



Design Example Report

| | |
|------------------------|--|
| Title | 12 W Non-Dimmable, Non-Isolated Buck LED Driver Using LYTSwitch™-0 LYT0006P/D |
| Specification | 190 VAC – 265 VAC Input; 85 V _{NOM} , 135 mA Output |
| Application | T8 Tube Lamp Replacement |
| Author | Applications Engineering Department |
| Document Number | DER-384 |
| Date | October 8, 2013 |
| Revision | 1.0 |

Summary and Features

- Combined single-stage high power factor (>0.7 at 230 VAC) with accurate constant current (CC) output
- Low cost, low component count and small PCB footprint solution
- Highly energy efficient, >90% across input
- Fast start-up time (<100 ms) – no perceptible delay
- Integrated protection and reliability features
 - Single shot no-load protection
 - Output short-circuit protection with auto-recovery
 - Auto-recovering hysteretic thermal shutdown protects both components and PCB
 - No damage during brown-out
- Meets IEC ring wave, differential line surge and EN55015 conducted EMI

PATENT INFORMATION

The products and applications illustrated herein (including transformer construction and circuits external to the products) may be covered by one or more U.S. and foreign patents, or potentially by pending U.S. and foreign patent applications assigned to Power Integrations. A complete list of Power Integrations' patents may be found at www.powerint.com. Power Integrations grants its customers a license under certain patent rights as set forth at <<http://www.powerint.com/ip.htm>>.

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Important Note:

Although this board is designed to satisfy safety isolation requirements, the engineering prototype has not been agency approved. Therefore, all testing should be performed using an isolation transformer to provide the AC input to the prototype board.



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1 Introduction

This document describes a cost effective power supply utilizing the LYTSwitch™-0 family (LYT0006D) in a highly compact buck topology.

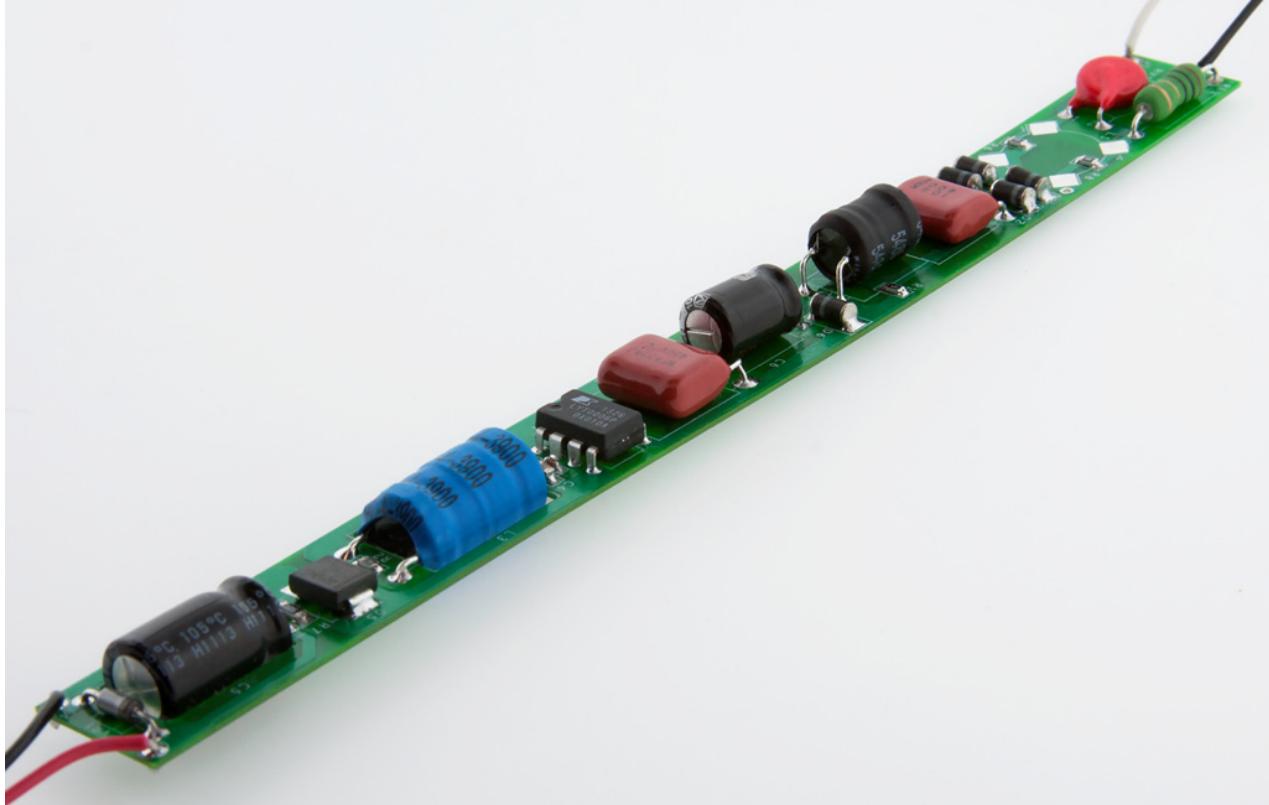


Figure 1 – Populated Circuit Board.

This power supply operates over an input voltage range of 190 VAC to 265 VAC. The DC bus voltage is high enough to support 85 V output when using a buck topology. In a buck converter the output voltage must always be lower than the input voltage. The output voltage is also limited by the maximum duty cycle of the LYTSwitch-0, which also requires the input voltage to be larger than the output voltage.

The reference design is not limited for LED tube or ballast lamp application; due to its simplicity the design layout can be easily modified for retrofit lamp applications.



Figure 2 – Populated Circuit Board, P Package, Top.





Figure 3 – Populated Circuit Board, P Package, Bottom.



Figure 4 – Populated Circuit Board, D Package, Top.



Figure 5 – Populated Circuit Board, D Package, Bottom.

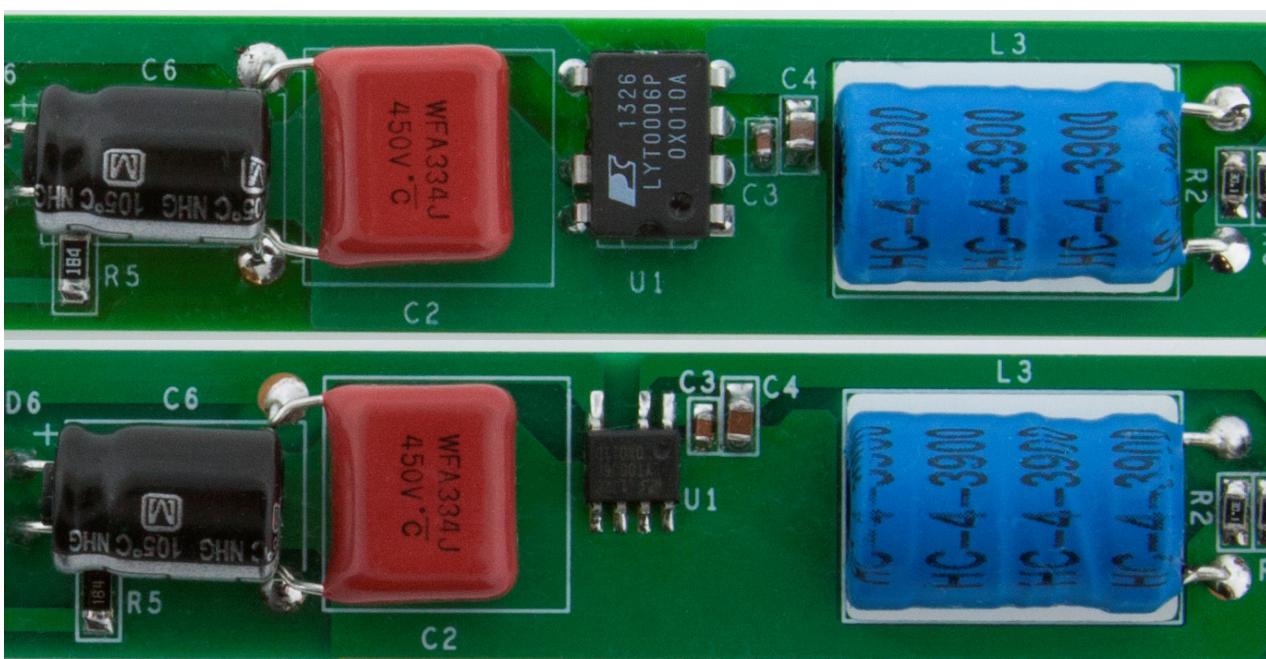


Figure 6 – There are 2 Possible LYTSwitch-0 Package Options for this Application - Only Difference is the Temperature Rise, P Package being Lower by 5 °C.



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2 Power Supply Specification

The table below represents the minimum acceptable performance of the design. Actual performance is listed in the results section.

| Description | Symbol | Min | Typ | Max | Units | Comment |
|---------------------------|------------|-----|-------|-----|-------|--|
| Input | | | | | | |
| Voltage Operation | V_{IN} | 190 | | 265 | VAC | 2 Wire – no P.E. |
| Frequency | f_{LINE} | 47 | 50/60 | | Hz | Operating frequency is not limited. Adjust sense resistor if application is for 400 Hz line. |
| Output | | | | | | |
| Output Voltage | V_{OUT} | 83 | 85 | 88 | V | |
| Output Current | I_{OUT} | | 135 | | mA | $\pm 4\%$ at 200 VAC - 240 VAC |
| Total Output Power | | | | | | |
| Continuous Output Power | P_{OUT} | | | 12 | W | |
| Efficiency | | | | | | |
| 240 VAC; 85 V LED | η | 90 | | | % | Measured at P_{OUT} , 25 °C |
| Power Factor | | | | | | |
| 240 VAC; 85 V LED | PF | 0.7 | | | | Measured at P_{OUT} , 25 °C |
| Environmental | | | | | | |
| Conducted EMI | | | | | | Meets CISPR22B / EN55015B |
| Line Surge | | | | | | 1.2/50 μ s surge, IEC 1000-4-5, Series Impedance: Differential Mode: 2 Ω |
| Differential Mode (L1-L2) | | | 1 | | kV | |
| Ring Wave (100 kHz) | | | | | | 500 A short circuit |
| Differential Mode (L1-L2) | | | 2.5 | | kV | Series Impedance: Differential Mode: 2 Ω |



3 Schematic

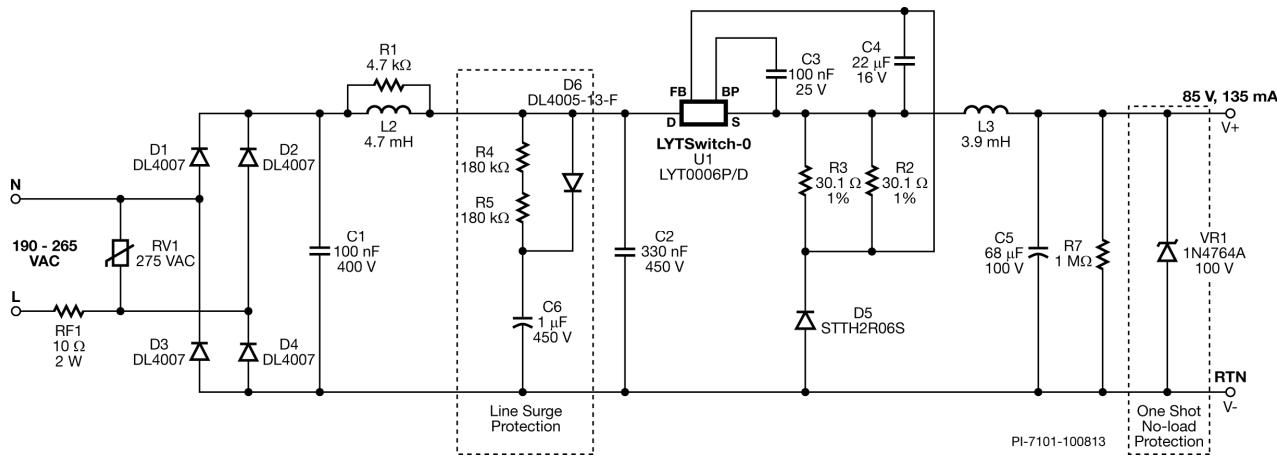


Figure 7 – Schematic.

Note: Zener diode VR1 is optional and provides one-time no-load protection. Refer to AN-60 for additional OVP options.



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4 Circuit Description

The power supply shown in Figure 7 uses the LYT0006P (U1) in a high-side buck configuration to deliver a constant 135 mA current at an output voltage of 85 VDC. The power supply is designed for driving LEDs, which should always be driven with a constant current (CC) supply.

4.1 Input EMI Filtering

Fuse RF1 provides short circuit protection. Diodes D1, D2, D3 and D4 form a full bridge for full wave rectification for good power factor. Four single diodes were used in the layout instead of a single package to equally distribute power losses (heat) and to reduce cost. Capacitor C1, C2 and differential-mode choke L2 form a π filter in order to meet conducted EMI standards. Capacitor C1 and C2 are also used for energy storage reducing line noise and protecting against line surge. There is a provision for an additional common-mode choke (L1) on the board in case more inductance is required to meet system EMI requirements.

For differential line surge of 1 kV and above, RCD (C6, D6, R4 and R5) circuit and MOV (RV1) are used to clamp the surge energy from the line. For surge requirement 2 kV and above, replace RF1 by a normal fuse with high I^2t rating. Remove the RCD circuit for 500 V differential line surge. A differential line surge of 2.5 kV will only require RV1 to protect the AC rectifier.

The reference design filter is optimized to achieve high PF. Through the proper combination and optimization of π filter and output voltage, 0.7 PF at nominal input is achieved.

4.2 LYTSwitch-0

LYTSwitch-0 is optimized to design a simple and cost effective LED driver with tight line and temperature regulation from 0 to 100 °C (LYTSwitch-0 case temperature). The PIXIs spreadsheet was used to achieve the best line regulation by balancing the power inductor and the sense resistor. The total input capacitance was optimized to deliver the highest possible power factor, by minimizing the distortion in input current and spreading the input current across the entire AC cycle.

The LYTSwitch-0 family has a built-in thermal limit to protect the power supply in case the tube is subjected to an excessive operating temperature.

The buck converter stage consists of the integrated power MOSFET switch within LYT0006D (U1), a freewheeling diode D5, sense resistors (R2, R3), power inductor L3 and output capacitor C5. The converter is operating mostly in Continuous Mode (CM) in order to deliver the desired output current. A fast freewheeling diode was selected to minimize the switching losses.



