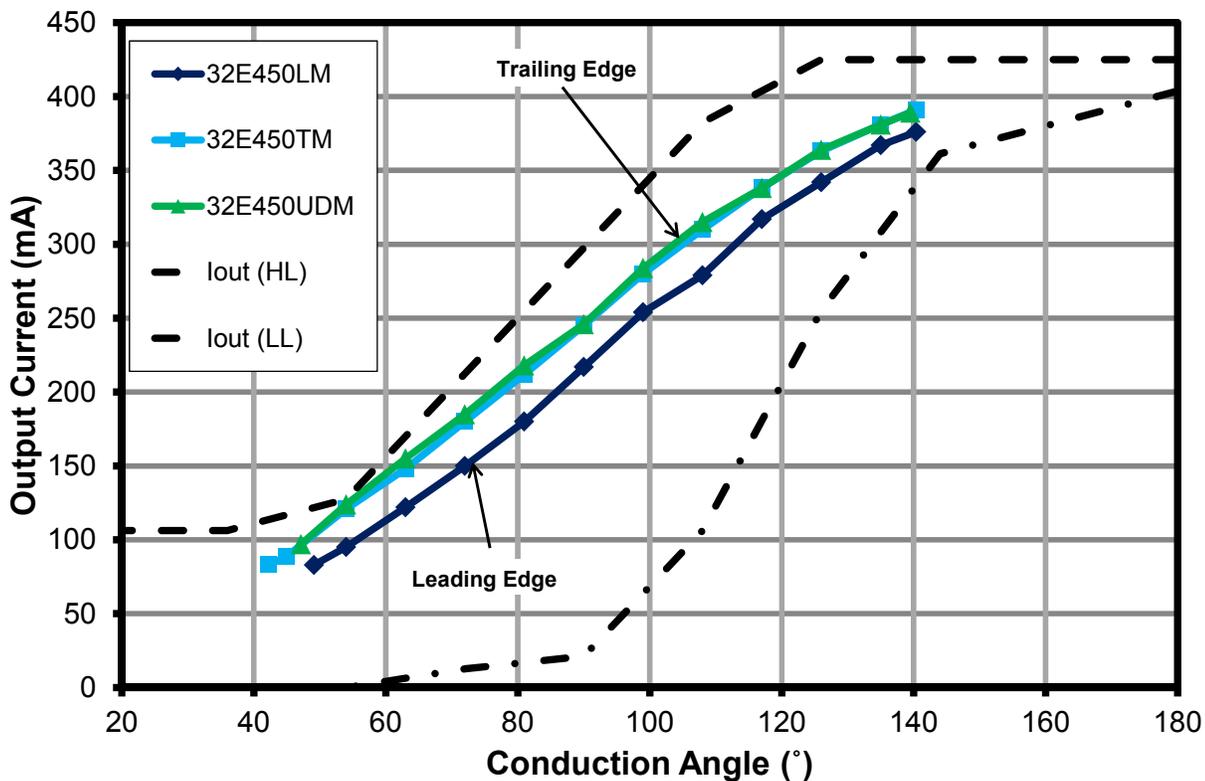


Figure 17 – Clipsal Dimmers Dimming Curve at 230 VAC, 50 Hz Input.

| Dimmer | Minimum Conduction Angle, (°) | Minimum I_{OUT} (mA) | Maximum Conduction Angle, (°) | Maximum I_{OUT} (mA) | Dim Ratio |
|-----------|-------------------------------|------------------------|-------------------------------|------------------------|-----------|
| 32E450LM | 49.14 | 83 | 140.4 | 376 | 4.5 |
| 32E450TM | 42.3 | 83 | 140.4 | 391 | 4.7 |
| 32E450UDM | 47.16 | 97 | 139.5 | 389 | 4.0 |

Figure 18 – Clipsal Dimmers Minimum and Maximum Dimming Characteristic at 230 VAC, 50 Hz Input.

10.2 Performance with China Dimmers

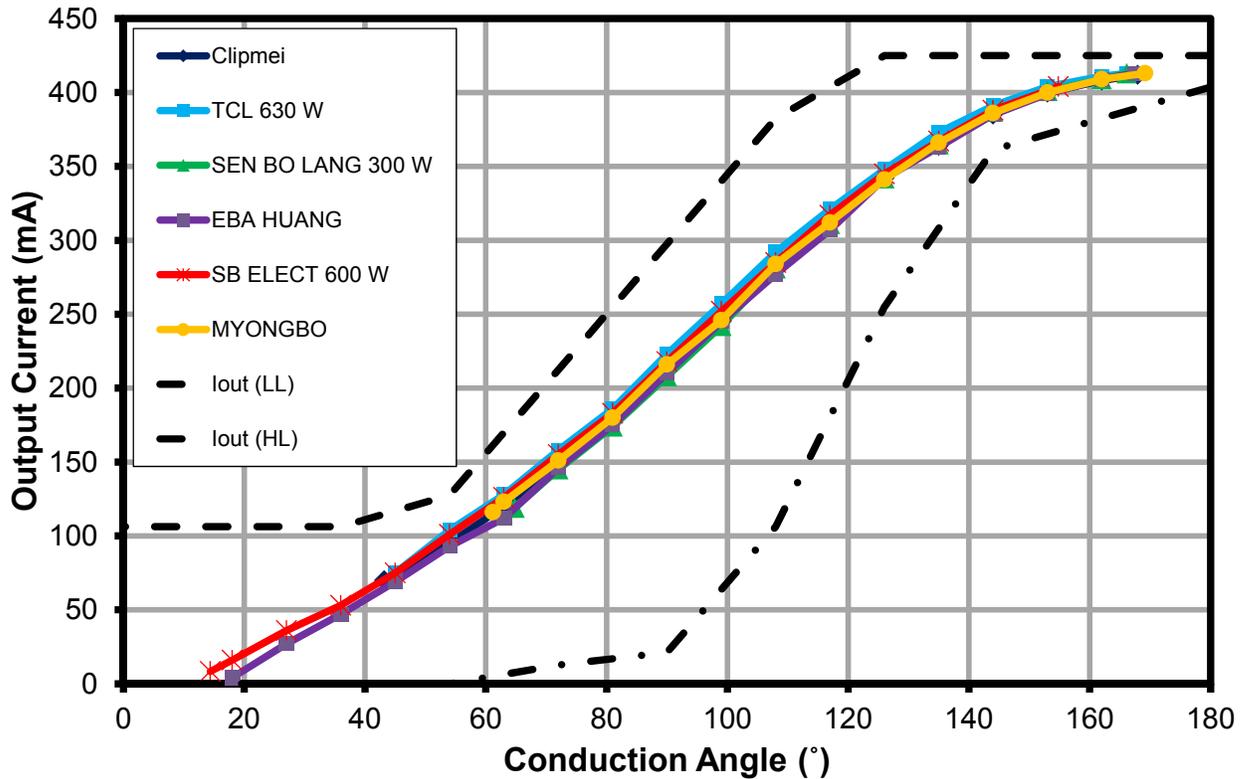


Figure 19 – China Dimmers Dimming Curve at 230 VAC, 50 Hz Input.

| Dimmer | Minimum Conduction Angle, (°) | Minimum I _{OUT} (mA) | Maximum Conduction Angle, (°) | Maximum I _{OUT} (mA) | Dim Ratio |
|-------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-----------|
| CLIPMEI | 43.2 | 70 | 167.94 | 412 | 5.9 |
| TCL 630 W | 45 | 75 | 166.14 | 413 | 5.5 |
| SEN BO LANG 300 W | 64.8 | 119 | 166.14 | 413 | 3.5 |
| EBA HUANG | 18 | 4.2 | 167.4 | 413 | 98.3 |
| SB ELECT 600 W | 14.4 | 8.4 | 154.8 | 404 | 48.1 |
| MYONGBO | 61.2 | 116 | 169.2 | 413 | 3.6 |
| KBE 650 W | 14.4 | 3 | 165.6 | 412 | 137.3 |
| MANK 200 W | 70.2 | 136 | 165.6 | 412 | 3.0 |

Figure 20 – China Dimmers Minimum and Maximum Dimming Characteristic at 230 VAC, 50 Hz Input.



10.3 Performance with Korean Dimmers

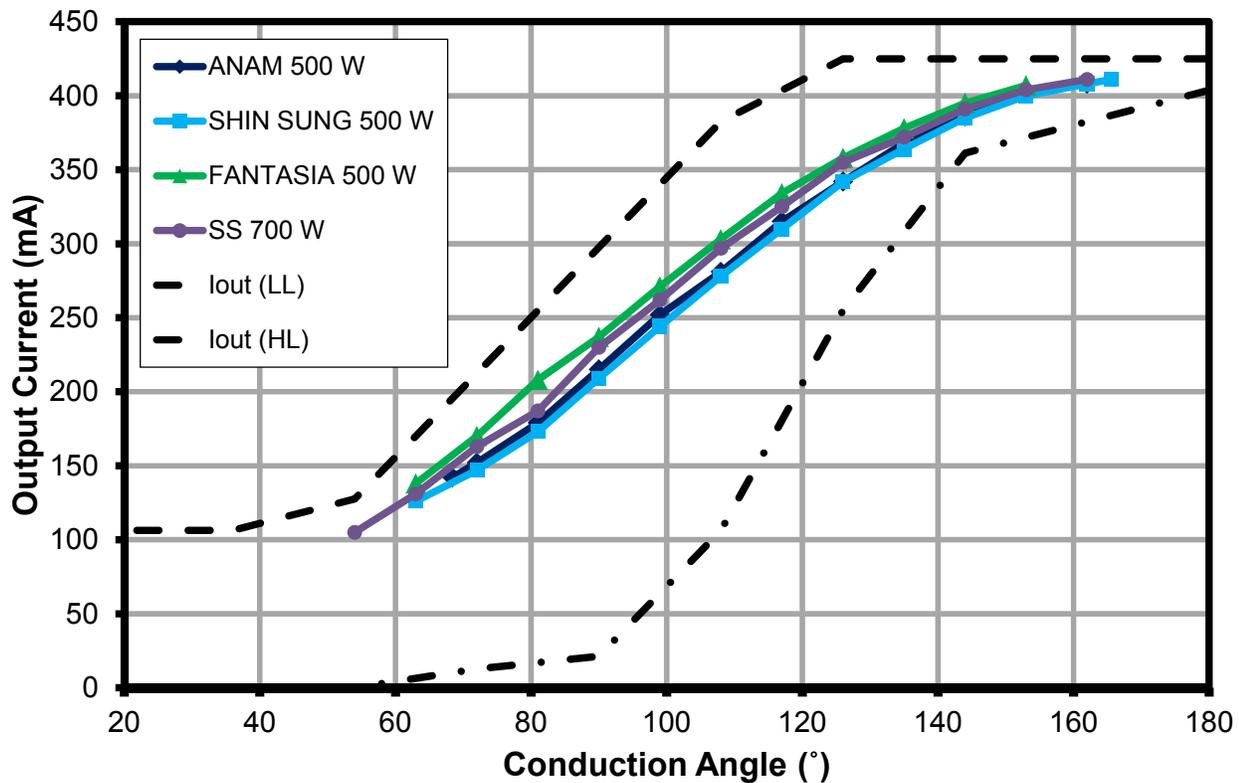


Figure 21 – Korean Dimmers Dimming Curve at 230 VAC, 50 Hz Input.

| Dimmer | Minimum Conduction Angle, (°) | Minimum I _{OUT} (mA) | Maximum Conduction Angle, (°) | Maximum I _{OUT} (mA) | Dim Ratio |
|-----------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-----------|
| ANAM 500 W | 68.4 | 142 | 162 | 408 | 2.9 |
| SHIN SUNG 500 W | 63 | 126 | 165.6 | 411 | 3.3 |
| FANTASIA 500 W | 63 | 138 | 153 | 407 | 2.9 |
| SS 700 W | 54 | 105 | 162 | 411 | 3.9 |

Figure 22 – Korean Dimmers Minimum and Maximum Dimming Characteristic at 230 VAC, 50 Hz Input.

