

# **Design Example Report**

Title	42W, 4 Output Supply using TOP245Y
Specification	Input: 230 VAC Outputs: 5V/4A, 6.8V/1.8A, 12V/0.8A, -10V/0.1A
Application	Set Top Box w/Hard Drive
Author	Power Integrations Applications Department
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Revision	1.0

## **Summary and Features**

- High Efficiency (81% min)
- Low Parts Count
- Low Output Ripple
- Meets Conducted CISPR22B EMI with Margin
- Small Transformer (EER35)

The products and applications illustrated herein (including circuits external to the products and transformer construction) may be covered by one or more U.S. and foreign patents or potentially by pending U.S. and foreign patent applications assigned to Power Integrations. A complete list of Power Integrations' patents may be found at www.powerint.com.

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## **Important Note:**

7.5

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Although this board is designed to satisfy safety isolation requirements, the engineering prototype has not been agency approved. Therefore, all testing should be performed using an isolation transformer to provide the AC input to the prototype board.

Design Reports contain a power supply design specification, schematic, bill of materials, and transformer documentation. Performance data and typical operation characteristics are included. Typically only a single prototype has been built.

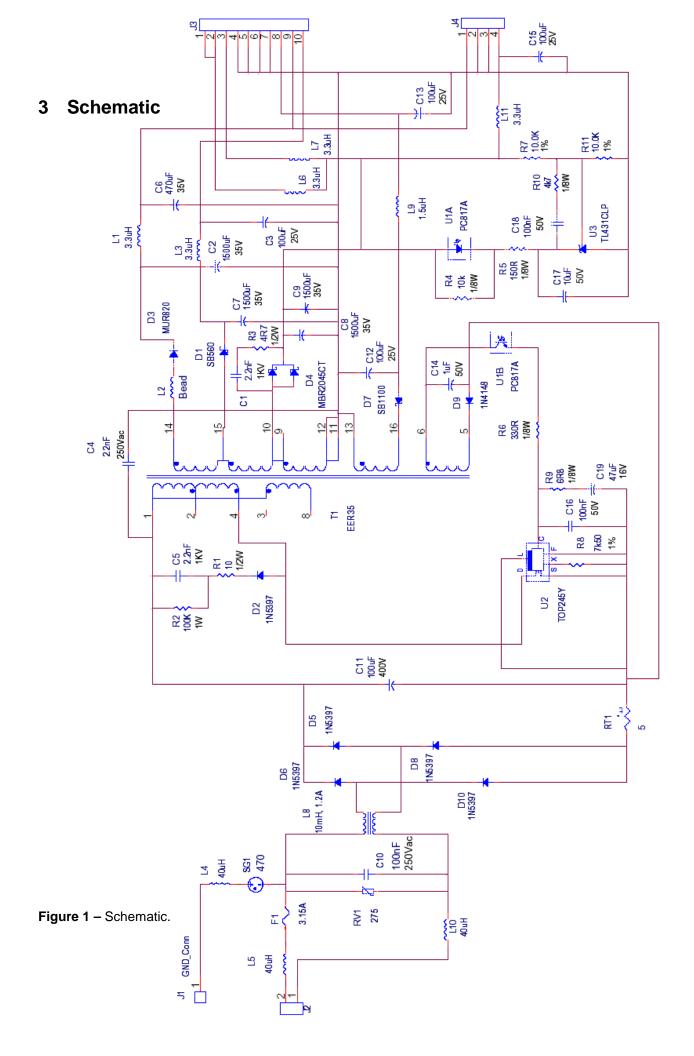
# 1 Introduction

This document is an engineering report describing a 230VAC input, 4 output supply power supply utilizing a TOP245Y. This power supply is intended for use in a set top box.

The document contains the power supply specification, schematic, bill of materials, transformer documentation, printed circuit layout, and performance data.