A standard off the shelf inductor is used in the power converter for low cost design.

Decreasing the capacitance of output capacitor (C5) does not limit the driver operation. In fact, C5 can be removed for direct drive application, where low output current ripple is required.

4.3 Output Rectification

Power inductor is operating mostly in continuous mode for this power level, a fast output diode (D5) was used to minimize reverse current ($t_{RR} < 35 \text{ nS}$ is recommended) to achieve high efficiency and low thermal operation.

4.4 Output Feedback

Regulation is maintained by skipping switching cycles. As the output current rises, the voltage into the FEEDBACK (FB) pin also rises. If this voltage exceeds V_{FB} then subsequent switching cycles will be skipped until the voltage reduces below V_{FB} . Output current is sensed from R2, R3 and filtered by C4, then fed to the FB pin and compared to an internal reference for accurate regulation. The key to achieving good line regulation is in balancing the power inductor and sense resistor values after the minimum inductance has been calculated. This can be done through the PIXIs design spreadsheet.

The bypass capacitor (C4) is connected between the FB pin and the SOURCE (S) pin and helps reduce power loss during output current sensing. The capacitor acts to sample-and-hold the feedback current information for the FB pin. No limiting resistor is required between the FB pin and C4, because the peak voltage will not exceed the maximum rating of the device.

4.5 No-Load Protection

An optional, one shot, no-load protection circuit is incorporated into the design. In case of accidental no-load operation, the output capacitor is protected by VR1. Zener diode VR1 would need to be replaced after a failure. Refer to AN-60 for other OVP options.

In the real operation (LED retrofit lamp) the load is always connected VR1 is not necessary and can be removed to save cost. For accidental load disconnect especially during board level testing during manufacturing, a 70 VAC can be applied to the input initially and the output current measured to determine whether the load is connected or not. This test will allow safe, non-destructive initial power up of the board, without the need for an OV protection circuit.



5 PCB Layout

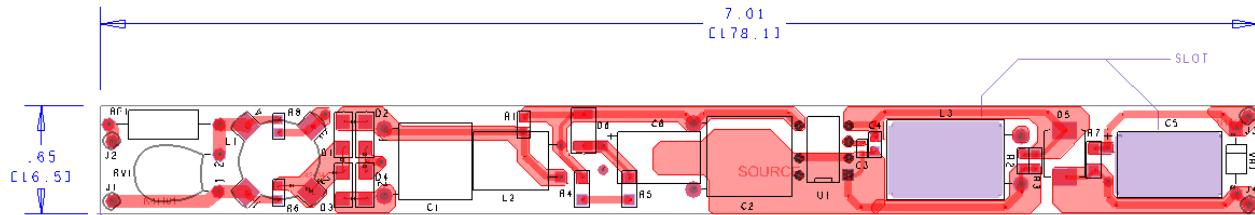


Figure 8 – Printed Circuit Layout for DIP-8 P Package. Top View.

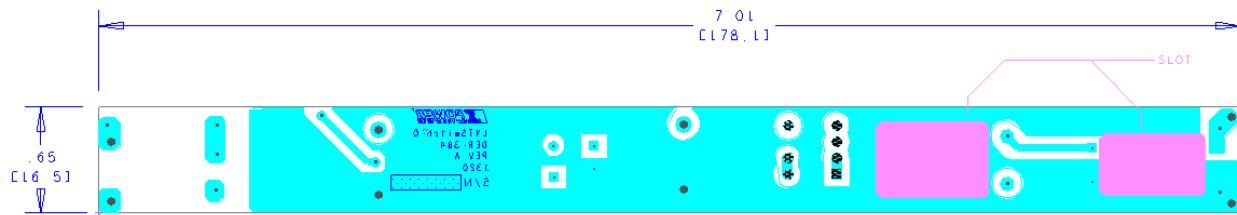


Figure 9 – Printed Circuit Layout for P Package. Bottom View.

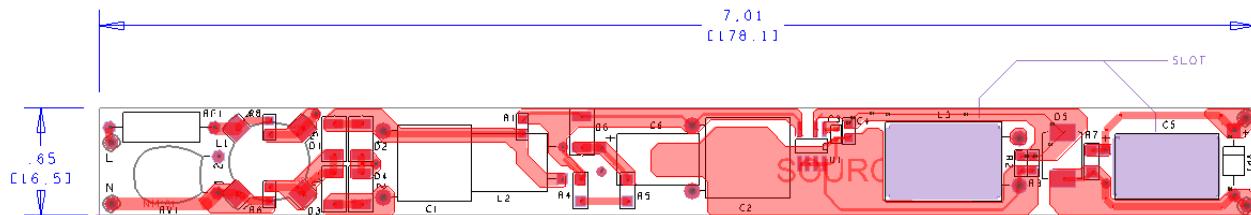


Figure 10 – Printed Circuit Layout for SO-8 D Package. Top View.

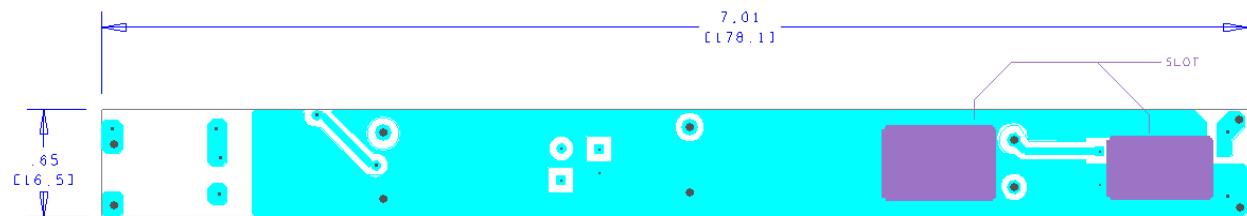


Figure 11 – Printed Circuit Layout for D Package. Bottom View.

6 Bill of Materials

| Item | Qty | Ref Des | Description | Manufacturer P/N | Manufacturer |
|-------------------|-----|----------------|---|------------------|--------------------|
| Electrical | | | | | |
| 1 | 1 | C1 | 100 nF, 400 V, Film | ECQ-E4104KF | Panasonic |
| 2 | 1 | C2 | 330 nF, 450 V, METALPOLYPRO | ECW-F2W334JAQ | Panasonic |
| 3 | 1 | C3 | 100 nF, 25 V, Ceramic, X7R, 0603 | VJ0603Y104KNXAO | Vishay |
| 4 | 1 | C4 | 22 μ F, 16 V, Ceramic, X7R, 0805 | C2012X5R1C226K | TDK |
| 5 | 1 | C5 | 68 μ F, 100 V, Electrolytic, Gen. Purpose, (10 x 16) | UHE2A680MPD | Nichicon |
| 6 | 1 | C6 | 1.0 μ F, 450 V, Electrolytic, NHG, (8 x 11.5) | ECA-2WHG010 | Panasonic |
| 7 | 4 | D1 D2 D3 D4 | 1000 V, 1 A, Rectifier, Glass Passivated, DO-213AA (MELF) | DL4007-13-F | Diodes, Inc. |
| 8 | 1 | D5 | DIODE ULTRA FAST 600 V 2 A HE SMC, DO-214AB | STTH2R06S | ST Micro |
| 9 | 1 | D6 | 600 V, 1 A, Rectifier, Glass Passivated, DO-213AA (MELF) | DL4005-13-F | Diodes, Inc. |
| 10 | 1 | L2 | 4.7 mH, 0.150 A, 20% | RL-5480-3-4700 | Renco Elect |
| 11 | 1 | L3 | 3.9 mH, 0.250 A, 20% | RL-5480HC-4-3900 | Renco Elect |
| 12 | 1 | R1 | 4.7 k Ω , 5%, 1/8 W, Thick Film, 0805 | ERJ-6GEYJ472V | Panasonic |
| 13 | 2 | R2 R3 | 31/8 Ω , 1%, 1/8 W, Thick Film, 0805 | ERJ-6ENF30R1V | Panasonic |
| 14 | 2 | R4 R5 | 180 k Ω , 5%, 1/4 W, Thick Film, 1206 | ERJ-8GEYJ184V | Panasonic |
| 15 | 1 | R7 | 1 M Ω , 5%, 1/4 W, Thick Film, 1206 | ERJ-8GEYJ105V | Panasonic |
| 16 | 1 | RF1 | 10 Ω , 5%, 2 W, Wirewound, Fusible | FW20A10R0JA | Bourns |
| 17 | 1 | RV1 | 275 V, 23 J, 7 mm, RADIAL | V275LA4P | Littlefuse |
| 18 | 1 | U1 | LYTSwitch-0, DIP-8B | LYT0006P/D | Power Integrations |
| 19 | 1 | VR1 | 100 V, 5%, 1 W, DO-41 | 1N4764A-TAP | Vishay |
| Mechanical | | | | | |
| 16 | 1 | WIRE (V-) | Wire, UL1007, #24 AWG, Blk, PVC, 4" | 1007-24/7-0 | Anixter |
| 17 | 1 | WIRE (L) | Wire, UL1007, #24 AWG, Blu, PVC, 4" | 1007-24/7-6 | Anixter |
| 18 | 1 | WIRE (V+) | Wire, UL1007, #24 AWG, Red, PVC, 4" | 1007-24/7-2 | Anixter |
| 19 | 1 | WIRE (N) | Wire, UL1007, #24 AWG, Wht, PVC, 4" | 1007-24/7-9 | Anixter |
| 20 | 1 | PCB | FR4, 0.31, 1 Oz Cu (0.65" X 7.0") | | |



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7 Inductor Design Spreadsheet

| ACDC_LYTSwitchZero_052813; Rev.0.8; Copyright Power Integrations 2013 | INPUT | INFO | OUTPUT | UNIT | LYTSwitchZero_Rev_0-8.xls: LYTSwitchZero Design Spreadsheet |
|---|---------------|------|---------------|--------|--|
| INPUT VARIABLES | | | | | |
| VACMIN | 190 | | 190 | Volts | Minimum AC Input Voltage |
| VACNOM | 230 | | 230 | | |
| VACMAX | 265 | | 265 | Volts | Maximum AC Input Voltage |
| FL | 50 | | 50 | Hertz | Line Frequency |
| VO | 85 | | 85 | Volts | Output Voltage |
| IO | 135 | | 135 | mA | Output Current |
| Pout | | | 11.5 | W | |
| EFFICIENCY | 0.90 | | 0.90 | | Overall Efficiency Estimate (Adjust to match Calculated, or enter Measured Efficiency) |
| CIN | 0.43 | | 0.43 | uF | Input Filter Capacitor |
| DC INPUT VARIABLES | | | | | |
| VMIN | | | 85.70624 | Volts | Minimum DC Bus Voltage |
| VMAX | | | 374.7666 | Volts | |
| LYTSwitchZero | | | | | |
| LYTSwitchZero | LYT0006 | | LYT0006 | | |
| ILIMIT | | | 0.375 | Amps | Typical Current Limit |
| ILIMIT_MIN | | | 0.33275 | Amps | Minimum Current Limit |
| ILIMIT_MAX | | | 0.401 | Amps | Maximum Current Limit |
| FSMIN | | | 62000 | Hertz | Minimum Switching Frequency |
| IRMS | | | 110.4053 | mA | Expected RMS current through LYTswitch |
| VDS | | | 4.8375 | Volts | Maximum On-State Drain To Source Voltage drop |
| DIODE | | | | | |
| VD | | | 0.7 | Volts | Freewheeling Diode Forward Voltage Drop |
| VRR | | | 400 | Volts | Recommended PIV rating of Freewheeling Diode |
| IF | | | 1 | Amps | Recommended Diode Continuous Current Rating |
| Diode Recommendation | | | BYV26C | | Suggested Freewheeling Diode |
| OUTPUT INDUCTOR | | | | | |
| Core type | Off-the-Shelf | | Off-the-Shelf | | Select core type between Ferrite and Off-the-Shelf |
| Core size | | | | | Select core size |
| Custom Core | | | | | Enter custom core description (if used) |
| AE | | | N/A | mm^2 | Core Effective Cross Sectional Area |
| LE | | | N/A | mm | Core Effective Path Length |
| AL | | | N/A | nH/T^2 | Ungapped Core Effective Inductance |
| BW | | | N/A | mm | Bobbin Physical Winding Width |
| NL | | | N/A | | Number of turns on inductor |
| BP | | | N/A | Gauss | Peak flux density |
| LG | | | N/A | mm | Gap length |
| OD | | | N/A | | Maximum Primary Wire Diameter including insulation |
| INS | | | N/A | | Estimated Total Insulation Thickness (= 2 * film thickness) |
| DIA | | | N/A | | Bare conductor diameter |
| AWG | | | N/A | | Primary Wire Gauge (Rounded to next smaller standard AWG value) |



| | | | | | |
|----------------------------|-------|--|----------|------|--|
| CM | | | N/A | | Bare conductor effective area in circular mils |
| CMA | | | N/A | | !!! INCREASE CMA > 200 (increase L(primary layers),decrease NS, use larger Core) |
| L | | | N/A | | |
| LP | 3510 | | 3510 | uH | Output Inductor, Recommended Standard Value |
| IO_Average | | | 135.7396 | mA | Average output current |
| ILRMS | | | 174.5175 | mA | Estimated RMS inductor current (at VMAX) |
| FEEDBACK COMPONENTS | | | | | |
| RFB | 15.05 | | 15.05 | Ohms | Feedback Resistor. Use closest standard 1% value |
| CFB | | | 22 | uF | Feedback Capacitor |
| OUTPUT REGULATION | | | | | |
| IO_VACMIN | | | 135.7396 | mA | Output Current at VACMIN |
| IO_VACNOM | | | 136.7358 | mA | Output Current at VACNOM |
| IO_VACMAX | | | 135.3795 | mA | Output Current at VACMAX |



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8 Performance Data

All measurements performed at room temperature ($\approx 25^{\circ}\text{C}$) otherwise specified.