10.4 Performance with German Dimmers

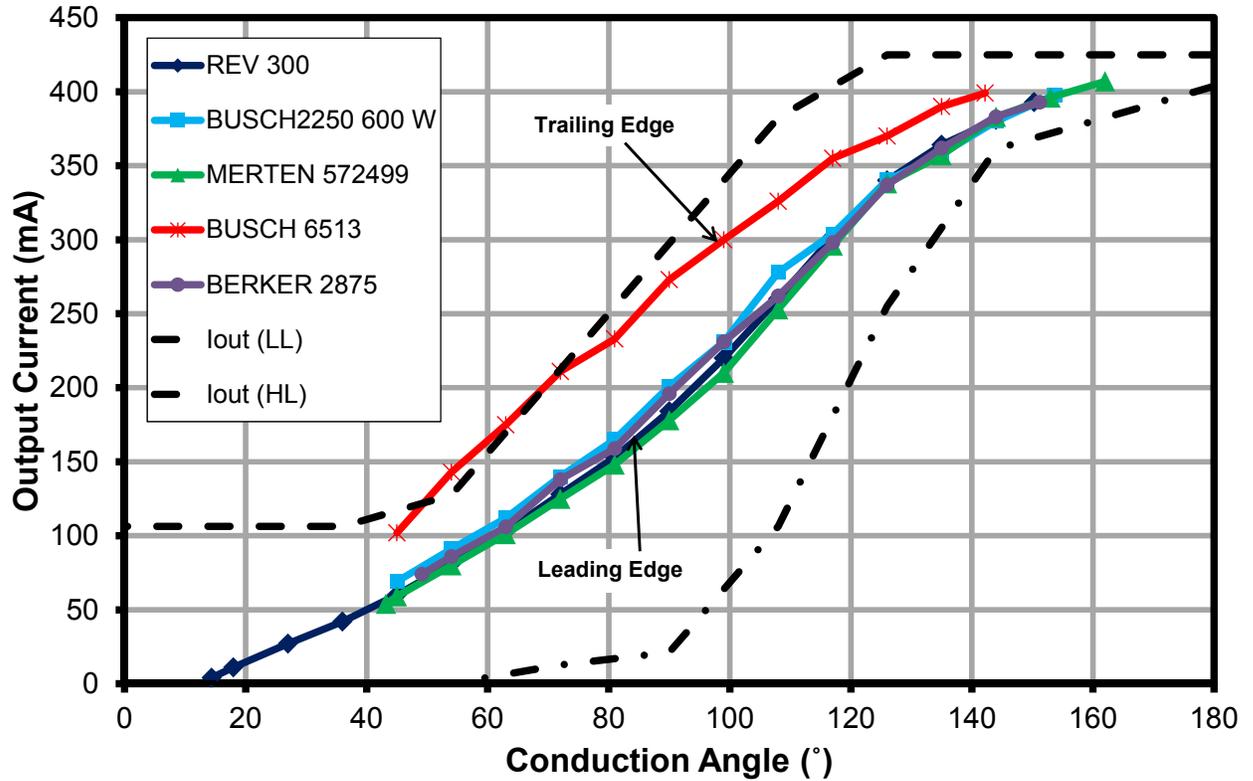


Figure 23 – German Dimmers Dimming Curve at 230 VAC, 50 Hz Input.

| Dimmer | Minimum Conduction Angle, (°) | Minimum I _{OUT} (mA) | Maximum Conduction Angle, (°) | Maximum I _{OUT} (mA) | Dim Ratio |
|---------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-----------|
| REV300 | 14.4 | 4 | 150.3 | 393 | 98.3 |
| BUSCH 2250 600 W | 45 | 69 | 153.72 | 398 | 5.8 |
| MERTEN 572499 400 W | 43.2 | 54 | 162 | 407 | 7.5 |
| BUSCH 6513 420 W | 39.6 | 90 | 142.2 | 399 | 4.4 |
| BERKER 2875 600 W | 49.14 | 74 | 151.2 | 393 | 5.3 |

Figure 24 – German Dimmers Minimum and Maximum Dimming Characteristic at 230 VAC, 50 Hz Input.



11 Thermal Performance

Images captured after running for >30 minutes at room temperature (25 °C), open frame for the conditions specified.

11.1 Non-Dimming $V_{IN} = 185 \text{ VAC}$, 50 Hz, 36 V LED Load

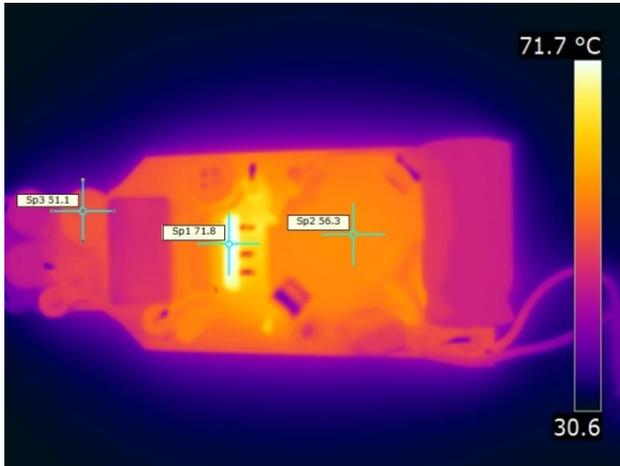


Figure 25 – Top Side.

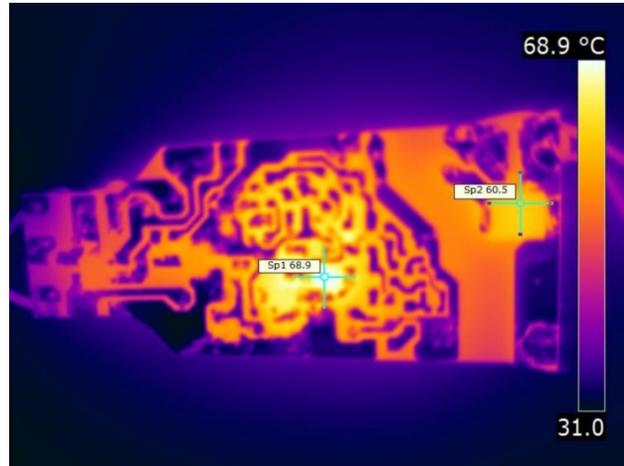


Figure 26 – Bottom Side.

11.2 Non-Dimming $V_{IN} = 265 \text{ VAC}$, 50 Hz, 36 V LED Load

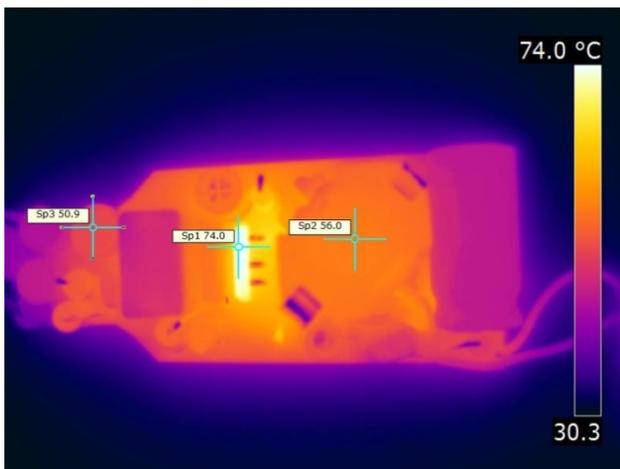


Figure 27 – Top Side.

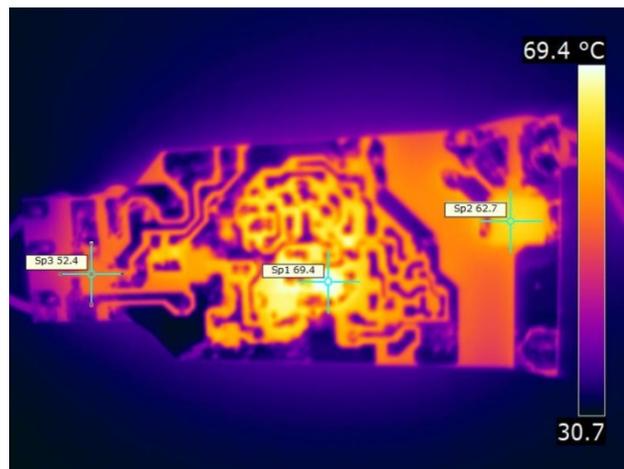


Figure 28 – Bottom Side.



11.3 Dimming $V_{IN} = 230\text{ VAC}$, 50 Hz, 90° Conduction Angle, 36 V LED Load

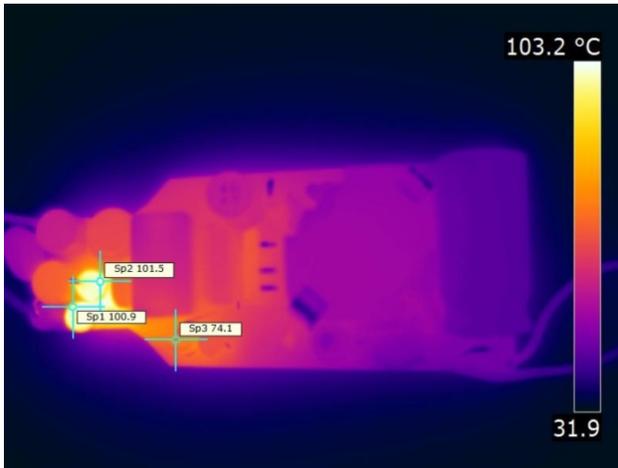


Figure 29 – Top Side.