# **Power Supply Specification**

Description	Symbol	Min	Тур	Max	Units	Comment
Input						
Voltage	$V_{IN}$	180		265	VAC	2 Wire – no P.E.
Frequency	f <sub>LINE</sub>	47	50		Hz	
No-load Input Power (230 VAC)				0.3	W	
Output	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	4.75	5.00	5.05	.,	. 50/
Output Voltage 1 Output Ripple Voltage 1	V <sub>OUT1</sub> V <sub>RIPPLE1</sub>	4.75	5.00	5.25 50	V mV	± 5% 20 MHz Bandwidth
Output Current 1	RIPPLE1	1	2.5	4	A	20 MHZ Bandwidth
Output Voltage 2	V <sub>OUT2</sub>	6.12	6.80	7.48	V	± 10%
Output Ripple Voltage 2	V <sub>RIPPLE2</sub>	0.12	0.00	50	mV	20 MHz Bandwidth
, ,,		1.2	1.5	1.8		20 WI IZ Dandwidth
Output Current 2	I <sub>OUT2</sub>			_	A	. 400/
Output Voltage 3	V <sub>OUT3</sub>	10.8	12.0	13.2	V	± 10%
Output Ripple Voltage 3	V <sub>RIPPLE3</sub>			50	mV	20 MHz Bandwidth
Output Current 3	I <sub>OUT3</sub>	0.2	0.8	2.5	Α	
Output Voltage 4	$V_{OUT4}$	-9	-10	-11	V	± 10%
Output Ripple Voltage 4	$V_{RIPPLE4}$			50	mV	20 MHz Bandwidth
Output Current 4	I <sub>OUT4</sub>		0.05	0.10	Α	
Total Output Power						
Continuous Output Power	P <sub>OUT</sub>			41.8	W	
Peak Output Power	P <sub>OUT_PEAK</sub>			52.7	W	
Efficiency	η	80			%	Measured at P <sub>OUT</sub> (42 W), 25 °C
Environmental						
Conducted EMI		Mee	ts CISPR2	2B / EN55	022B	
Safety		Design		t IEC950,	UL1950	
Caroly			Cla 	ıss II İ	l	1.2/50 μs surge, IEC 1000-4-5,
Surge		4			kV	Series Impedance: Differential Mode: $2 \Omega$ Common Mode: $12 \Omega$
Surge		3			kV	100 kHz ring wave, 500 A short circuit current, differential and common mode
Ambient Temperature	T <sub>AMB</sub>	0		60	°C	Free convection, sea level



# 4 Circuit Description

## 4.1 Input EMI Filtering

Components L5, L8, L10, C4, and C10 provide EMI filtering, while L4, L5, L10, SG1, and RV1 provide line surge protection.

## 4.2 TOPSwitch Primary

Components D2, R1-2, and C5 comprise an RCD clamp with damping to limit the primary leakage spike. Use of a normal recovery diode in this clamp circuit allows some leakage energy to be recycled. Capacitors C16 and C19 bypass the U2 control pin. Components C19 and R9 also provide frequency compensation for U2. Resistor R8 sets the U2 current limit to 90% of its nominal value.

## 4.3 Output Rectification

Output rectification and filtering is provided by D4 and C8-9 for the 5V output, D1 and C7 for the 6.8V output, D3 and C2 for the 12V output, and D7 and C12 for the -10V output. Components L1, 3, L6, L7, L9, C3, C6, C13 and C15 are used for additional high frequency filtering. Ferrite bead L2 is used to center the 12V output closer to its nominal value.

## 4.4 Output Feedback

Output feedback is provided from the 5V output. Resistors R7 and R11 program the output voltage. The output error signal is coupled back to the supply primary via R5 and U1. Capacitor C18 and 10 compensate U3, while C17 allows current through U1 during startup to prevent output overshoot. Resistor R4 discharges C17 when the supply is off.

# **PCB Layout**

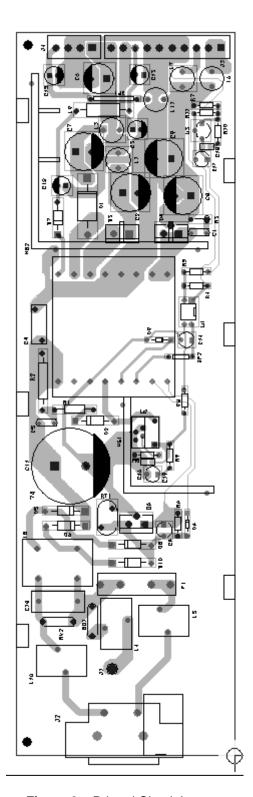


Figure 2 – Printed Circuit Layout.