| Input | | Input Measurement | | | LED Load Measurement | | | Regulation (%) | Efficiency (%) |
|--------------------------------|--------------|--|---|------------------------|----------------------|--|---|-------------------------|----------------|
| VAC (V _{RMS}) | Freq (Hz) | V _{IN} (V _{RMS}) | I _{IN} (mA _{RMS}) | P _{IN} (W) | PF | V _{OUT} (V _{DC}) | I _{OUT} (mA _{DC}) | P _{OUT} (W) | |
| V_{OUT} Minimum | | | | | | | | | |
| 190 | 50 | 189.93 | 83.76 | 12.377 | 0.778 | 82.0 | 136.2 | 11.190 | 0.89 |
| 200 | 50 | 199.89 | 81.65 | 12.432 | 0.762 | 82.0 | 136.6 | 11.230 | 1.19 |
| 220 | 50 | 219.95 | 78.22 | 12.460 | 0.724 | 82.0 | 136.6 | 11.220 | 1.19 |
| 240 | 50 | 239.93 | 75.75 | 12.459 | 0.686 | 82.0 | 136.2 | 11.180 | 0.89 |
| 265 | 50 | 264.97 | 73.32 | 12.464 | 0.642 | 81.9 | 135.8 | 11.140 | 0.59 |
| V_{OUT} Nominal | | | | | | | | | |
| 190 | 50 | 189.95 | 84.98 | 12.777 | 0.792 | 85.0 | 135.7 | 11.580 | 0.52 |
| 200 | 50 | 199.89 | 82.94 | 12.818 | 0.773 | 85.0 | 136.1 | 11.600 | 0.81 |
| 220 | 50 | 219.95 | 79.45 | 12.924 | 0.740 | 85.1 | 136.9 | 11.670 | 1.41 |
| 240 | 50 | 239.93 | 76.78 | 12.922 | 0.701 | 85.1 | 136.5 | 11.630 | 1.11 |
| 265 | 50 | 264.97 | 74.40 | 12.930 | 0.656 | 85.1 | 136.1 | 11.590 | 0.81 |
| V_{OUT} Maximum | | | | | | | | | |
| 190 | 50 | 189.95 | 86.14 | 13.173 | 0.805 | 88.1 | 135.4 | 11.970 | 0.30 |
| 200 | 50 | 199.89 | 84.04 | 13.230 | 0.788 | 88.1 | 135.8 | 12.000 | 0.59 |
| 220 | 50 | 219.95 | 80.51 | 13.307 | 0.752 | 88.2 | 136.3 | 12.050 | 0.96 |
| 240 | 50 | 239.93 | 77.84 | 13.391 | 0.717 | 88.2 | 136.7 | 12.080 | 1.26 |
| 265 | 50 | 264.97 | 75.55 | 13.417 | 0.670 | 88.2 | 136.4 | 12.050 | 1.04 |

Table 1 – Test Data from the UUT.



8.1 Active Mode Efficiency

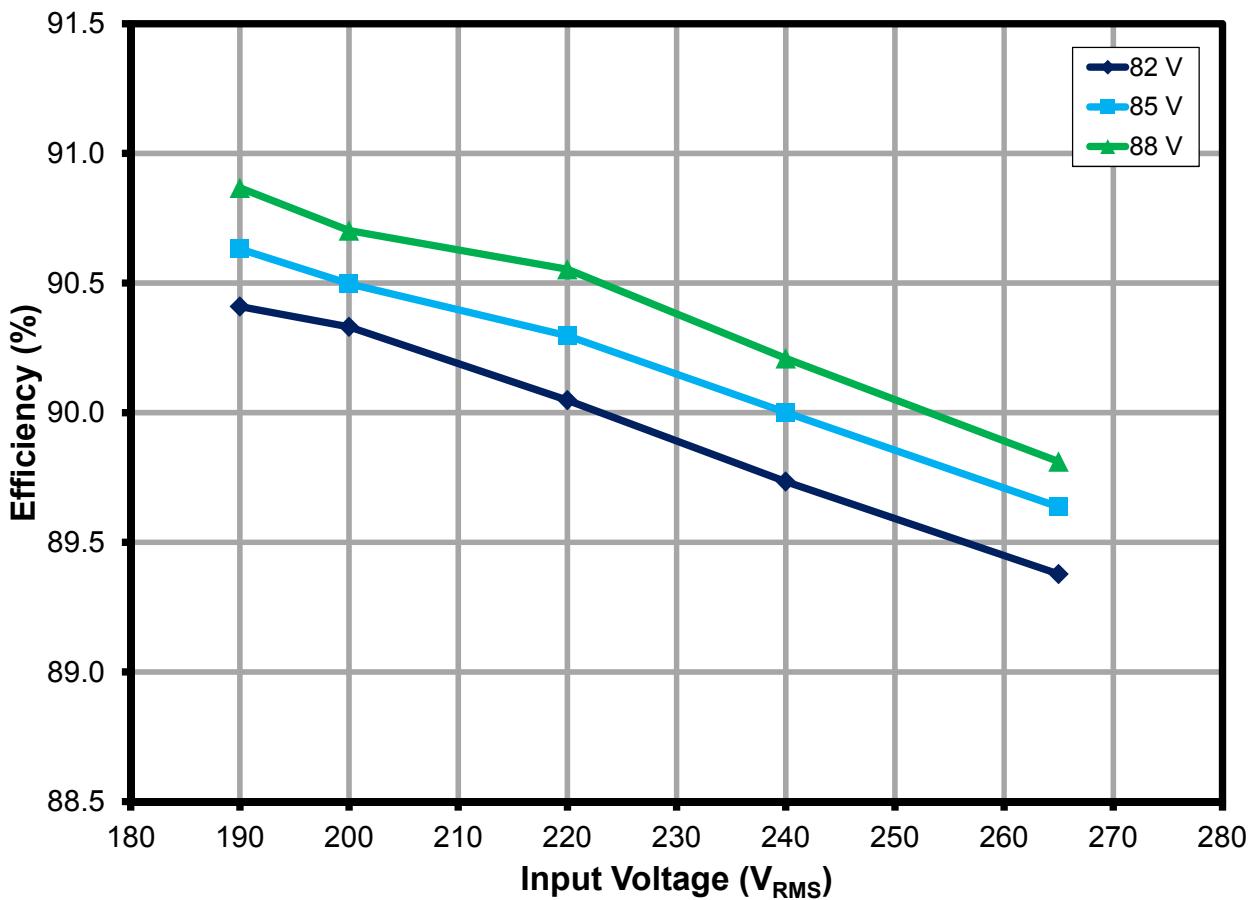


Figure 12 – Efficiency with Respect to AC Input Voltage 190-265 VAC (60 Hz) Input.



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8.2 Output Current Regulation

8.2.1 Output Current Regulation Across Line and Load

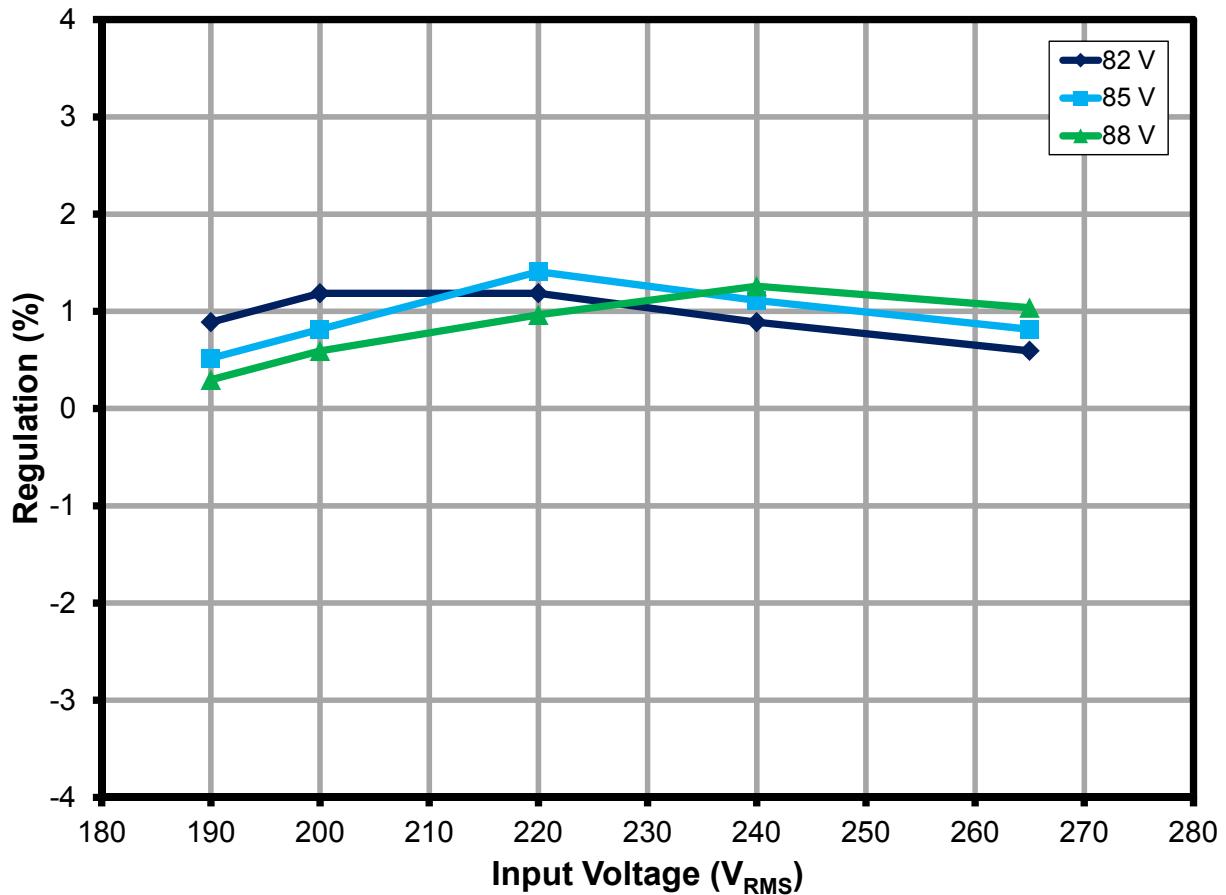


Figure 13 – Load Regulation, Room Temperature.



8.3 Load Regulation

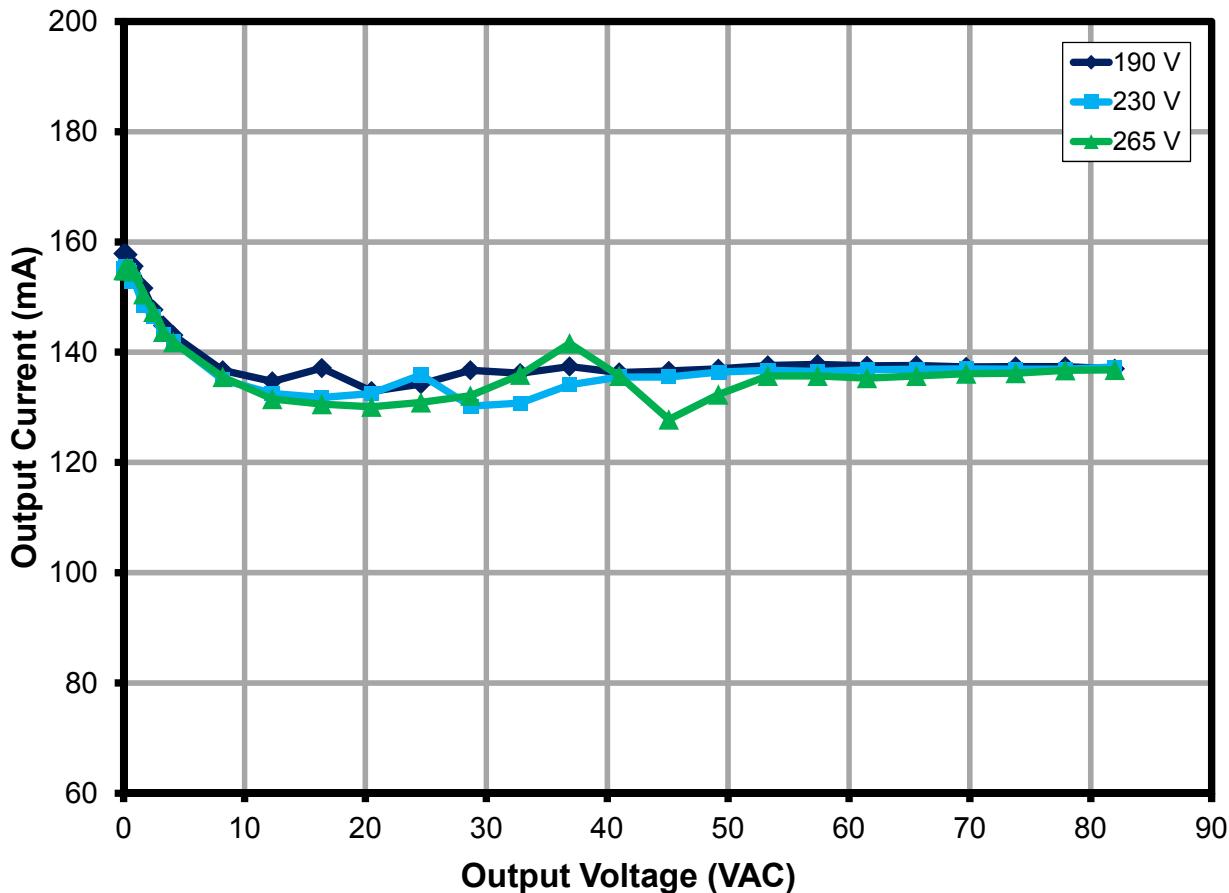


Figure 14 – Load Regulation at 190 V, 230 V and 265 V. The Design Can Operate in a Wide Operating Output Voltage.