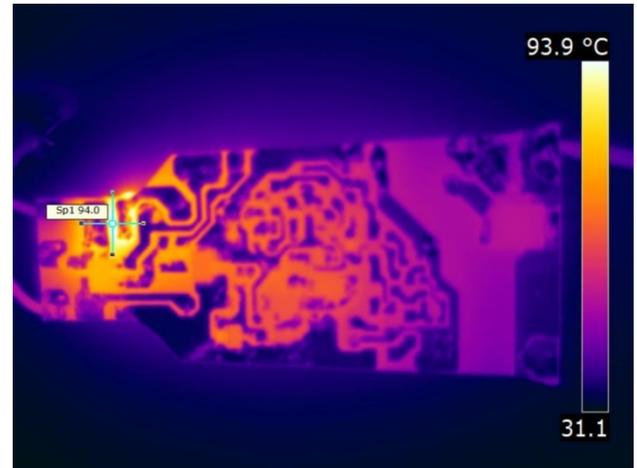


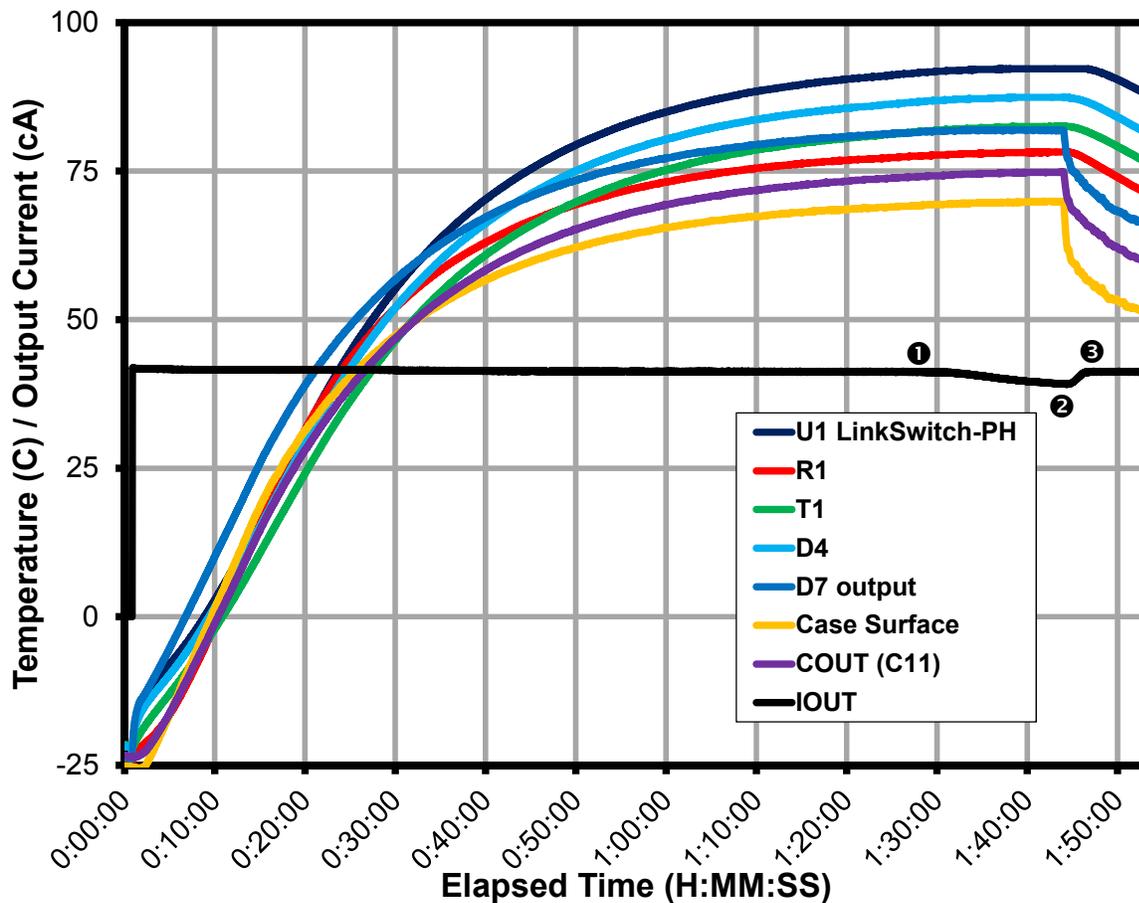
Figure 30 – Bottom Side.



11.4 Thermal Fold Back

A test board had T type thermocouples attached to key components. The unit was then potted using Silgard 170 and placed inside a thermal chamber. A chart recorder was used to monitor the temperature and output current while the external ambient temperature was swept from -25 °C to 70 °C. Testing was performed at 230 VAC, 60 Hz with no dimmer connected. The frequency of 60 Hz was specifically chosen to ensure sampling of chart recorder was synchronized to output of LED driver. Note current is represented in centi-Amps ie a value of 40 = 0.4 A

This data shows (point 1) that the thermal fold back occurs at a case temperature of 70 °C, with an IC temperature of ~92 °C. This indicates that the fold back threshold may be raised further. At point 2 the oven door was opened and the output current returned to the original value (point 3).



Non-Dimming Waveforms

11.5 Input Voltage and Input Current Waveforms

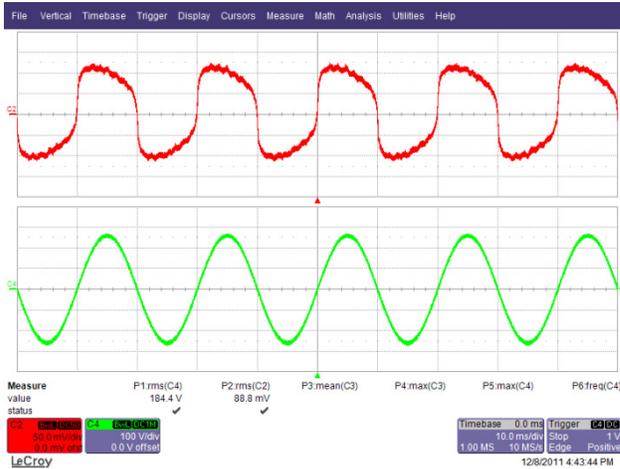


Figure 31 – 185 VAC, Full Load.
 Upper: I_{IN} , 50 mA / div.
 Lower: V_{IN} , 100 V, 10 ms / div.

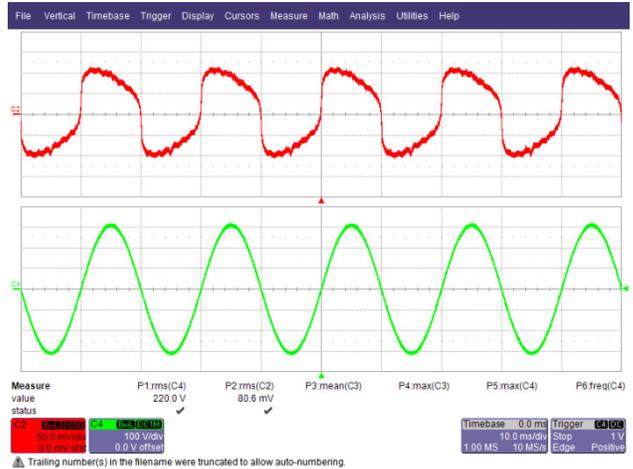


Figure 32 – 220 VAC, Full Load.
 Upper: I_{IN} , 50 mA / div.
 Lower: V_{IN} , 100 V, 10 ms / div.

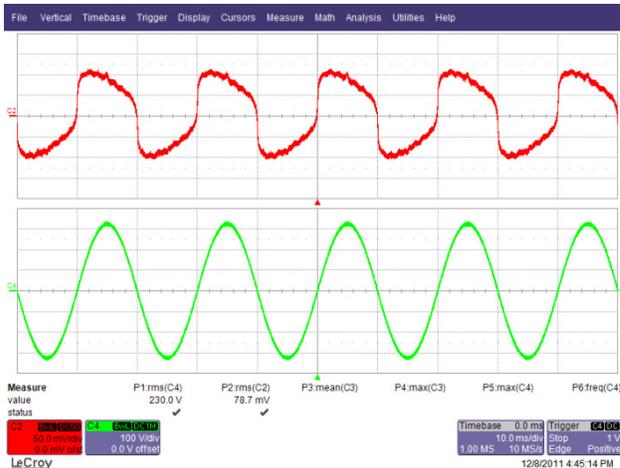


Figure 33 – 230 VAC, Full Load.
 Upper: I_{IN} , 50 mA / div.
 Lower: V_{IN} , 100 V, 10 ms / div.

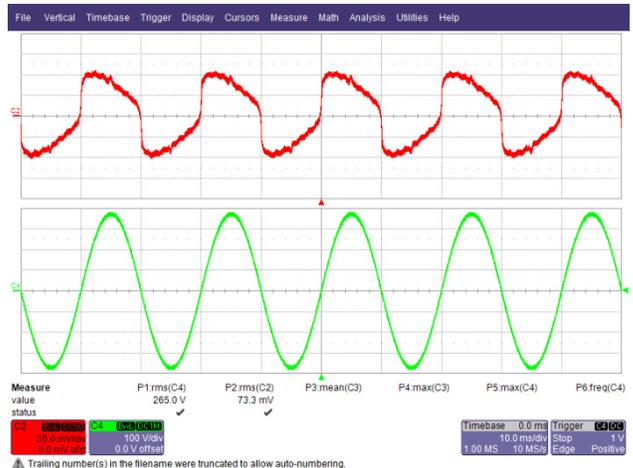


Figure 34 – 265 VAC, Full Load.
 Upper: I_{IN} , 50 mA / div.
 Lower: V_{IN} , 100 V, 10 ms / div.



11.6 Output Current and Output Voltage at Normal Operation

| Input Condition | I _{OUT} , Mean (mA) | I _{OUT} , Peak to Peak (mA) | I _{OUT} Ripple (%) |
|-----------------|------------------------------|--------------------------------------|-----------------------------|
| 185 VAC, 50 Hz | 388 | 250 | ±32.2 |
| 220 VAC, 60 Hz | 412 | 260 | ±31.6 |
| 230 VAC, 50 Hz | 418 | 267 | ±31.94 |
| 265 VAC, 50 Hz | 437 | 278 | ±31.81 |

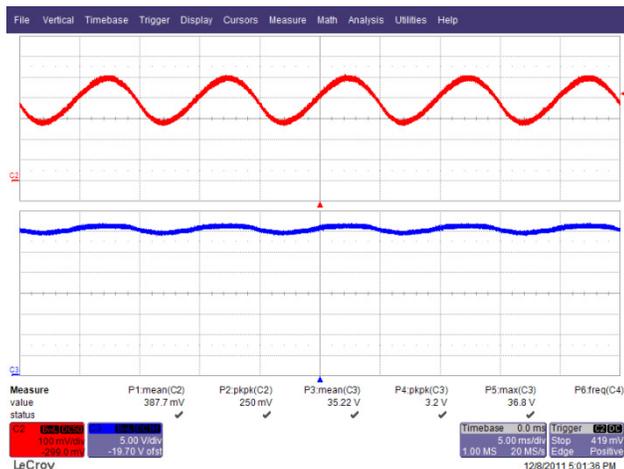


Figure 35 – 185 VAC, 50 Hz Full Load.
Upper: I_{OUT}, 100 mA / div.
Lower: V_{OUT}, 5 V, 5 ms / div.