# **Bill Of Materials**

Item C	ity Part Reference	Description	Mfg Part Number	Mfg
1	2 C1 C5	Cap, Cer, 2200pF, 1KV, 10%	DD-222	Vishay
2	4 C2 C7 C8 C9	Cap,AI Elect,1500uF,35V,12.5mmX35mm,LXZ Series,NIPPON CHEMI-CON	LXZ35VB152MK35LL	Nippon Chemi-Con
3	3 C3 C13 C15	Cap,Al Elect,100uF,25V,6.3mmX11.5mm,NHG Series,Panasonic	ECA-1EHG101	Panasonic
4	1 C4	Cap,Cer,2.2nF, Y2, 250VAC	440LD22	Cera-Mite
5	1 C6	Cap,AI Elect,470uF,35V,10mmX20mm,LXZ Series,NIPPON CHEMI-CON	LXZ35VB471MJ20LL	Nippon Chemi-Con
6	1 C10	Cap,Metal Poly,0.1uF, 250/275VAC	ECQ-U2A104ML	Panasonic
7	1 C11	Cap,Al Elect,100uF,400V,30mmX25mm,TSED Series, Panasonic	ECO-S2GP101CA	Panasonic
8	1 C12	Cap,Al Elect,100uF,25V,6.3mmX11.5mm,LXZ Series,NIPPON CHEMI-CON	LXZ25VB101MF11LL	Nippon Chemi-Con
9	1 C14	Cap,Al Elect,1uF,50V,5mmX11.5mm,NHG Series,Panasonic	ECA-1HHG010	Panasonic
10	2 C16 C18	Cap,Cer, 0.10 uF, 50V, X7R, 10%	ECU-S1H104KBB	Panasonic
11	1 C17	Cap,Al Elect,10uF,50V,5mmX11.5mm, NHG Series,Panasonic	ECA-1HHG100	Panasonic
12	1 C19	Cap,Al Elect,47uF,16V,5mmX11.5mm,NHG Series,Panasonic	ECA-1CHG470	Panasonic
13	1 D1	Rectifier Schottky 5A 60V DO-201AD	SB560	General Semiconductor
14	5 D2 D5 D6 D8 D10	Rectifier GPP 600V 1.5A DO-204	1N5397	Rectron
15	1 D3	Diode,Ultrafast, 8A, 100V	MUR820	ON Semiconductor
16	1 D4	Diode Schottky 45V 20A TO-220AB	MBR2045CT	General Semiconductor
17	1 D7	Diode Schottky,100V 1A DO-41	SB1100	Diodes, Inc.
18	1 D9	Diode SGL JUNC 100V 4.0NS DO-35	1N4148	
19	1 F1	FUSE T-LAG 3.15A, 250V,Slo-Blo		Bel Fuse
20	1 J1	Geound Wire Assembly		
21	1 J2	AC Input Receptacle	HJC-028	Singatron
22	1 J3	CONN HEADER 10POS(1 X10) .156 VERT TIN		Molex
23	1 J4	CONN HEADER 4POS(1 X 4) .156 VERT TIN		Molex
24	5 L1 L3 L6 L7 L11	Inductor,3.3uH,2.66A	822LY_3R3M	Toko