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8.4 Power Factor

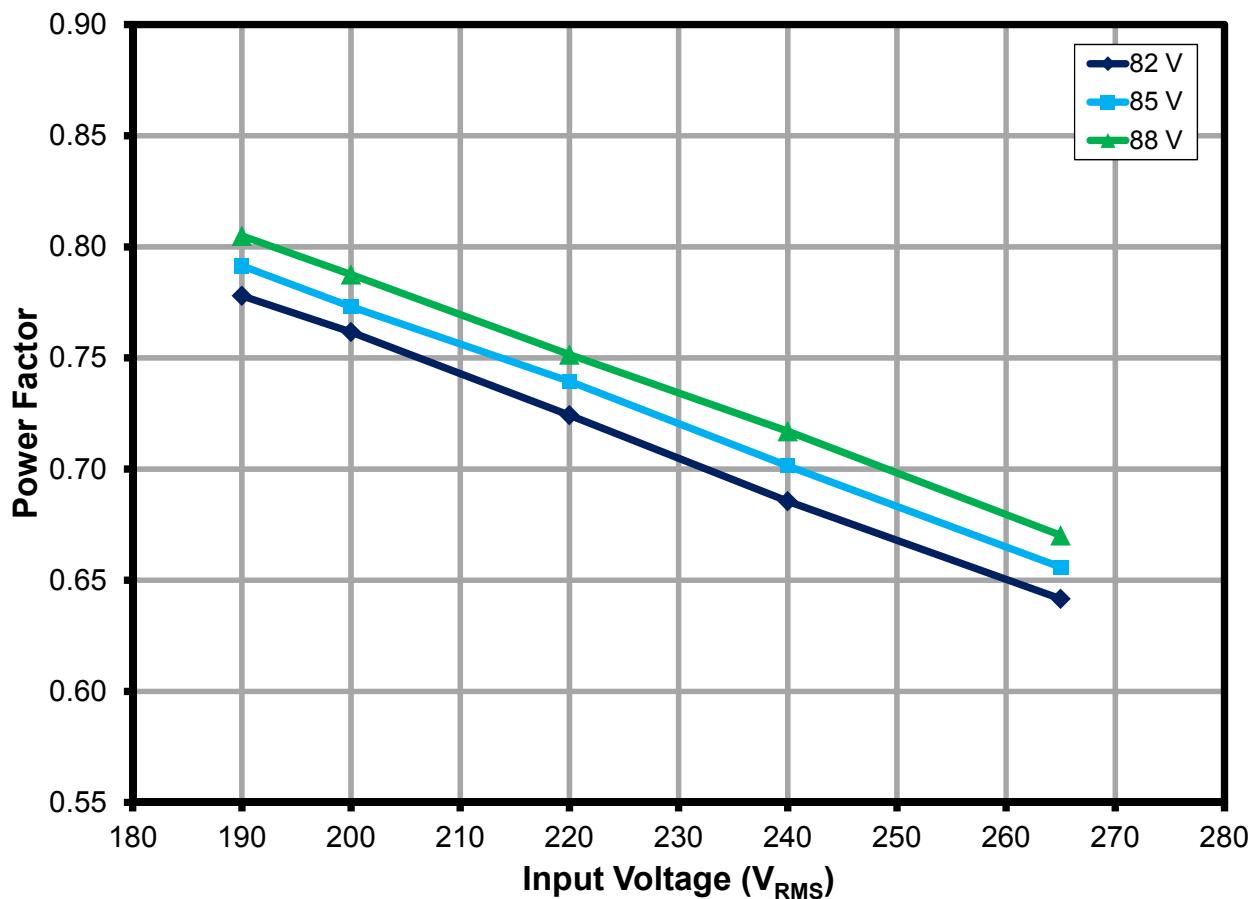


Figure 15 – Power Factor Performance at Different LED Voltage.



9 Thermal Performance

9.1 Equipment Used

| | | | |
|------------|---|--------------|--|
| AC Source: | Chroma Programmable AC Source Model No: 6415 | Wattmeter: | Yokogawa Power Meter Model No: WT2000 |
| | | Data Logger: | Agilent |

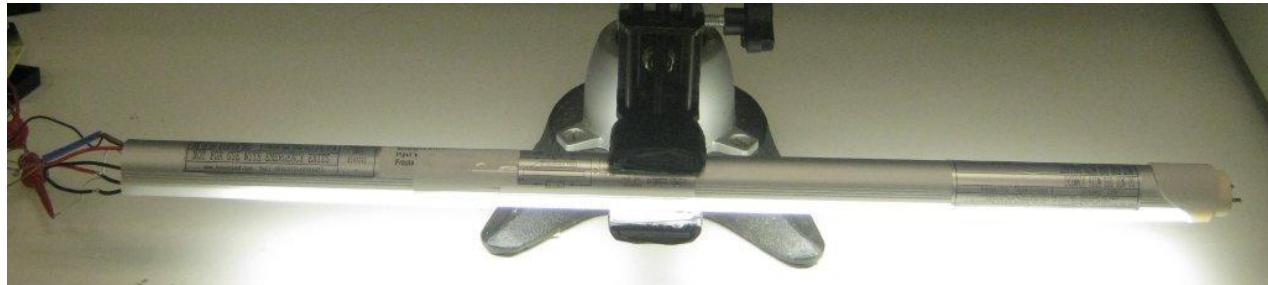


Figure 16 – LED Driver Inserted in a T8, 2 ft. Tube for Thermal Evaluation.

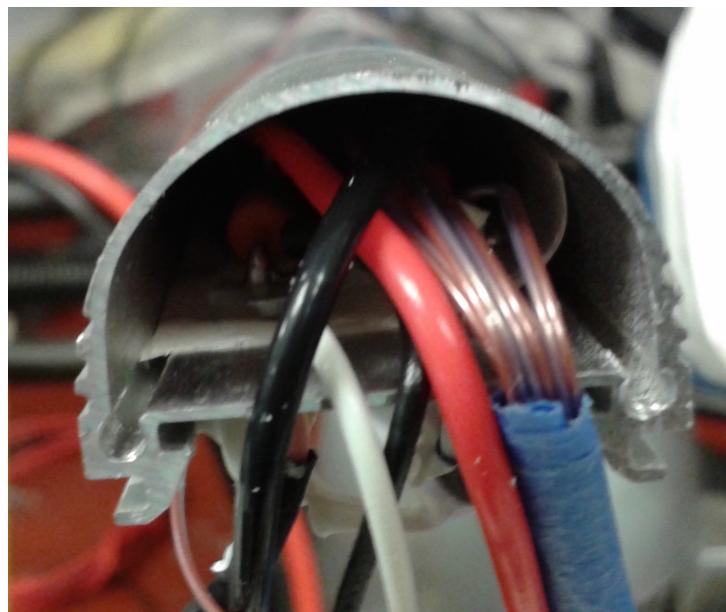


Figure 17 – LED Driver Thermal Unit Fitted Inside a T8 Tube Housing.

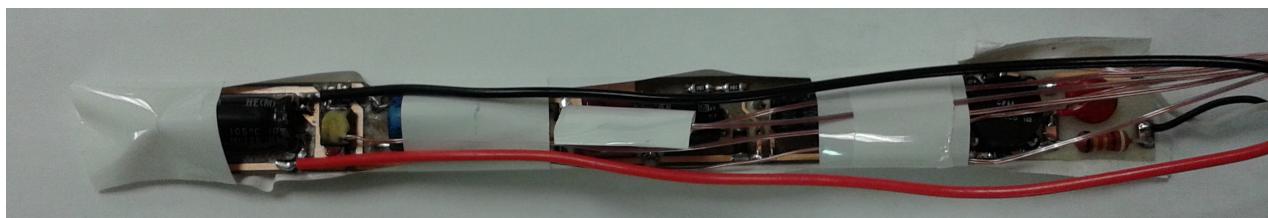


Figure 18 – Thermal Unit with Thermocouple Set-up.



9.2 Thermal Results

Input: 190 V / 50 Hz

Load: 85 V / 135 m A LED load.

| Device Location | Unit | Measurement |
|---------------------|------|-------------|
| External Ambient | °C | 36.8 |
| Internal Ambient | °C | 42.7 |
| Bridge (D2) | °C | 50.0 |
| LYT0006P/D (U1) | °C | 49.0 |
| Power Inductor (L2) | °C | 44.0 |
| Output Diode (D5) | °C | 50.0 |

Table 2 – Thermal Measurement.



9.3 Thermal Scan

Open-frame thermal measurement at 25 °C ambient. UUT was soaked for 1 hour to achieve steady-state before the measurement.

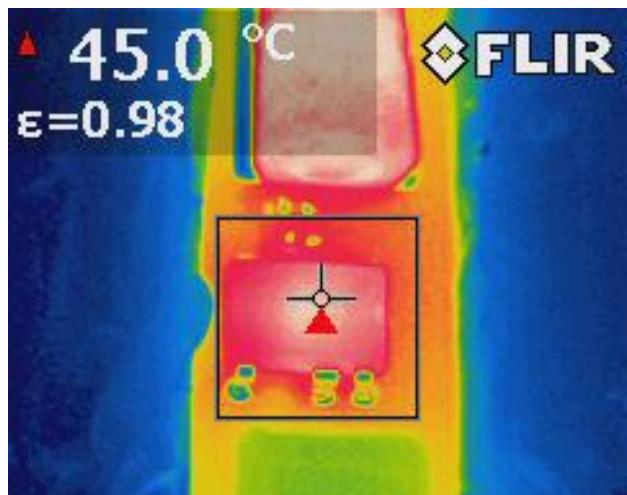


Figure 19 – LYT0006P Device Temperature (°C).



Figure 20 – LYT0006D Device Temperature (°C).

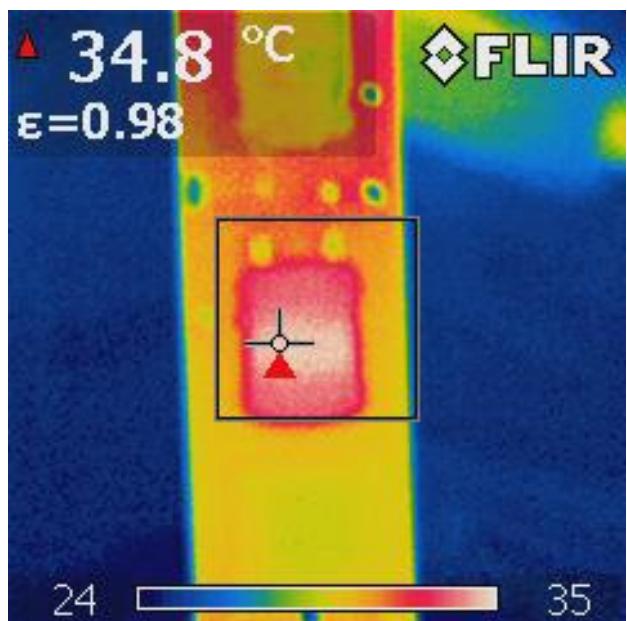


Figure 21 – EMI Choke; L1 Temperature (°C).

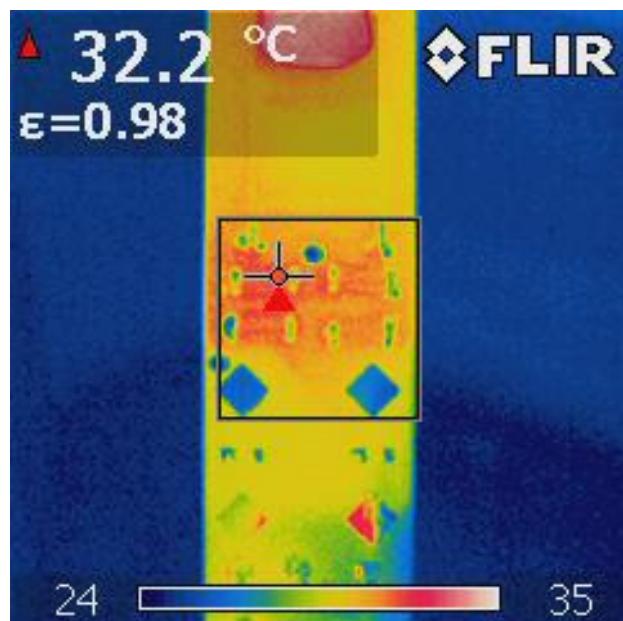


Figure 22 – D1 Temperature (°C).



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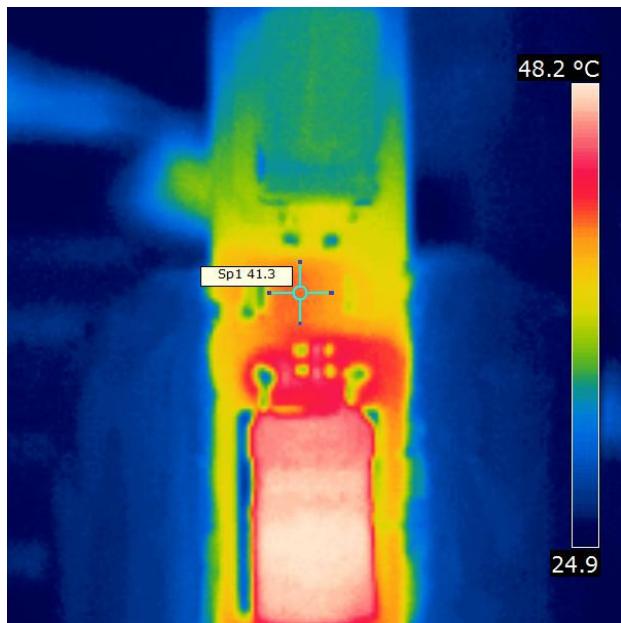


Figure 23 – D5 Freewheeling Diode Temperature (°C)

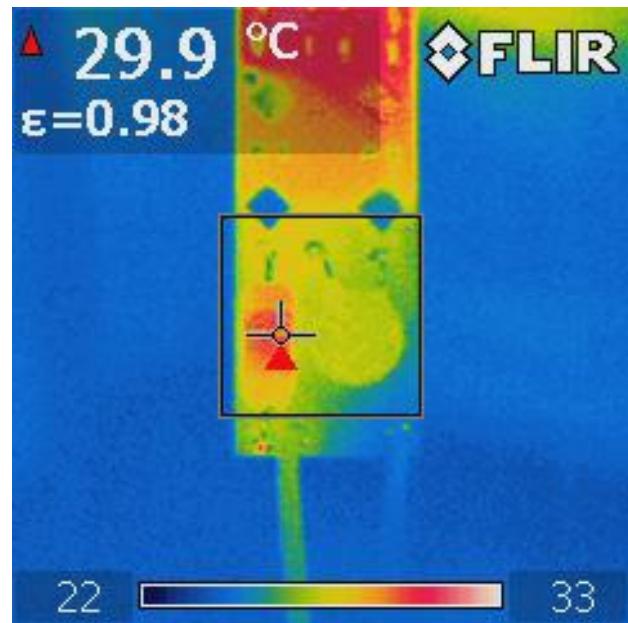


Figure 24 – Temperature (°C) at Bottom Side of PCB.