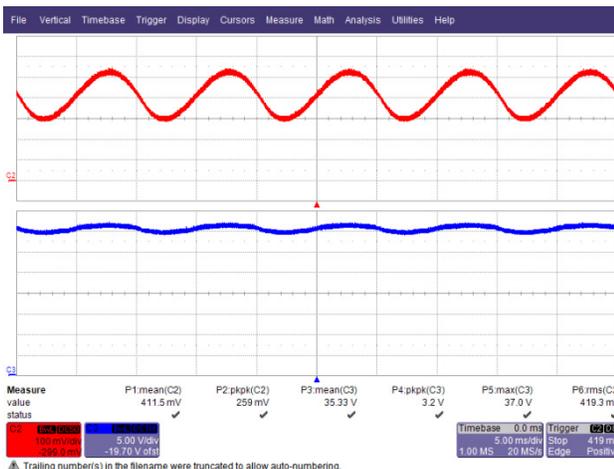


Figure 36 – 220 VAC, 50 Hz Full Load.
Upper: I_{OUT}, 100 mA / div.
Lower: V_{OUT}, 5 V, 5 ms / div.

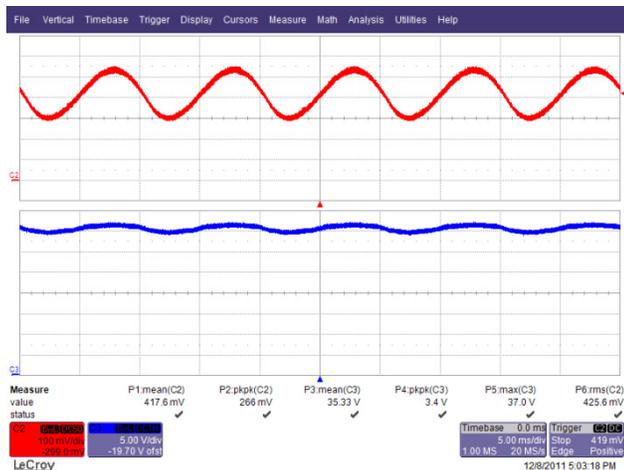


Figure 37 – 230 VAC, 50 Hz Full Load.
Upper: I_{OUT}, 100 mA / div.
Lower: V_{OUT}, 5 V, 5 ms / div.

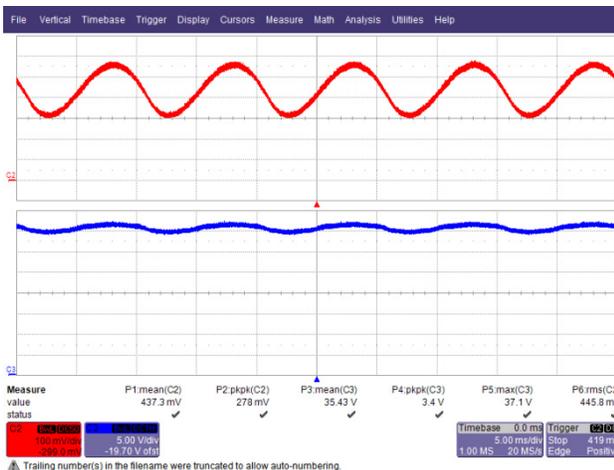


Figure 38 – 265 VAC, 50 Hz Full Load.
Upper: I_{OUT}, 100 mA / div.
Lower: V_{OUT}, 5 V, 5 ms / div.



11.7 Output Current/Voltage Rise and Fall

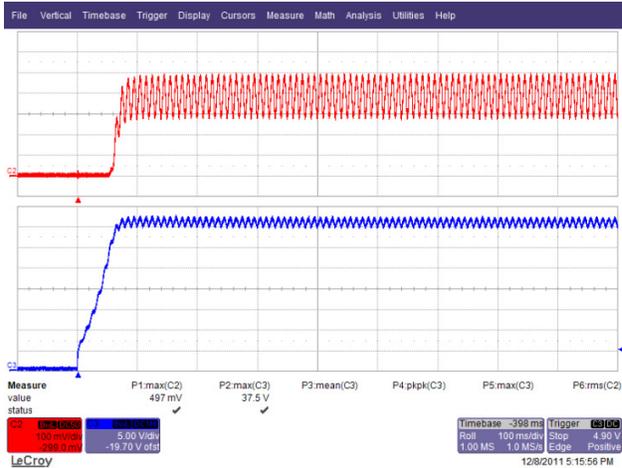


Figure 39 – 185 VAC Output Rise.
Upper: I_{OUT} , 100 mA / div.
Lower: V_{OUT} , 5 V, 100 ms / div.

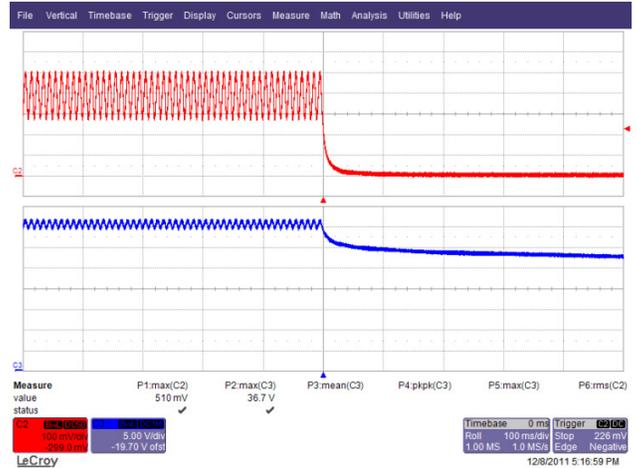


Figure 40 – 185 VAC Output Fall.
Upper: I_{OUT} , 100 mA / div.
Lower: V_{OUT} , 5 V, 100 ms / div.

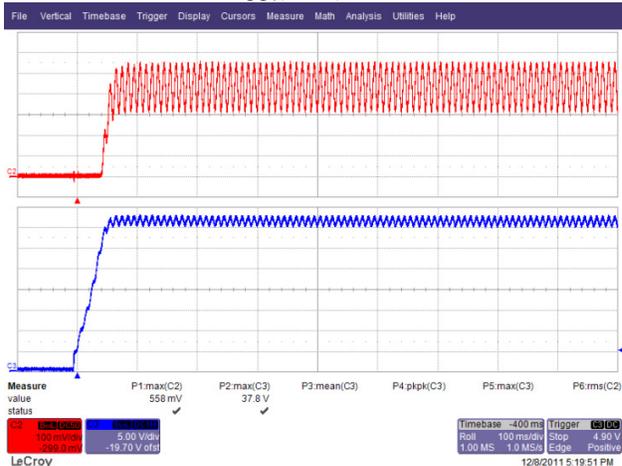


Figure 41 – 265 VAC Output Rise.
Upper: I_{OUT} , 100 mA / div.
Lower: V_{OUT} , 5 V, 100 ms / div.

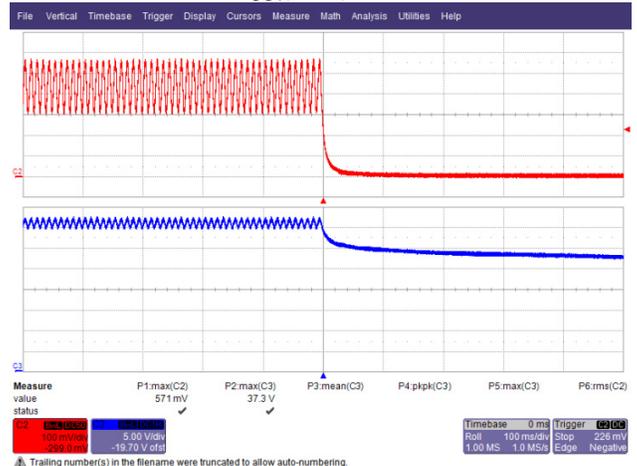


Figure 42 – 265 VAC Output Fall.
Upper: I_{OUT} , 100 mA / div.
Lower: V_{OUT} , 5 V, 100 ms / div.

11.8 Input Voltage and Output Current Waveform at Start-up

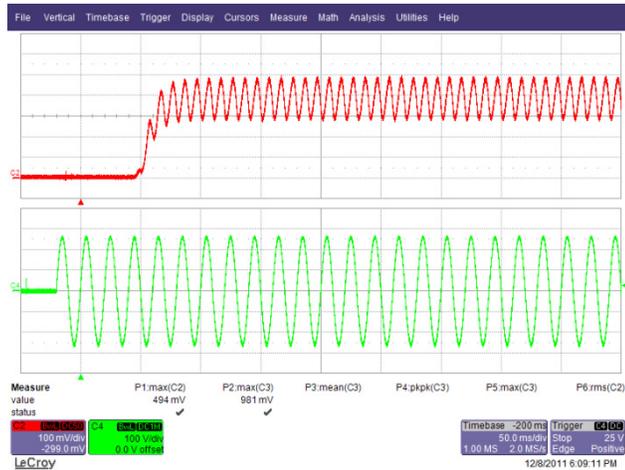


Figure 43 – 185 VAC, 50 Hz.
 Upper: I_{OUT} , 0.1 A / div.
 Lower: V_{IN} , 100 V, 50 ms / div.

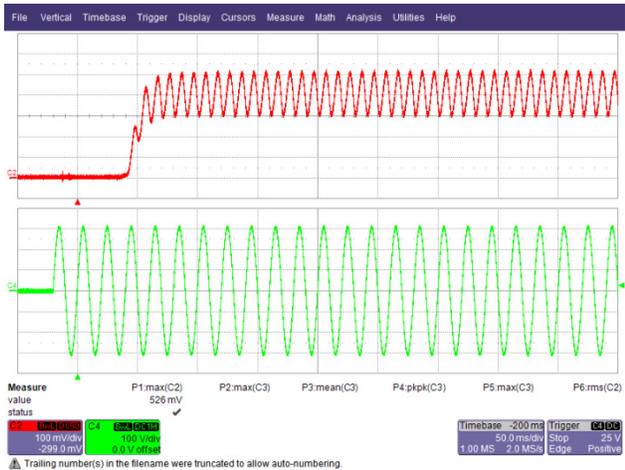


Figure 44 – 220 VAC, 50 Hz.
 Upper: I_{OUT} , 0.1 A / div.
 Lower: V_{IN} , 100 V, 50 ms / div.