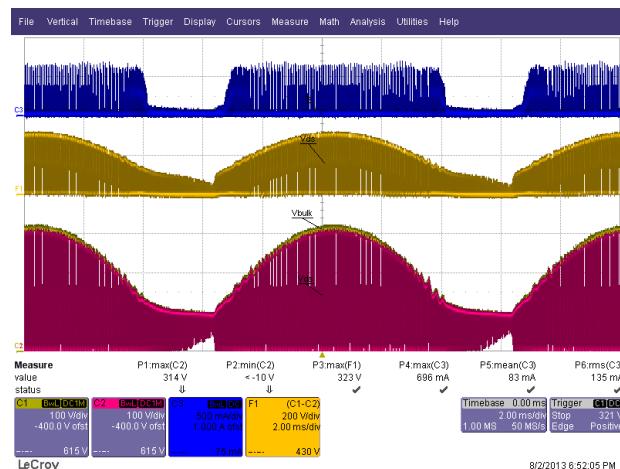
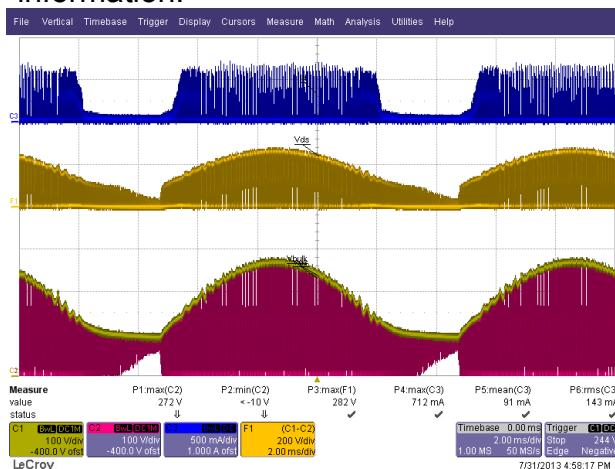


10 Waveforms

10.1 Drain Voltage, Current Normal Operation

Skipped cycles are normal as they are the mode used to regulate the output current. These skipped cycles will occur every time the voltage drop on sense resistor (R_2 , R_3) reaches 1.65 V. The unit will enter into auto-restart if there is not at least one missing pulse within 50 ms.

In some designs with high power inductance and operating mostly in CCM, a reverse current may be present. This can be avoided by increasing the device size, increasing the input capacitance, or adding a drain blocking diode. See AN-60 for more additional information.



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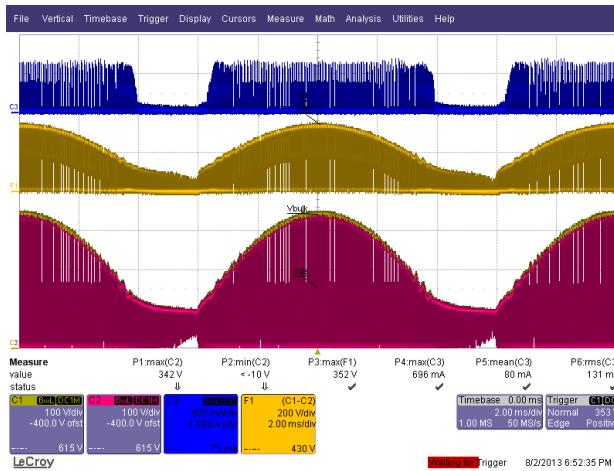


Figure 27 – 240 VAC, 50 Hz, Nominal V_{LED} Load.

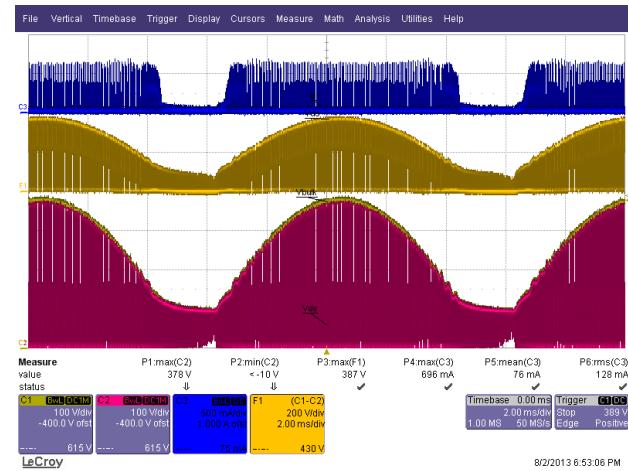


Figure 28 – 265 VAC, 50 Hz, Nominal V_{LED} Load.

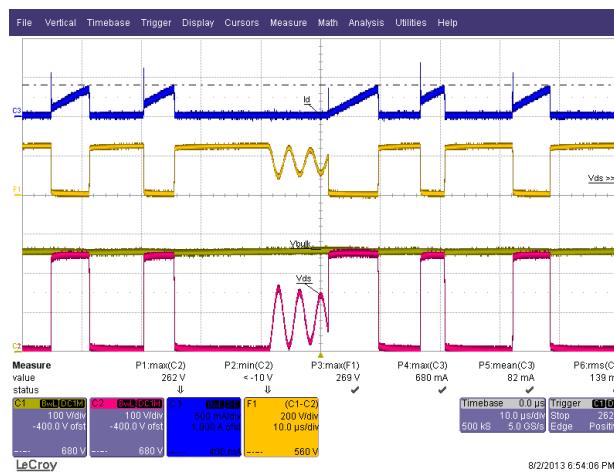
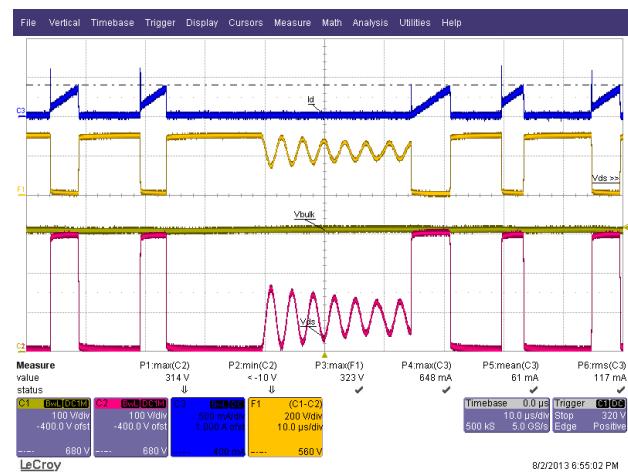
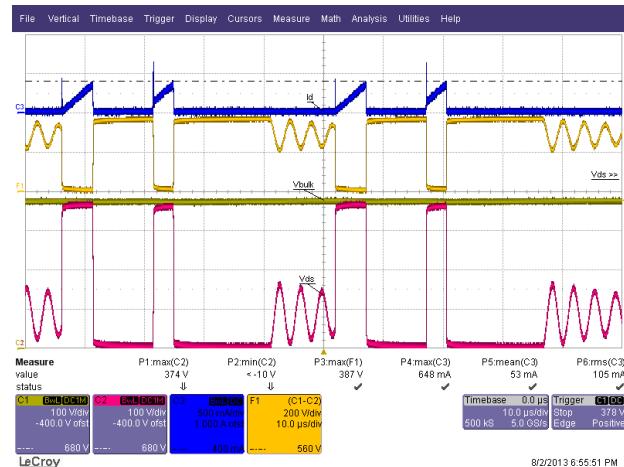
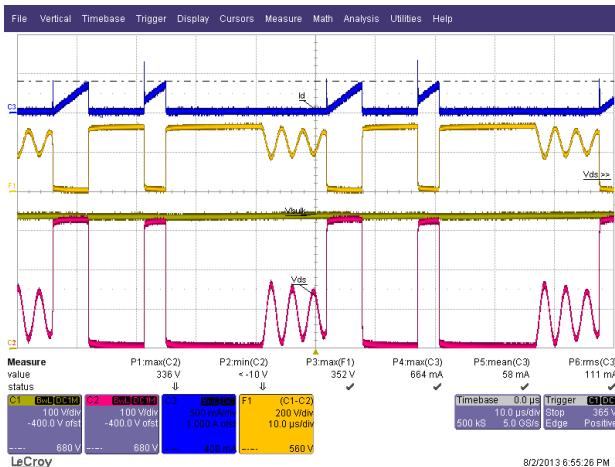


Figure 29 – 190 VAC, 50 Hz, Nominal V_{LED} Load.



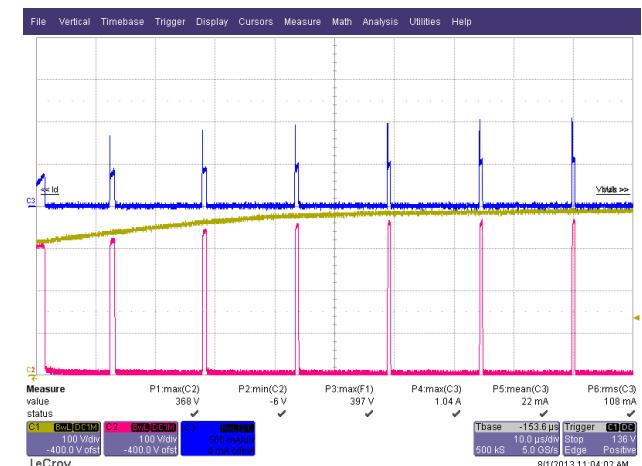
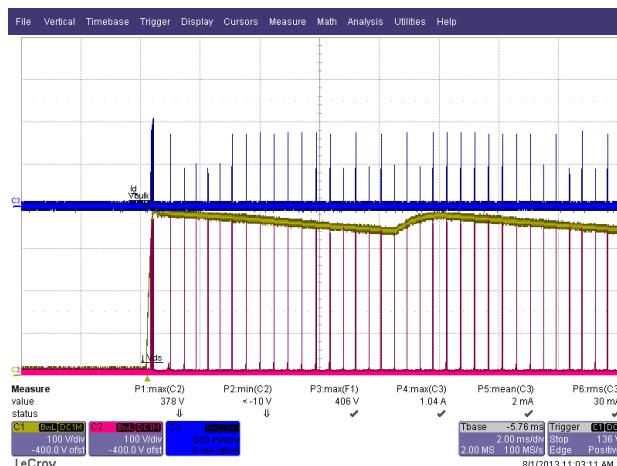
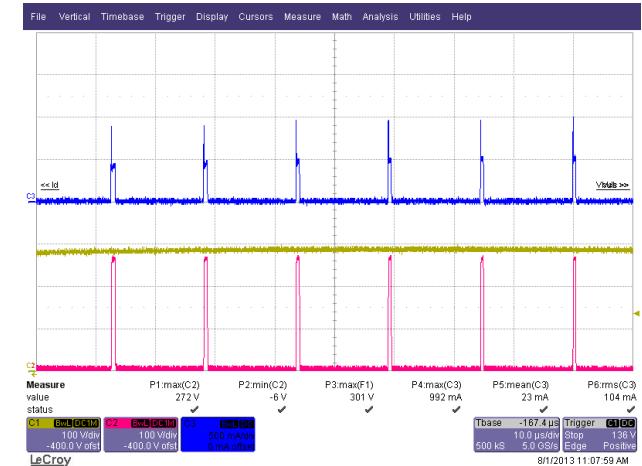


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10.2 Drain Voltage and Current When Output Short

Device is operating within range, no inductor saturation was observed.



10.3 Drain Voltage and Current Start-up Profile

Device is operating within range, no inductor saturation was observed.

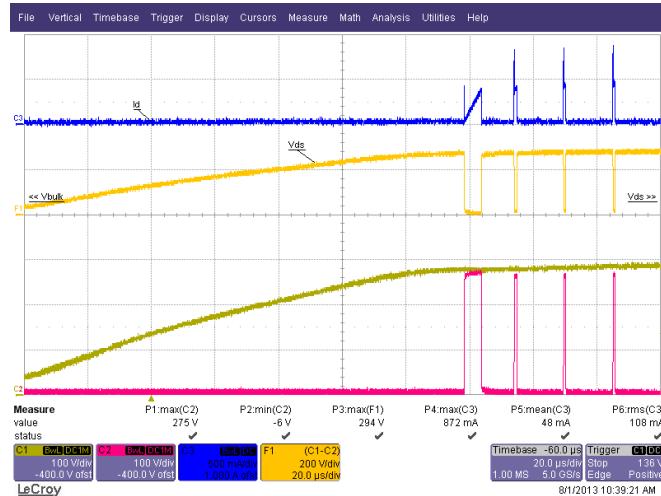
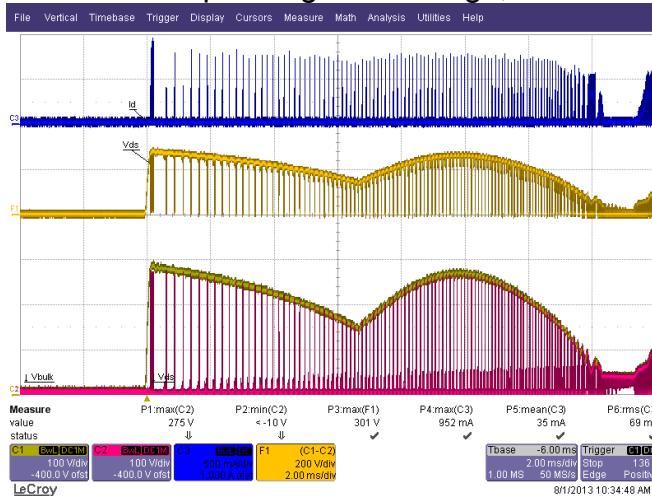


Figure 37 – 190 VAC / 50 Hz Start-up.
Ch1: V_{BULK} , 100 V / div.
Ch2: V_{S-G} , 100 V / div.
Ch3: I_{DRAIN} , 0.5 A / div.
F1: V_{D-S} , 200 V / div.
Time Scale: 2 ms / div.

Figure 38 – 190 VAC / 50 Hz Start-up.
Ch1: V_{BULK} , 100 V / div.
Ch2: V_{S-G} , 100 V / div.
Ch3: I_{DRAIN} , 0.5 A / div.
F1: V_{D-S} , 200 V / div.
Time Scale: 20 μ s / div.

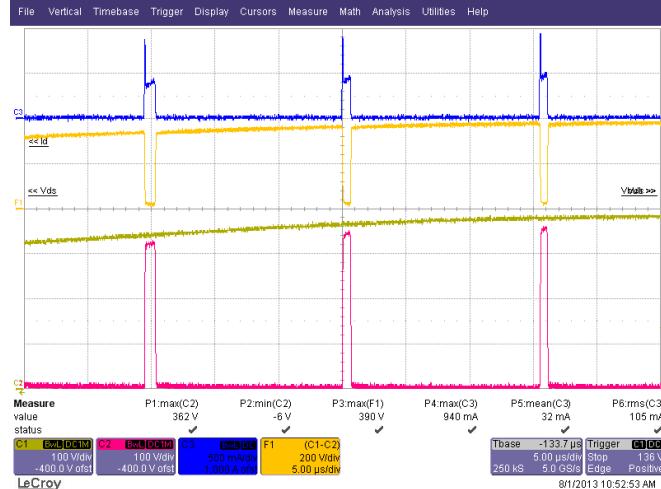
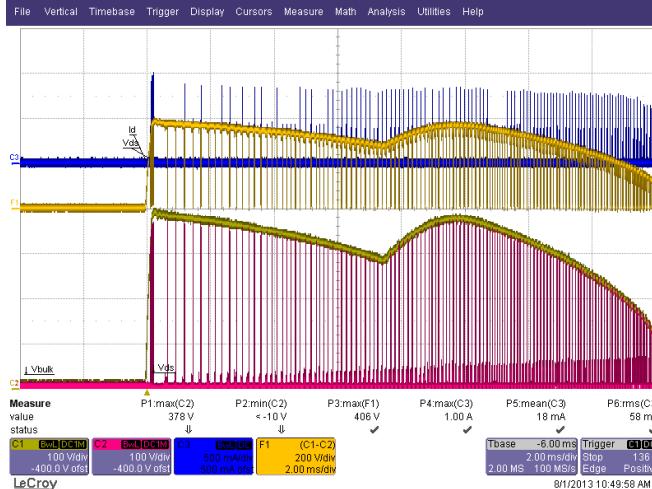


Figure 39 – 265 VAC / 50 Hz Start-up.
Ch1: V_{BULK} , 100 V / div.
Ch2: V_{S-G} , 100 V / div.
Ch3: I_{DRAIN} , 0.5 A / div.
F1: V_{D-S} , 200 V / div.
Time Scale: 2 ms / div.

Figure 40 – 265 VAC / 50 Hz Start-up.
Ch1: V_{BULK} , 100 V / div.
Ch2: V_{S-G} , 100 V / div.
Ch3: I_{DRAIN} , 0.5 A / div.
F1: V_{D-S} , 200 V / div.
Time Scale: 5 μ s / div.

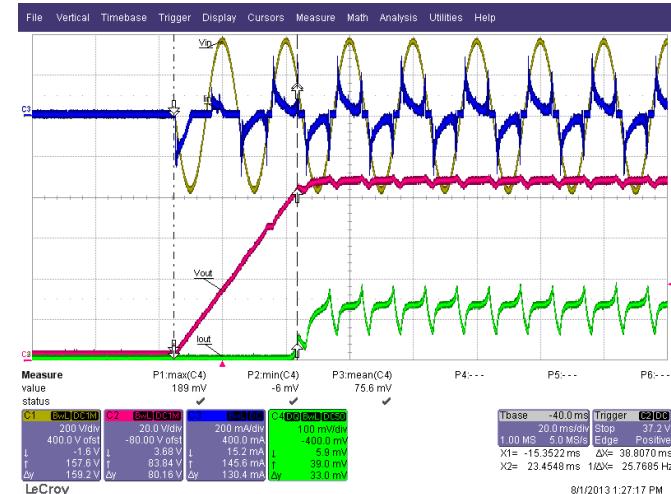
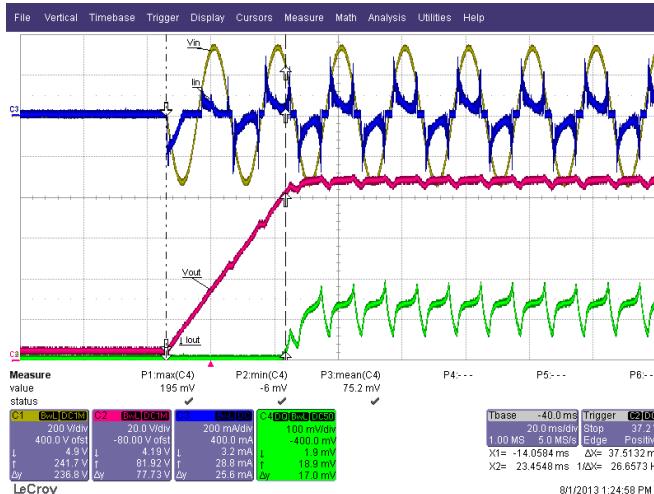
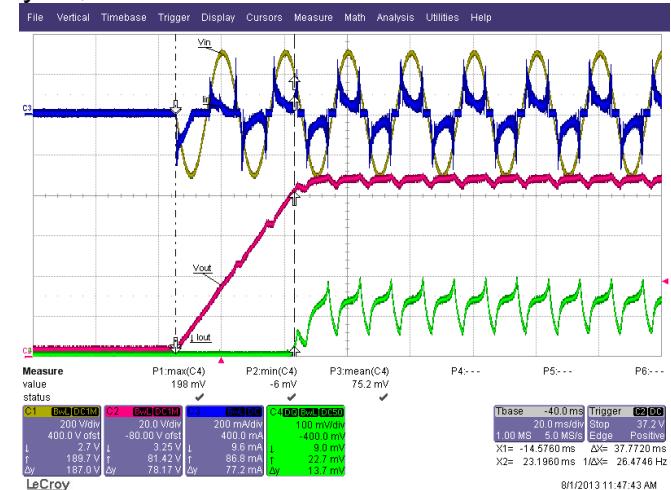
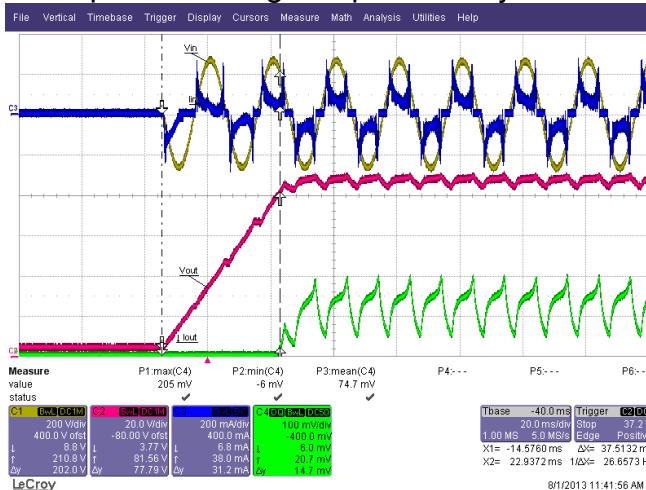


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10.4 Output Current Start-up Profile

Output current/light is present in just one AC cycle, 100 ms.



10.5 Input-Output Profile

There is no limitation to the amount of output capacitance that can be added. If the application requires low output current ripple then increase the output capacitor value until the desired level is achieved. Note that the output current waveform below will change depending on LED load impedance which also varies according to LED type. An LED with high bulk resistance (low current rated LED) will tend to have lower ripple than high current LED with low bulk resistance for the same current impressed.

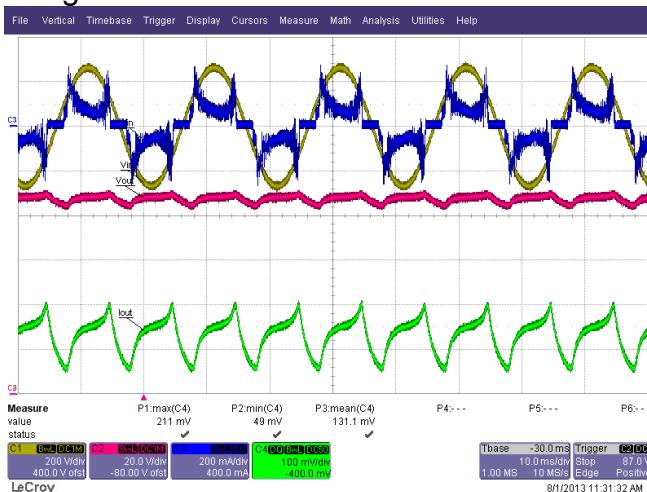


Figure 45 – 190 VAC / 50 Hz, Nominal V_{LED} Load.

Ch1 (Yellow): V_{IN} , 200 V / div.
 Ch2 (Red): V_{OUT} , 20 V.
 Ch3 (Blue): I_{IN} , 200 mA / div.
 Ch4 (Green): I_{OUT} , 100 mA / div.
 Time Scale: 10 ms / div.

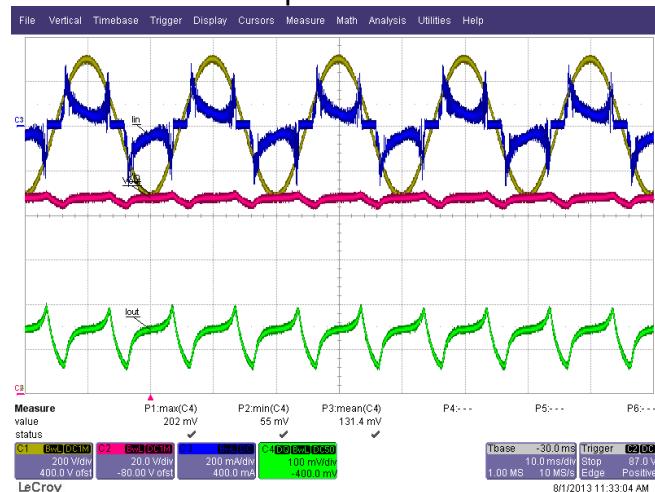


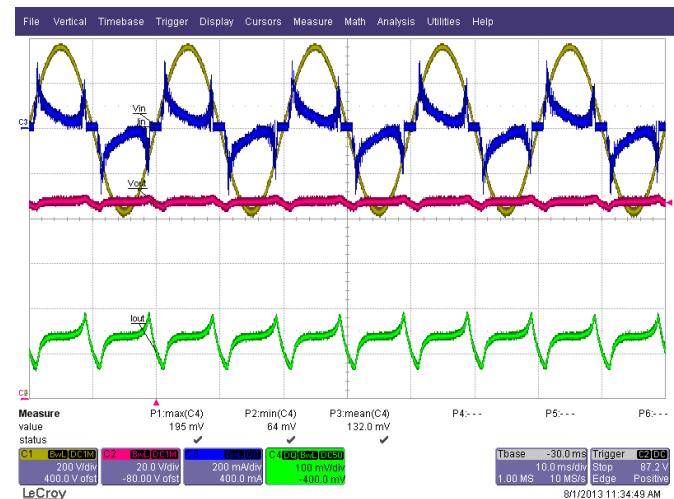
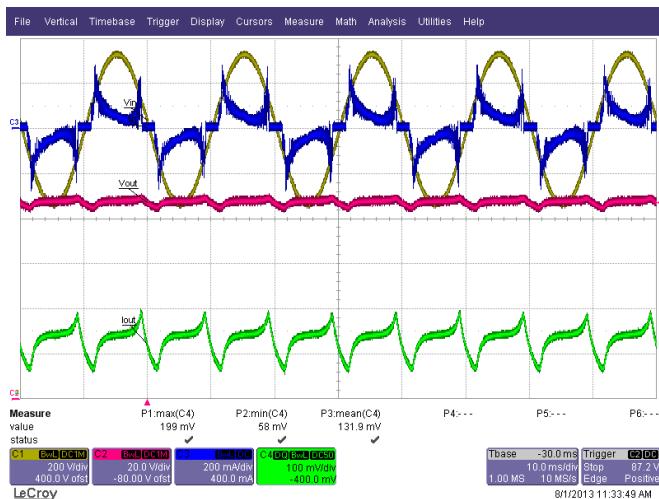
Figure 46 – 220 VAC / 50 Hz, Nominal V_{LED} Load.

Ch1 (Yellow): V_{IN} , 200 V / div.
 Ch2 (Red): V_{OUT} , 20 V.
 Ch3 (Blue): I_{IN} , 200 mA / div.
 Ch4 (Green): I_{OUT} , 100 mA / div.
 Time Scale: 10 ms / div.



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10.6 Line Sag and Surge

An inherent advantage of the buck converter implemented within LYTSwitch-0 is the imperceptible start-up delay, the driver will turn-on within 100 ms as shown below. No failure of any component occurred during line fluctuation tests.



Figure 49 – Line Sag Test at 230 - 0 V at 1 s Interval.

Ch1: V_{IN} , 200 V / div.

Ch2: V_{OUT} , 20 V / div.

Ch4: I_{OUT} , 100 mA / div.

Time Scale: 2 s / div.

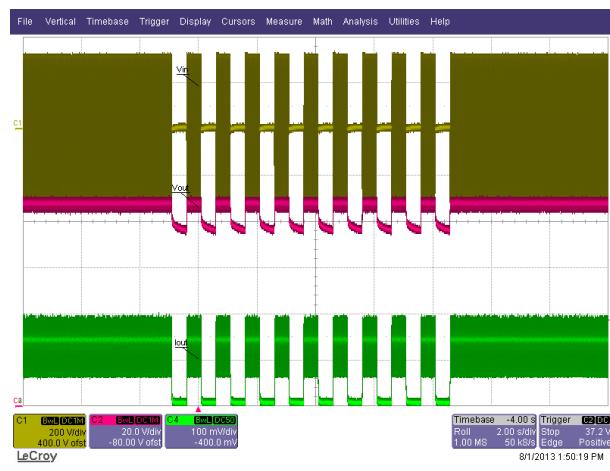


Figure 50 – Line Sag Test at 230 - 0 V at 0.5 s Interval.

Ch1: V_{IN} , 200 V / div.

Ch2: V_{OUT} , 20 V / div.

Ch4: I_{OUT} , 100 mA / div.

Time Scale: 2 s / div.