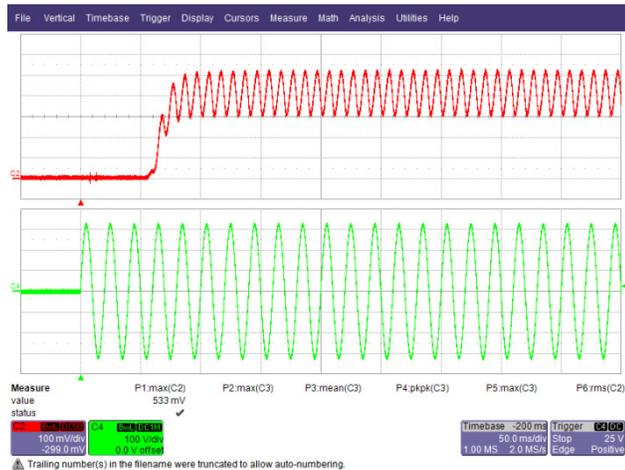


Figure 45 – 230 VAC, 50 Hz.
 Upper: I_{OUT} , 0.1 A / div.
 Lower: V_{IN} , 100 V, 50 ms / div.

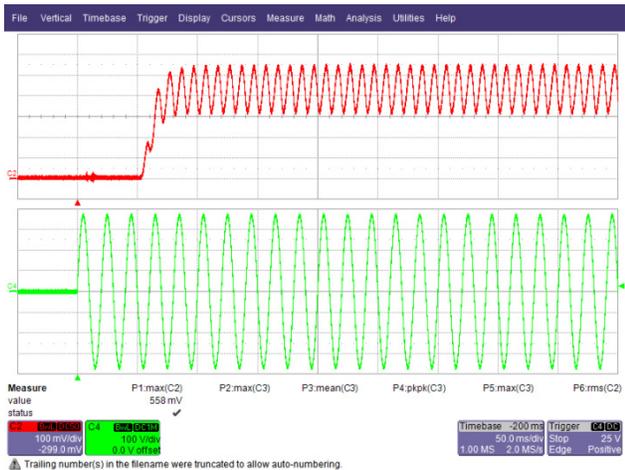


Figure 46 – 265 VAC, 50 Hz.
 Upper: I_{OUT} , 0.1 A / div.
 Lower: V_{IN} , 100 V, 50 ms / div.



11.9 Drain Voltage and Current at Normal Operation

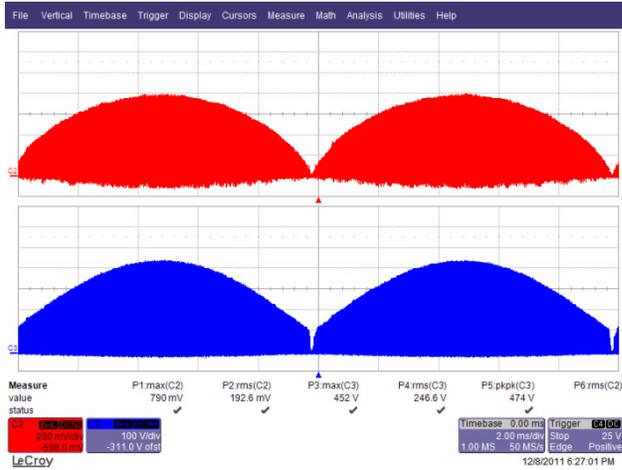


Figure 47 – 185 VAC, 50 Hz.
 Upper: I_{DRAIN} , 0.2 A / div.
 Lower: V_{DRAIN} , 100 V, 2 ms / div.

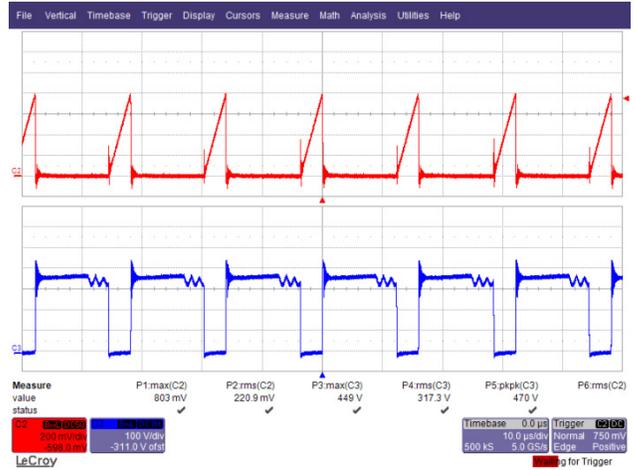


Figure 48 – 185 VAC, 50 Hz.
 Upper: I_{DRAIN} , 0.2 A / div.
 Lower: V_{DRAIN} , 100 V / div., 10 µs / div.

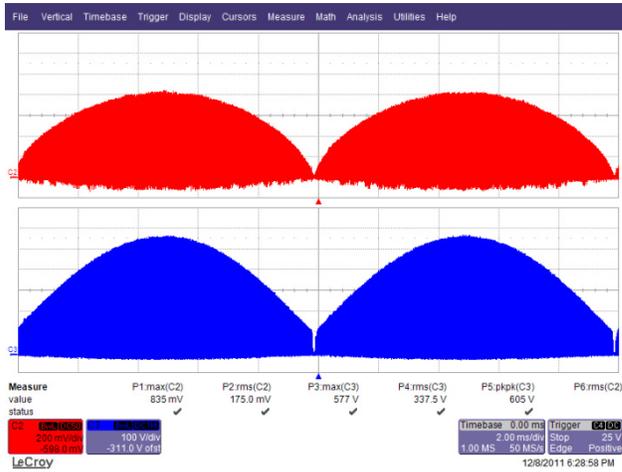


Figure 49 – 265 VAC, 50 Hz.
 Upper: I_{DRAIN} , 0.2 A / div.
 Lower: V_{DRAIN} , 100 V, 2 ms / div.



Figure 50 – 265 VAC, 50 Hz.
 Upper: I_{DRAIN} , 0.2 A / div.
 Lower: V_{DRAIN} , 100 V / div., 10 µs / div.

11.10 Drain Voltage and Current at Start-up

At higher input voltage, the peak current can reach the current limit of the device and enter the SOA mode which disables the switching of the power MOSFET for 40 cycles or approximately 600 μ s. The SOA mode protects the device under short circuit and start-up condition and does not affect the output current rise during start-up since this condition happens when the output capacitor voltage is still far from the conduction voltage of the LED load as shown on the Figures below.

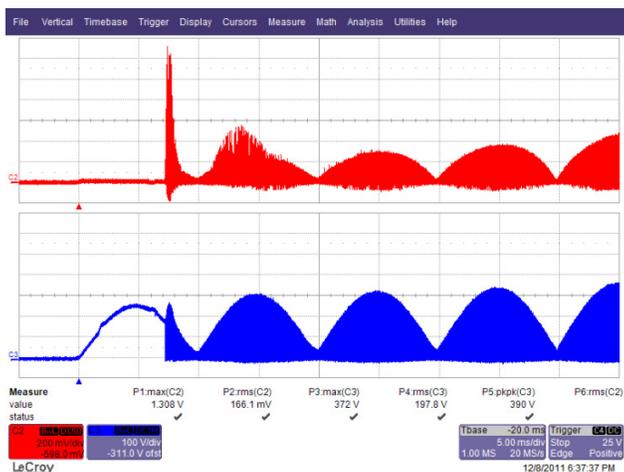


Figure 51 – 185 VAC, 50 Hz Start-up.
Upper: I_{DRAIN} , 200 mA / div.
Lower: V_{DRAIN} , 100 V, 5 ms / div.

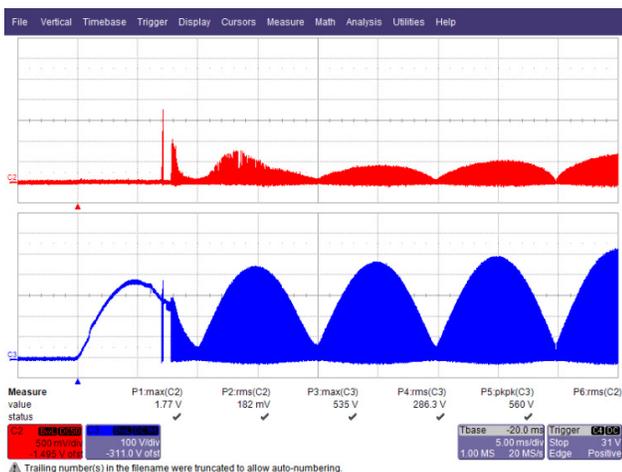


Figure 52 – 265 VAC, 50 Hz Start-up.
Upper: I_{DRAIN} , 500 mA / div.
Lower: V_{DRAIN} , 100 V, 5 ms / div.

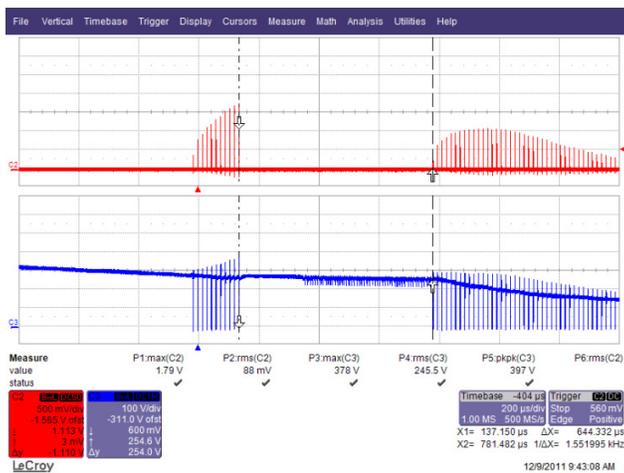


Figure 53 – Expanded 265 VAC Start-up Showing 600 μ s Dead Time.
Upper: I_{DRAIN} , 500 mA / div.
Lower: V_{DRAIN} , 100 V, 0.2 ms / div.

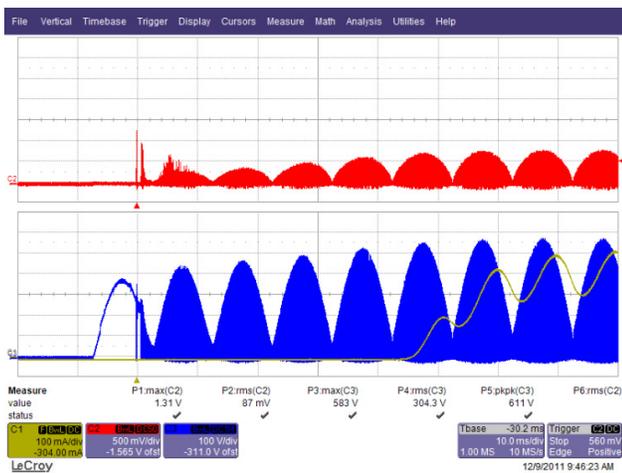


Figure 54 – Output Current rise at 265 VAC Start-up.
Upper: I_{DRAIN} , 500 mA / div.
Lower: V_{DRAIN} , 100 V, 10 ms / div.
 I_{OUT} , 100 mA, 10 ms / div.