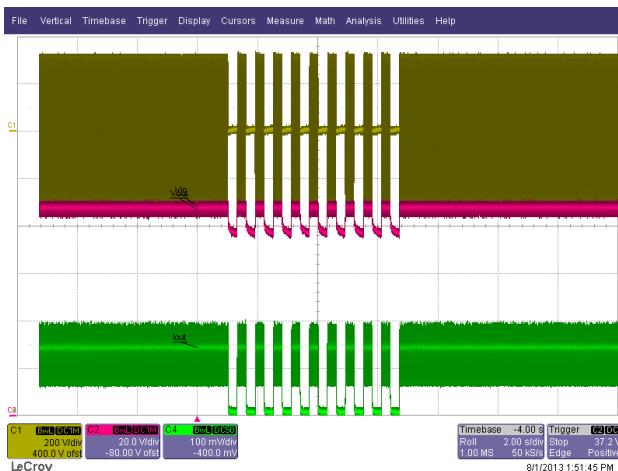


Figure 51 – Line Sag Test at 230 - 0 V at 0.3 s Interval.

Ch1: V_{IN} , 200 V / div.

Ch2: V_{OUT} , 20 V / div.

Ch4: I_{OUT} , 100 mA / div.

Time Scale: 2 s / div.

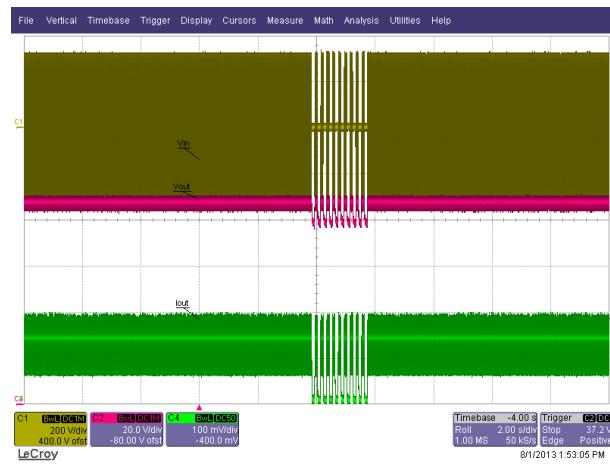


Figure 52 – Line Sag Test at 230 - 0 V at 0.1 s Interval.

Ch1: V_{IN} , 200 V / div.

Ch2: V_{OUT} , 20 V / div.

Ch4: I_{OUT} , 100 mA / div.

Time Scale: 2 s / div.

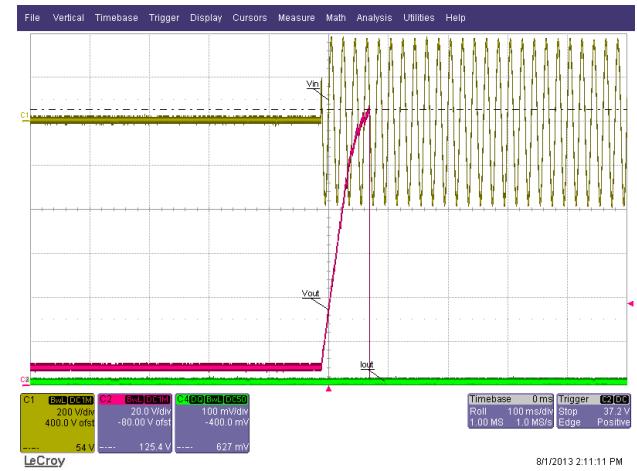
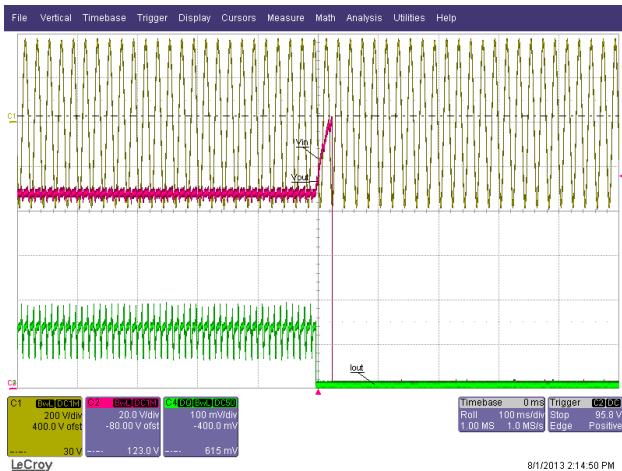


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10.7 One Shot No-load Protection

The reference design is protected with one shot no-load protection. Replace VR1 after fault. It's been observed that the SMD Zener tends to short out when it fails. Use of a SMD diode (500 mW) is recommended.



10.8 Brown-out / Brown-in

No failure of any component during brown-out test of 1 V / sec and 10 V / sec AC cut-in and cut-off.

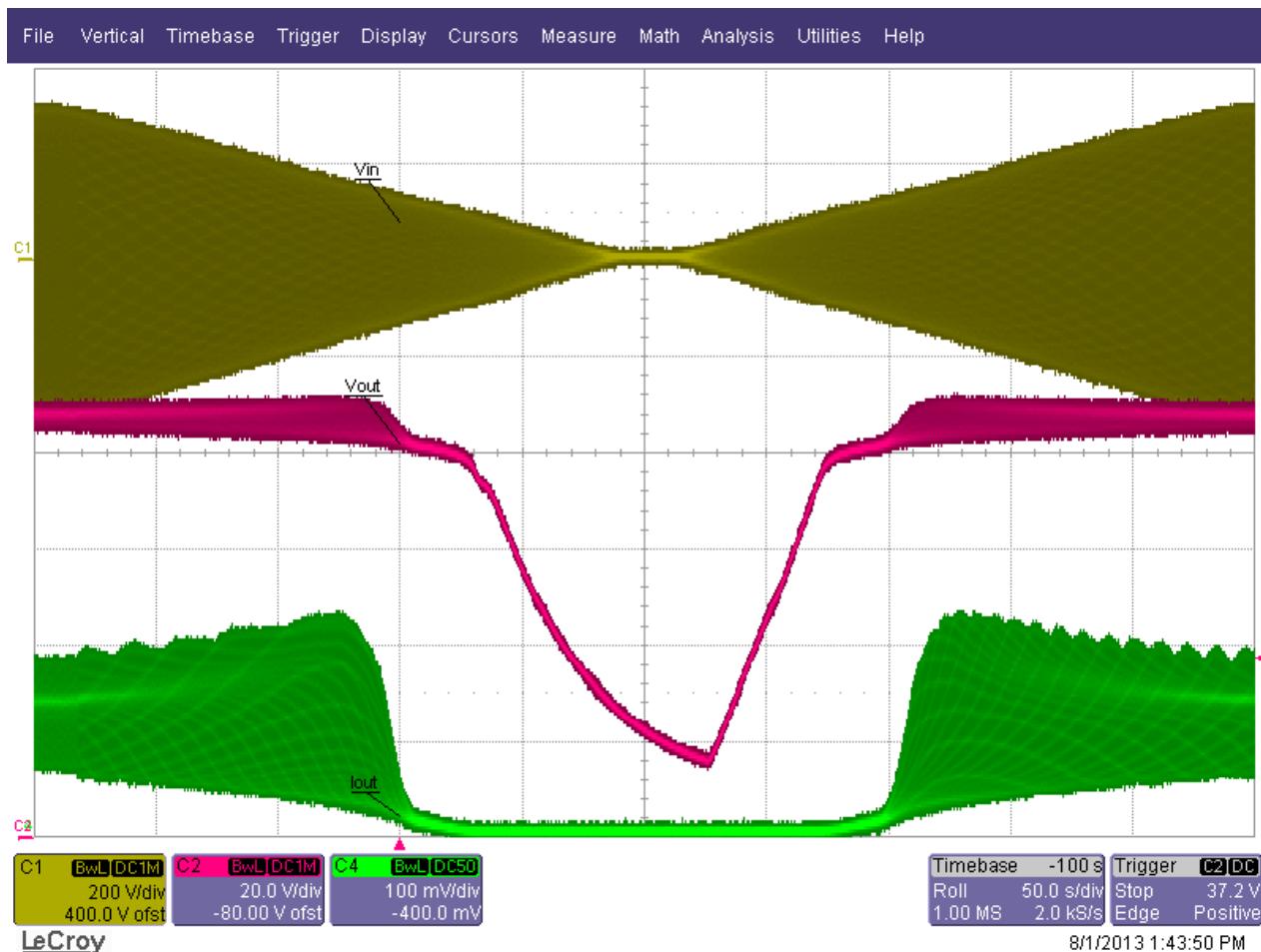


Figure 55 – Brown-out Test at 1 V / s.
The Unit is Able to Operate Normally Without Any Failure and Without Flicker.

230 V - 0 - 230 V.
 Ch1: V_{IN} , 200 V / div.
 Ch2: V_{OUT} , 20 V / div.
 Ch3: I_{OUT} , 100 mA / div.
 Time Scale: 50 s / div.



11 Line Surge

Differential input line 1 kV / 50 μ s surge testing was completed on a single test unit following the test method described in IEC61000-4-5. Input voltage was set at 230 VAC / 60 Hz. Output was loaded at full load and operation was verified following each surge event.

| Surge Level (kV) | Input Voltage (VAC) | Injection Location | Injection Phase (°) | Test Result (Pass/Fail) |
|------------------|---------------------|--------------------|---------------------|-------------------------|
| +1 | 230 | L to N | 90 | Pass |
| -1 | 230 | L to N | 90 | Pass |
| +1 | 230 | L to N | 270 | Pass |
| -1 | 230 | L to N | 270 | Pass |
| +1 | 230 | L to N | 0 | Pass |
| -1 | 230 | L to N | 0 | Pass |

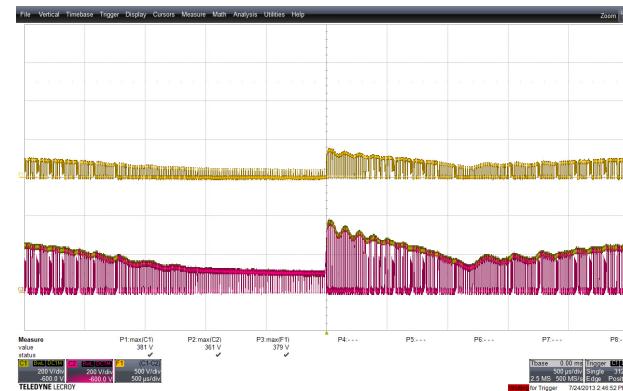
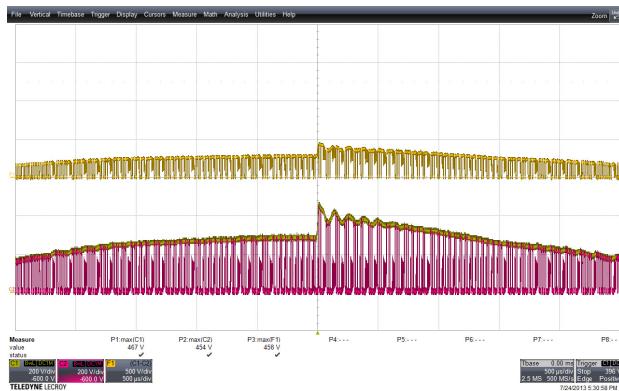
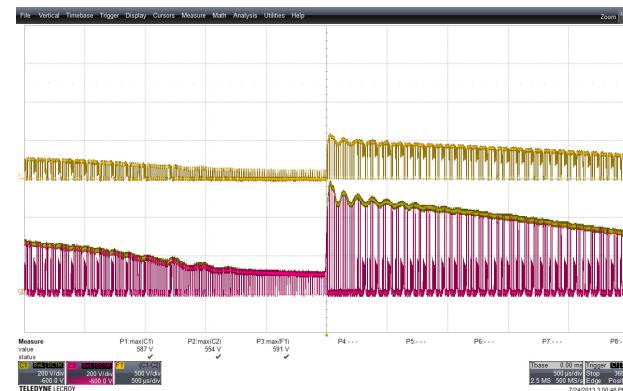
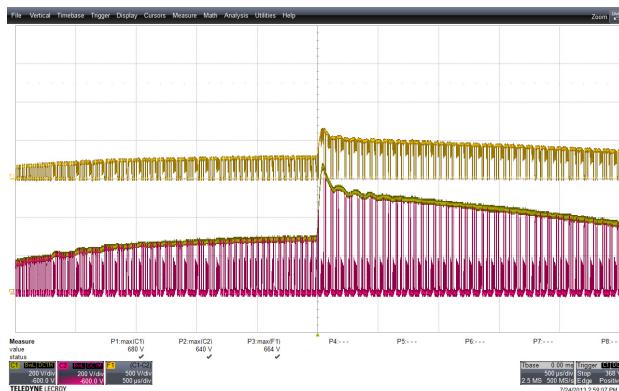
Unit passed under all test conditions. Tested up to 30% more voltage and no failure was observed.

Differential ring input line surge testing was completed on a single test unit following the test method described in IEC61000-4-5. Input voltage was set at 230 VAC / 60 Hz. Output was loaded at full load and operation was verified following each surge event.

| Surge Level (V) | Input Voltage (VAC) | Injection Location | Injection Phase (°) | Test Result (Pass/Fail) |
|-----------------|---------------------|--------------------|---------------------|-------------------------|
| +2500 | 230 | L to N | 90 | Pass |
| -2500 | 230 | L to N | 90 | Pass |
| +2500 | 230 | L to N | 270 | Pass |
| -2500 | 230 | L to N | 270 | Pass |
| +2500 | 230 | L to N | 0 | Pass |
| -2500 | 230 | L to N | 0 | Pass |

Unit passed under all test conditions. Tested up to 30% more voltage and no failure was observed.