11.11 Output Short Condition

During output short condition, the I_{FB} current falls below the $I_{FB(AR)}$ threshold and enters the auto-restart condition. During this condition, to minimize power dissipation on the power components, the auto-restart circuit turns the power supply on and off at an auto-restart duty cycle of typically DC_{AR} for as long as the fault condition persists.

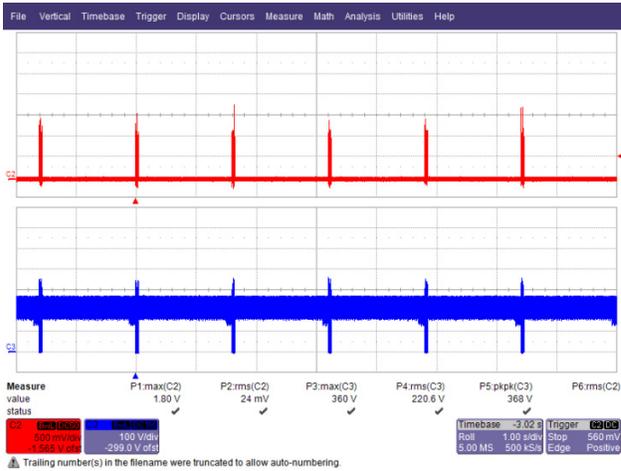


Figure 55 – 185 VAC, 50 Hz Output Short Condition.
Upper: I_{DRAIN} , 500 mA / div.
Lower: V_{DRAIN} , 100 V, 10 ms / div.

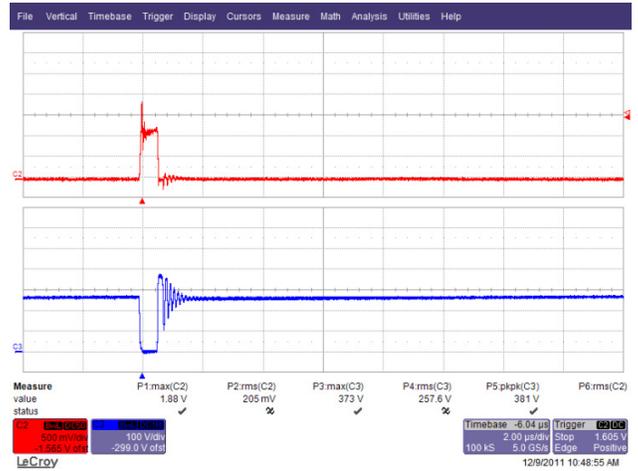


Figure 56 – 185 VAC, 50 Hz Output Short Condition.
Upper: I_{DRAIN} , 500 mA / div.
Lower: V_{DRAIN} , 100 V, 2 μ s / div.

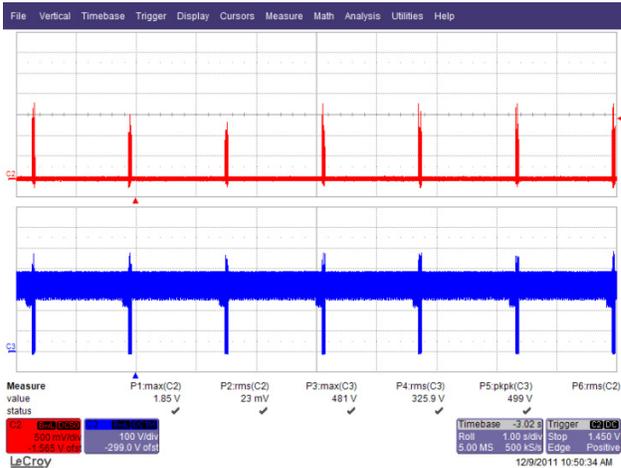


Figure 57 – 265 VAC, 50 Hz Output Short Condition.
Upper: I_{DRAIN} , 500 mA / div.
Lower: V_{DRAIN} , 100 V, 10 ms / div.

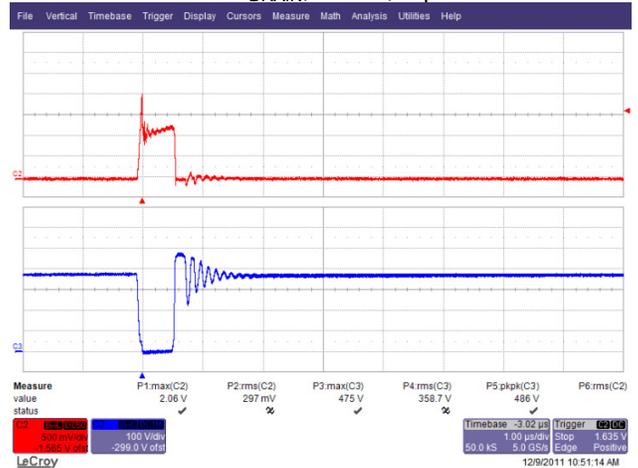


Figure 58 – 265 VAC, 50 Hz Output Short Condition.
Upper: I_{DRAIN} , 500 mA / div.
Lower: V_{DRAIN} , 100 V, 2 μ s / div.



11.12 Output Diode PIV

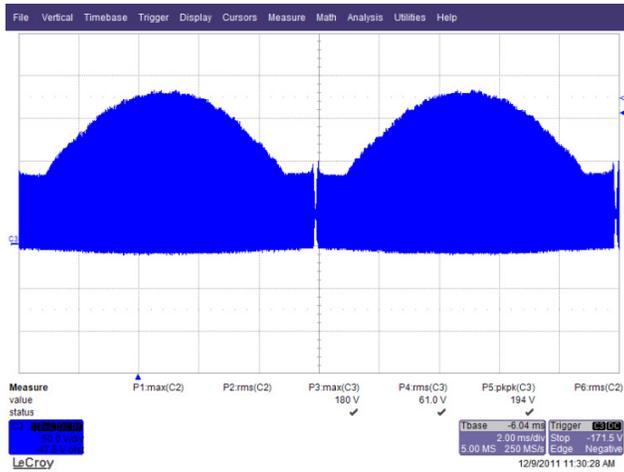


Figure 59 – 265 VAC, 50 Hz Normal Operation
 V_{RM} , 50 V / div., 2 ms / div.

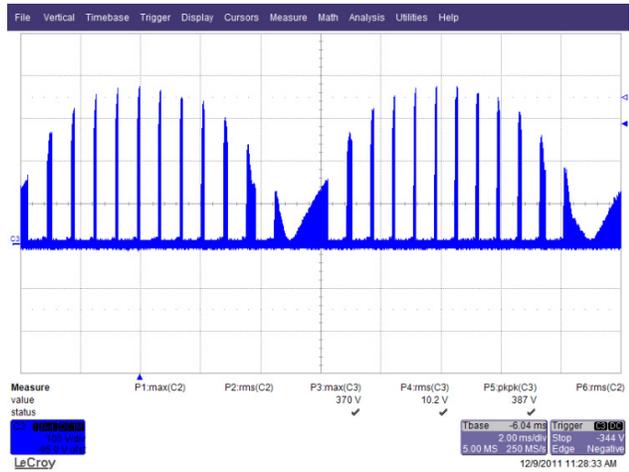


Figure 60 – 265 VAC, 50 Hz Output Short
 V_{RM} , 50 V / div., 2 ms / div.



12 Dimming Waveforms

12.1 Input Voltage and Input Current Waveforms – CLIPSAL 32E450LM

Input: 230 VAC, 50 Hz

Output: 36 V LED Load

Dimmer: Clipsal 32E450LM (Leading Edge Type)

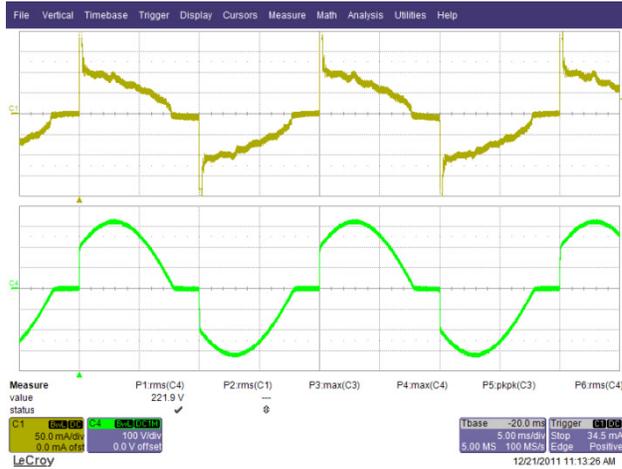


Figure 61 – 140° Conduction Angle.
Upper: I_{IN} , 50 mA / div.
Lower: V_{IN} , 100 V, 5 ms / div.

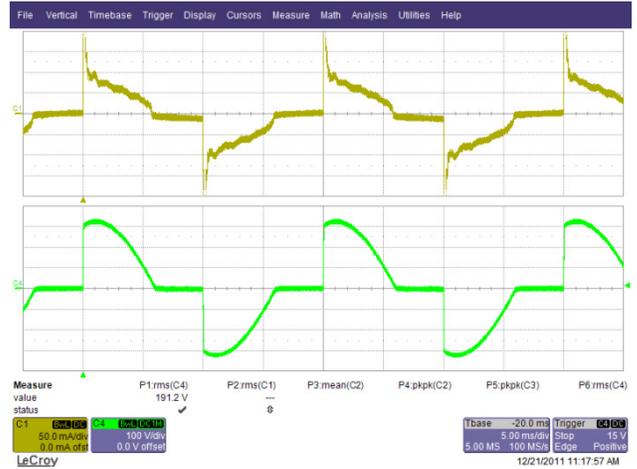


Figure 62 – 108° Conduction Angle.
Upper: I_{IN} , 50 mA / div.
Lower: V_{IN} , 100 V, 5 ms / div.

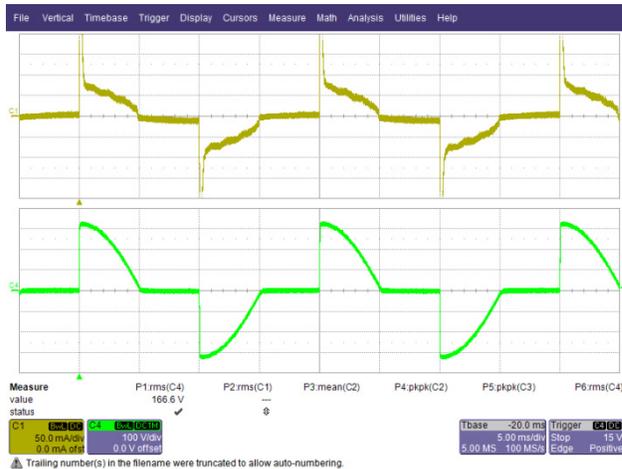


Figure 63 – 90° Conduction Angle.
Upper: I_{IN} , 50 mA / div.
Lower: V_{IN} , 100 V, 5 ms / div.



Figure 64 – 49° Conduction Angle.
Upper: I_{IN} , 50 mA / div.
Lower: V_{IN} , 100 V, 5 ms / div.



12.2 Output Current Waveforms – CLIPSAL 32E450LM

Input: 230 VAC, 50 Hz

Output: 36 V LED Load

Dimmer: Clipsal 32E450LM (Leading Edge Type)

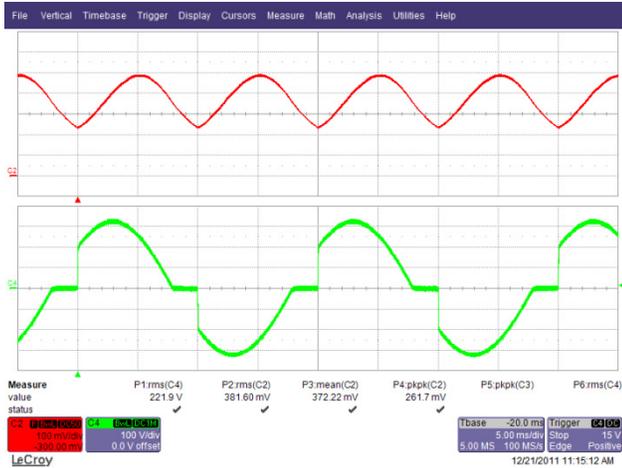


Figure 65 – 140° Conduction Angle.
 Upper: I_{OUT} , 100 mA / div.
 Lower: V_{IN} , 100 V, 5 ms / div.

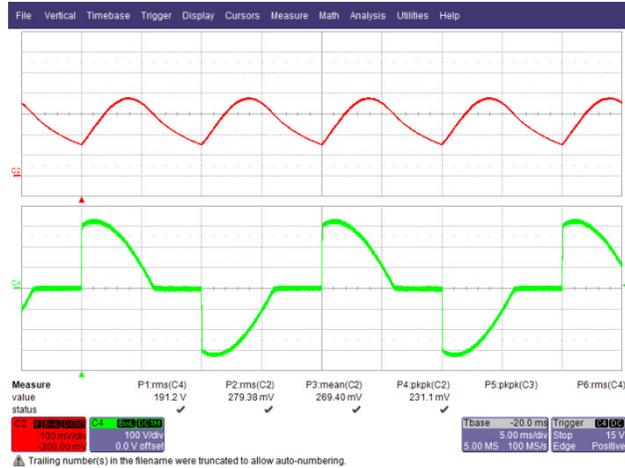


Figure 66 – 108° Conduction Angle.
 Upper: I_{OUT} , 100 mA / div.
 Lower: V_{IN} , 100 V, 5 ms / div.

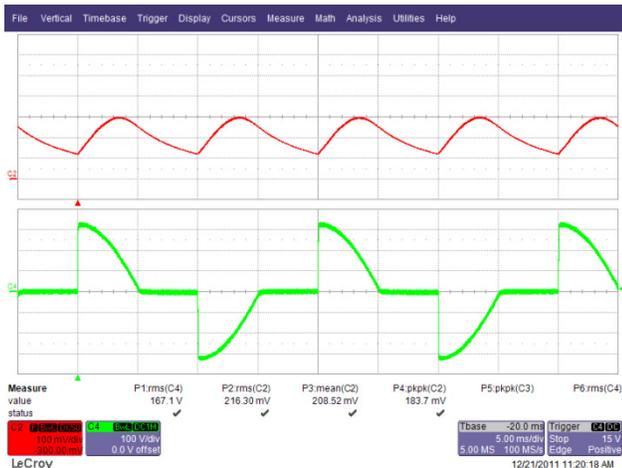


Figure 67 – 90° Conduction Angle.
 Upper: I_{OUT} , 100 mA / div.
 Lower: V_{IN} , 100 V, 5 ms / div.



Figure 68 – 49° Conduction Angle.
 Upper: I_{OUT} , 20 mA / div.
 Lower: V_{IN} , 100 V, 5 ms / div.



12.3 Input Voltage and Input Current Waveforms – CLIPSAL 32E450TM

Input: 230 VAC, 50 Hz

Output: 36 V LED Load

Dimmer: Clipsal 32E450TM (Trailing Edge Type)

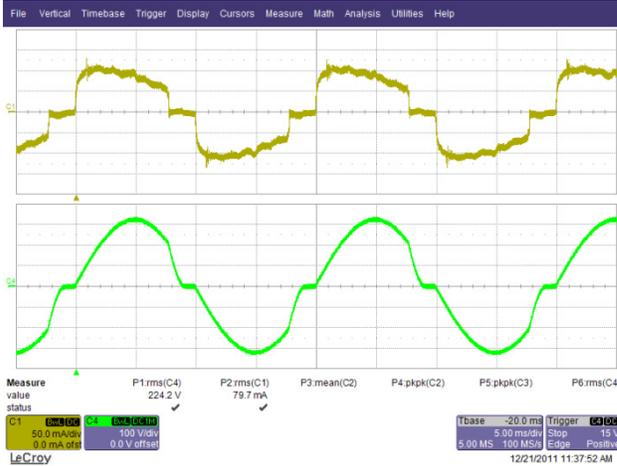


Figure 69 – 140° Conduction Angle.
 Upper: I_{IN} , 50 mA / div.
 Lower: V_{IN} , 100 V, 5 ms / div.



Figure 70 – 108° Conduction Angle.
 Upper: I_{IN} , 50 mA / div.
 Lower: V_{IN} , 100 V, 5 ms / div.

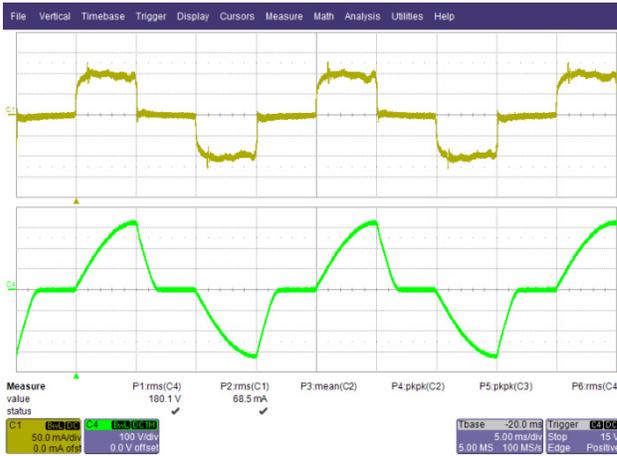


Figure 71 – 90° Conduction Angle.
 Upper: I_{IN} , 50 mA / div.
 Lower: V_{IN} , 100 V, 5 ms / div.



Figure 72 – 42° Conduction Angle.
 Upper: I_{IN} , 50 mA / div.
 Lower: V_{IN} , 100 V, 5 ms / div.



12.4 Output Current Waveforms – CLIPSAL 32E450TM

Input: 230 VAC, 50 Hz

Output: 36 V LED Load

Dimmer: Clipsal 32E450TM (Trailing Edge Type)

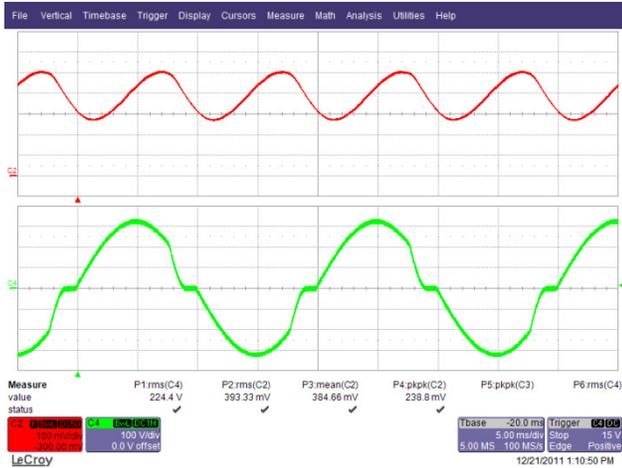


Figure 73 – 140° Conduction Angle.
 Upper: I_{OUT} , 100 mA / div.
 Lower: V_{IN} , 100 V, 5 ms / div.

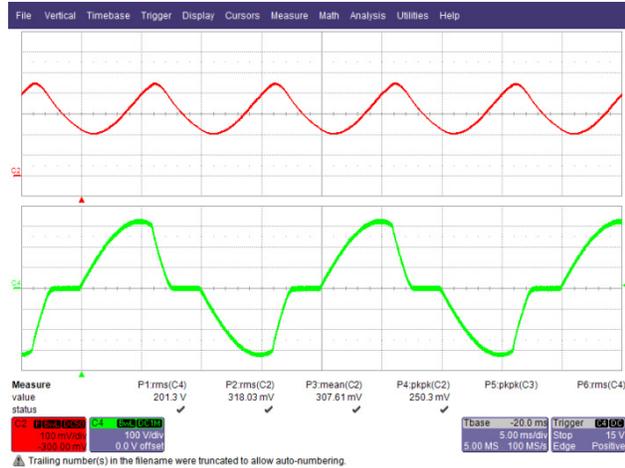


Figure 74 – 108° Conduction Angle.
 Upper: I_{OUT} , 100 mA / div.
 Lower: V_{IN} , 100 V, 5 ms / div.

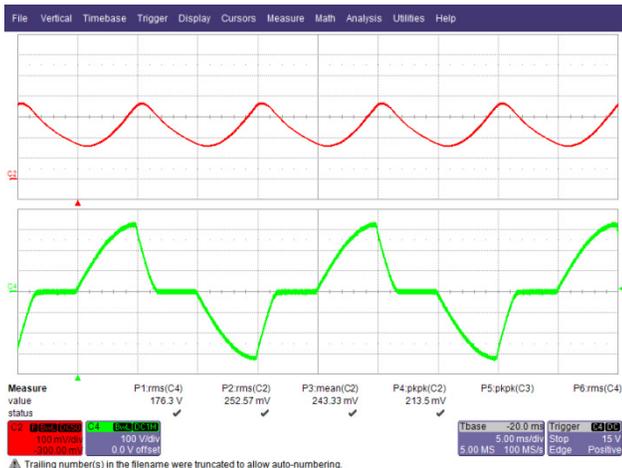


Figure 75 – 90° Conduction Angle.
 Upper: I_{OUT} , 100 mA / div.
 Lower: V_{IN} , 100 V, 5 ms / div.