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12 Conducted EMI

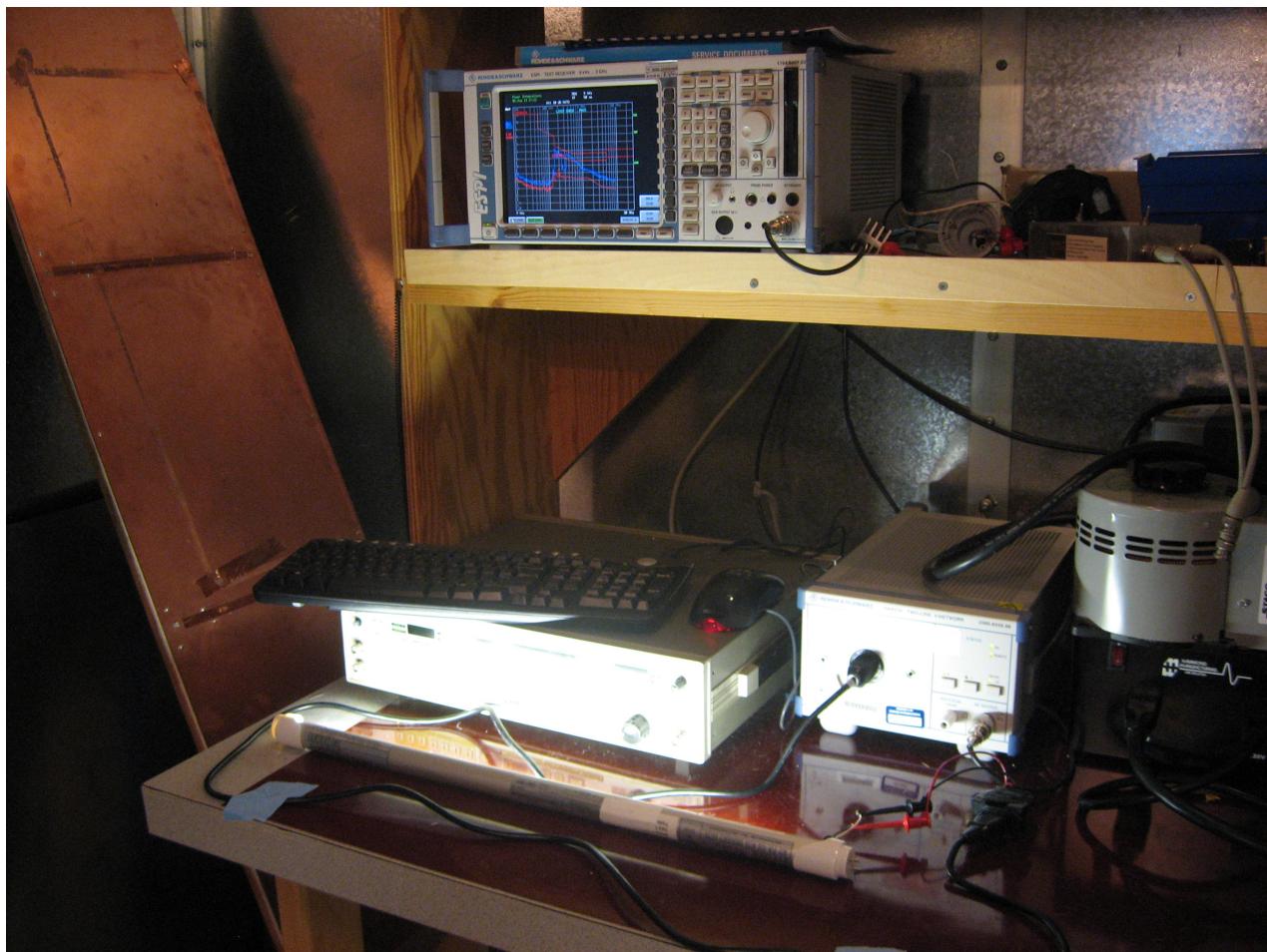


Figure 60 – The Driver was Tested in a Tube Lamp. Position the AC Inlet as Close as Possible to the End for Best EMI Performance. Let the DC Output Wire Cross the Driver.



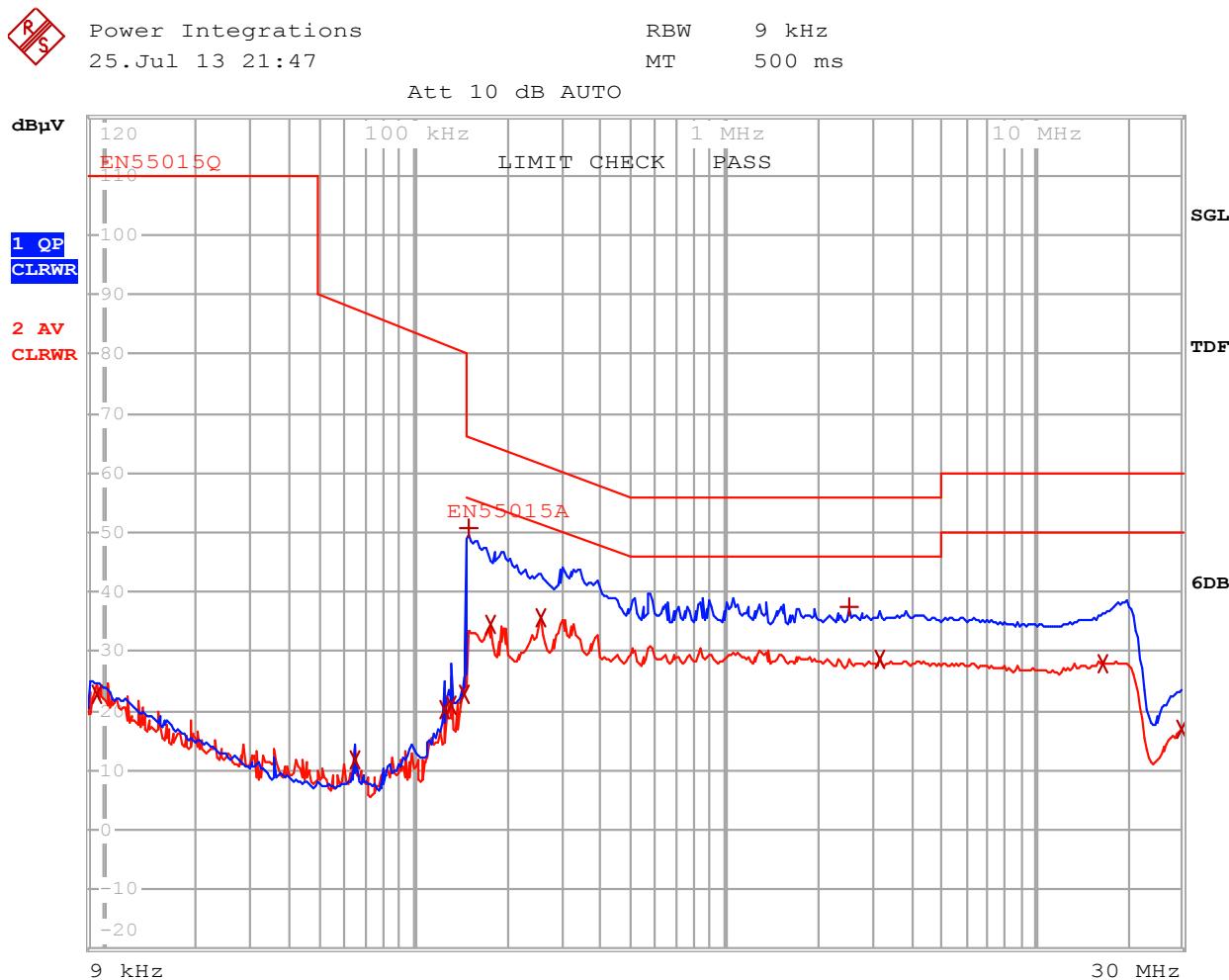


Figure 26 – Conducted EMI, Maximum Steady State Load, 230 VAC, 60 Hz, and EN55015 B Limits. UUT was Fitted Inside a T8 Tube Enclosure.



| EDIT PEAK LIST (Final Measurement Results) | | | | | |
|--|-------------------|-------|------------|--------|----------|
| Trace1: | EN55015Q | | | | |
| Trace2: | EN55015A | | | | |
| Trace3: | --- | | | | |
| TRACE | FREQUENCY | LEVEL | dB μ V | DELTA | LIMIT dB |
| 2 Average | 9.4590904509 kHz | 22.77 | N gnd | | |
| 2 Average | 64.5467705779 kHz | 11.79 | N gnd | | |
| 2 Average | 125.720633819 kHz | 20.27 | L1 gnd | | |
| 2 Average | 130.825395691 kHz | 21.01 | N gnd | | |
| 2 Average | 148.891503746 kHz | 22.87 | L1 gnd | | |
| 1 Quasi Peak | 151.5 kHz | 50.87 | N gnd | -15.04 | |
| 2 Average | 175.886796739 kHz | 34.50 | L1 gnd | -20.17 | |
| 2 Average | 256.711570318 kHz | 35.64 | L1 gnd | -15.89 | |
| 1 Quasi Peak | 2.50634031306 MHz | 37.58 | N gnd | -18.41 | |
| 2 Average | 3.15087835298 MHz | 28.85 | L1 gnd | -17.15 | |
| 2 Average | 16.4353775277 MHz | 27.83 | L1 gnd | -22.16 | |
| 2 Average | 30 MHz | 16.88 | L1 gnd | -33.11 | |

Table 3 – Conducted EMI, Maximum Steady State Load, 230 VAC, 60 Hz, and EN55015 B Limits. UUT was Fitted Inside a T8 Tube Enclosure.

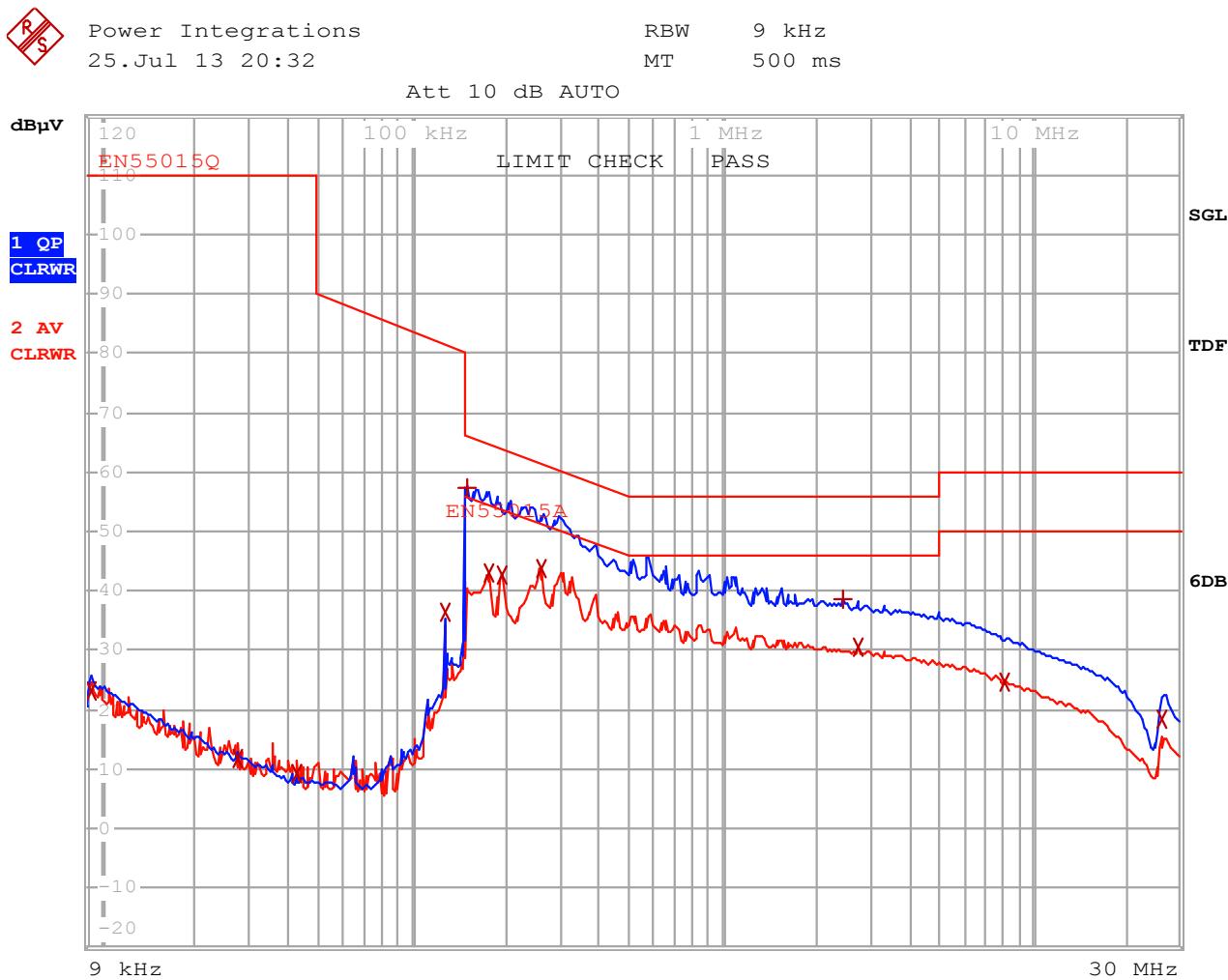


Figure 61 – Conducted EMI, Maximum Steady State Load, 230 VAC, 60 Hz, and EN55015 B Limits. UUT Without Enclosure.



| EDIT PEAK LIST (Final Measurement Results) | | | | | | |
|--|-------------------|-------|------------|-----|--------|----------------|
| Trace1: | EN55015Q | | | | | |
| Trace2: | EN55015A | | | | | |
| Trace3: | --- | | | | | |
| TRACE | FREQUENCY | LEVEL | dB μ V | L1 | gnd | DELTA LIMIT dB |
| 2 Average | 9.1809 kHz | 23.11 | L1 | gnd | | |
| 2 Average | 27.159076558 kHz | 11.76 | L1 | gnd | | |
| 2 Average | 42.0780345374 kHz | 9.26 | N | gnd | | |
| 2 Average | 128.247618558 kHz | 36.48 | L1 | gnd | | |
| 1 Quasi Peak | 151.5 kHz | 57.33 | N | gnd | -8.57 | |
| 2 Average | 175.886796739 kHz | 42.89 | L1 | gnd | -11.78 | |
| 2 Average | 194.288447245 kHz | 42.76 | L1 | gnd | -11.08 | |
| 2 Average | 259.278686021 kHz | 43.74 | L1 | gnd | -7.70 | |
| 1 Quasi Peak | 2.45695550736 MHz | 38.72 | L1 | gnd | -17.27 | |
| 2 Average | 2.71400741459 MHz | 30.37 | L1 | gnd | -15.62 | |
| 2 Average | 8.10890375706 MHz | 24.58 | L1 | gnd | -25.41 | |
| 2 Average | 26.2351923234 MHz | 18.47 | N | gnd | -31.52 | |

Table 4 – Conducted EMI, Maximum Steady State Load, 230 VAC, 60 Hz, and EN55015 B Limits. UUT without Enclosure.

13 Revision History

| Date | Author | Revision | Description & changes | Reviewed |
|-----------|--------|----------|-----------------------|-------------|
| 08-Oct-13 | JDC | 1.0 | Initial Release | Apps & Mktg |
| | | | | |
| | | | | |
| | | | | |



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