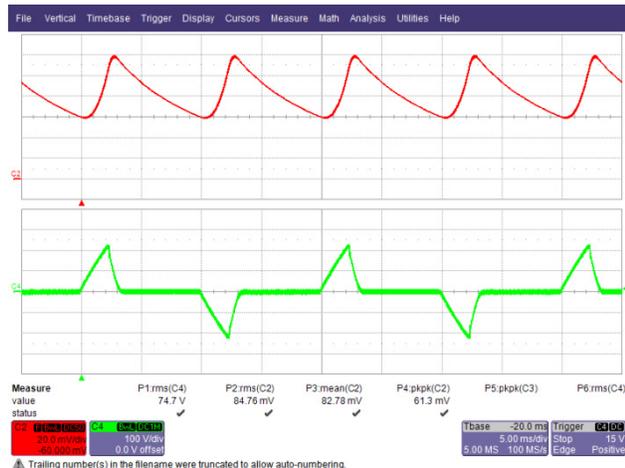


Figure 76 – 42° Conduction Angle.
 Upper: I_{OUT} , 20 mA / div.
 Lower: V_{IN} , 100 V, 5 ms / div.



13 Conducted EMI

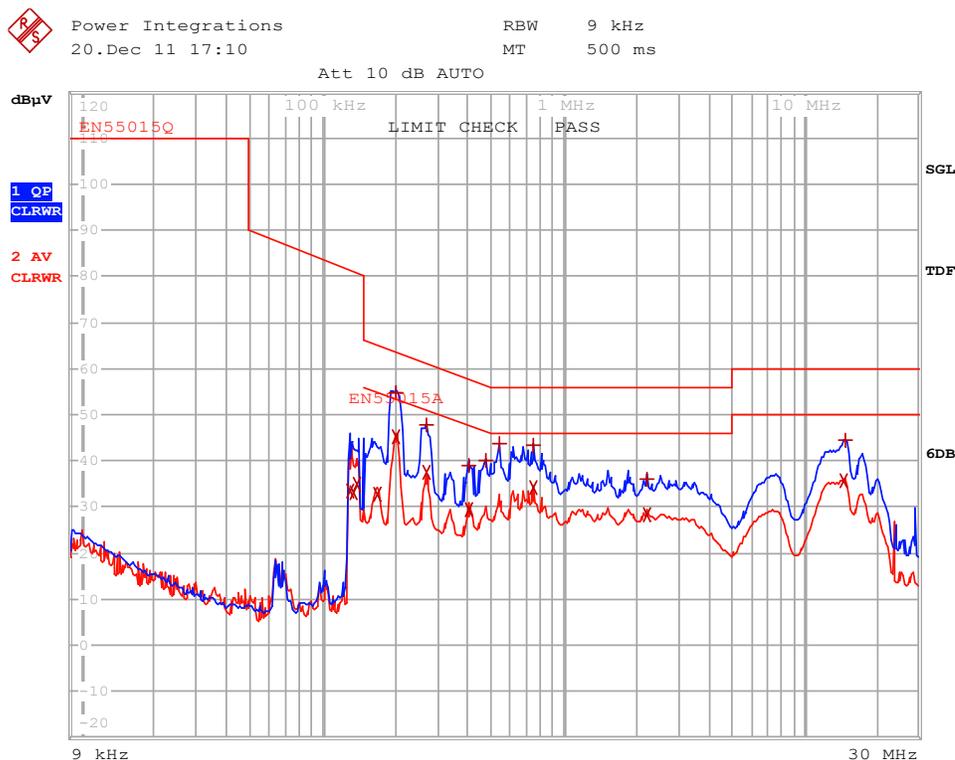
13.1 Test Set-up

The unit was tested using LED load ($\sim 36\text{ V } V_{\text{OUT}}$) with input voltage of 230 VAC, 60 Hz at room temperature.



Figure 77 – EMI Test Set-up with the Unit and LED Load Placed Inside the Cone.

13.2 Test Result



EDIT PEAK LIST (Final Measurement Results)

Trace1: EN55015Q
Trace2: EN55015A
Trace3: ---

| TRACE | FREQUENCY | LEVEL dBµV | DELTA LIMIT dB |
|--------------|-------------------|------------|----------------|
| 2 Average | 129.530094744 kHz | 33.58 | I1 gnd |
| 2 Average | 133.454986145 kHz | 33.20 | N gnd |
| 2 Average | 138.873793737 kHz | 34.80 | I1 gnd |
| 2 Average | 169.02375452 kHz | 32.68 | I1 gnd |
| 1 Quasi Peak | 202.1773373 kHz | 54.91 | I1 gnd |
| 2 Average | 202.1773373 kHz | 45.18 | I1 gnd |
| 1 Quasi Peak | 269.806440381 kHz | 47.88 | I1 gnd |
| 2 Average | 269.806440381 kHz | 37.64 | I1 gnd |
| 1 Quasi Peak | 405.722074413 kHz | 39.02 | I1 gnd |
| 2 Average | 405.722074413 kHz | 29.44 | I1 gnd |
| 1 Quasi Peak | 471.030732902 kHz | 39.96 | I1 gnd |
| 1 Quasi Peak | 541.437681113 kHz | 43.79 | I1 gnd |
| 1 Quasi Peak | 744.444692652 kHz | 43.23 | I1 gnd |
| 2 Average | 744.444692652 kHz | 34.01 | I1 gnd |
| 1 Quasi Peak | 2.20222749414 MHz | 36.09 | I1 gnd |
| 2 Average | 2.20222749414 MHz | 28.47 | I1 gnd |
| 2 Average | 14.5855630539 MHz | 35.82 | I1 gnd |
| 1 Quasi Peak | 14.8787328713 MHz | 44.44 | I1 gnd |

Figure 78 – Conducted EMI, 36 V LED Load, 230 VAC, 60 Hz, and EN55015 B Limits.



14 Line Surge

The unit was subjected to ± 2500 V 100 kHz ring wave and ± 500 V Differential Surge at 230 VAC using 10 strikes at each condition. A test failure was defined as a non-recoverable interruption of output requiring supply repair or recycling of input voltage.

| Level (V) | Input Voltage (VAC) | Injection Location | Injection Phase (°) | Type | Test Result (Pass/Fail) |
|-----------|---------------------|--------------------|---------------------|---------------------------|-------------------------|
| +2500 | 230 | L1, L2 | 0 | 100 kHz Ring Wave (500 A) | Pass |
| -2500 | 230 | L1, L2 | 0 | 100 kHz Ring Wave (500 A) | Pass |
| +2500 | 230 | L1, L2 | 90 | 100 kHz Ring Wave (500 A) | Pass |
| -2500 | 230 | L1, L2 | 90 | 100 kHz Ring Wave (500 A) | Pass |

| Level (V) | Input Voltage (VAC) | Injection Location | Injection Phase (°) | Type | Test Result (Pass/Fail) |
|-----------|---------------------|--------------------|---------------------|---------------------|-------------------------|
| +500 | 230 | L1, L2 | 0 | Surge (2 Ω) | Pass |
| -500 | 230 | L1, L2 | 0 | Surge (2 Ω) | Pass |
| +500 | 230 | L1, L2 | 90 | Surge (2 Ω) | Pass |
| -500 | 230 | L1, L2 | 90 | Surge (2 Ω) | Pass |

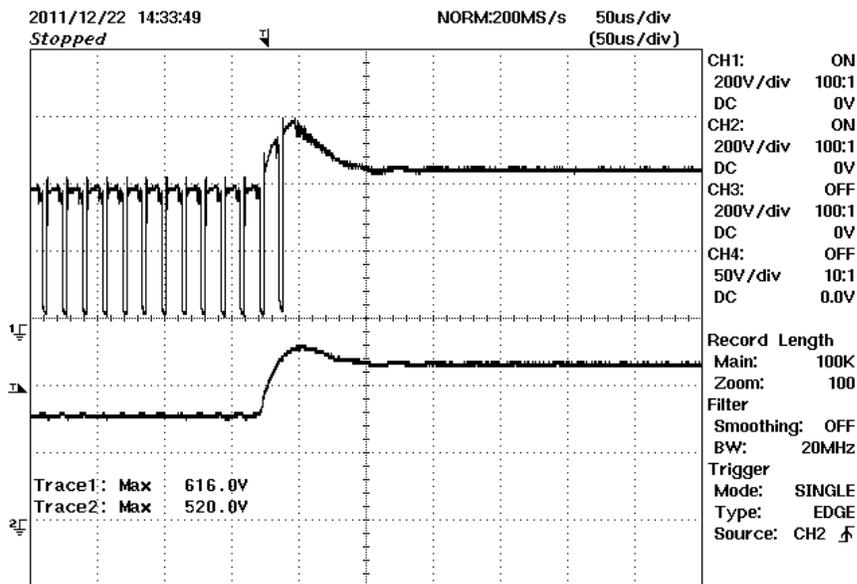


Figure 79 – 500 V Differential Line Surge at 90° Injection Phase without TVS VR1.
CH1: U1 VDS (<650 V); CH2: C6 Voltage.



For improved surge performance or higher surge margin requirement, TVS VR1 can be added.

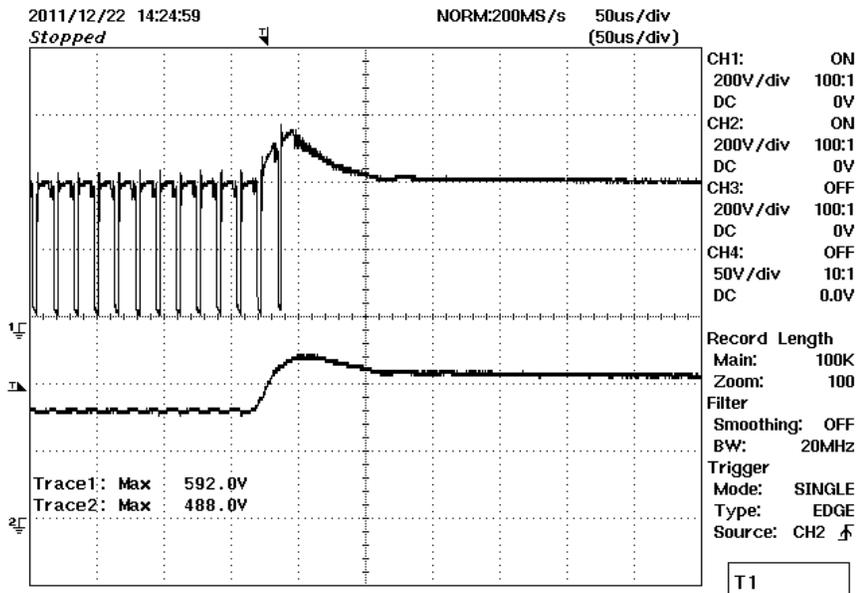


Figure 80 – 500 V Differential Line Surge at 90° Injection Phase with TVS VR1.
CH1: U1 VDS (<600 V); CH2: C6 Voltage.



15 Revision History

| Date | Author | Revision | Description and Changes | Reviewed |
|-------------|---------------|-----------------|--------------------------------|-----------------|
| 26-Jan-12 | CA | 1.0 | Initial Release | Apps & Mktg |
| 21-Mar-12 | AS | 1.1 | Text Edits | |
| | | | | |
| | | | | |



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