25	2 L2	Bead, Ferrite, 3.25X3.5 mm, 43 material	2643001501	Fair-Rite
25	2 L2	beau, Ferrite, 3.23/3.3 mm,43 material	2043001301	raii-Kile
26	3 L4 L5 L10	Inductor,40uH,Toroid		
27	1 L8	LINE FILTER,10mH,1.2A		TDK
28	1 L9	Bead, Ferrite, 6.7mm X 3.5mm, 43 material	2743004112	Fair-rite
29	1 R1	Res, 10.0, 1/2W, 5%, Carbon Film	CFR-50JB-10R	Yageo
30	1 R2	Res, 100K ,1W, 5%, Metal Film	RSF200JB-100K	Yageo
31	1 R3	Res, 4.7, 1/2W, 5%, Carbon Film	CFR-50JB-4R7	Yageo
32	1 R4	Res, 10K, 1/8W, 5%, Carbon Film	CFR-12JB-10K	Yageo
33	1 R5	Res, 150, 1/8W, 5%, Carbon Film	CFR-12JB-150R	Yageo
34	1 R6	Res, 330, 1/8W, 5%, Carbon Film	CFR-12JB-330R	Yageo
35	2 R7 R11	Res,10.0K, 1/4W, 1%, M-FILM	MFR-25FBF-10K0	Yageo
36	1 R8	Res,7.50K, 1/4W, 1%, M-FILM	MFR-25FBF-7K50	Yageo
37	1 R9	Res, 6.8, 1/8W, 5%, Carbon Film	CFR-12JB-6R8	Yageo
38	1 R10	Res, 4.7K, 1/8W, 5%, Carbon Film	CFR-12JB-4K7	Yageo
39	1 RT1	Thermistor,5 Ohms,3 A	SCK-053	THINKING ELECTRONICS
40	1 RV1	VARISTOR 275V 75J 14MM RADIAL LA	V275LA20A	Littlefuse
41	1 SG1	Gas Tube,470V,5kA,Axial	B88069X5740S102	Epcos
42	1 T1	XFMR,HORIZ,16 Pin,776uH,EER35 Core		
43	1 U1	IC,PC817A,PHOTOCOUPLER TRAN OUT CTR 80- 160% 4-DIP	ISP817A	ISOCOM
44	1 U2	IC,TOP245Y,INT. OFF-LINE SWITCHER,60W,TO220-7C	TOP245Y	Power Int.
45	1 U3	IC,TL431CLP, ADJ SHUNT REG TO-92	TL431CLP	TI

# 7 Transformer Specification

# 7.1 Electrical Diagram

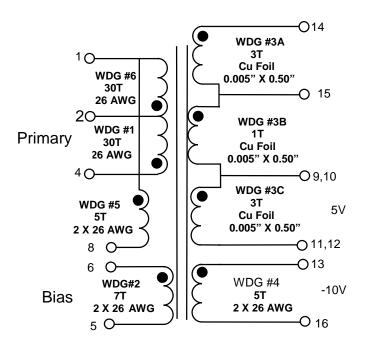


Figure 3 –Transformer Electrical Diagram

# 7.2 Electrical Specifications

Electrical strength	60 Hz 1 second, From	3000 Vac
	Pins 1-6 to Pins 7-12	
Primary Inductance	Pins 1-4, All other	791uH+/-10%
	windings open, 100 kHz	
Resonant Frequency	Pins 1-4, All other	1.3 MHz (min)
	windings open	
Primary leakage	Pins 1-4, Pins 7-12	<15 uH
inductance	shorted, 100 kHz	

## 7.3 Materials

Item	Description
[1]	Core: EER35, ungapped, Nippon Ceramic NC-2H material or
	equiv. Gap for A <sub>L</sub> of 220 nH/T <sup>2</sup>
[2]	Bobbin: EER35 Horizontal 12 pin, TDK BEER35-1116CPH or
	equivalent
[3]	Magnet Wire: #26 AWG Solderable Double Coated
[4]	Copper Foil, 0.50" X 0.005" thick
[5}	Tinned Bus Wire, 24 AWG
[6]	Tape: 3M Type 1298 Polyester Film or equiv. 1.03" wide
[7]	Tape: 3M Type 1298 Polyester Film or equiv. 0.65" wide
[8]	Tape: 3M Type 1298 Polyester Film or equiv. 0.55" wide
[9]	Tape: 3M Type 44. Polyester web or equiv. 0.24" wide (min)
[10]	Transformer Varnish

# 7.4 Transformer Build Diagram

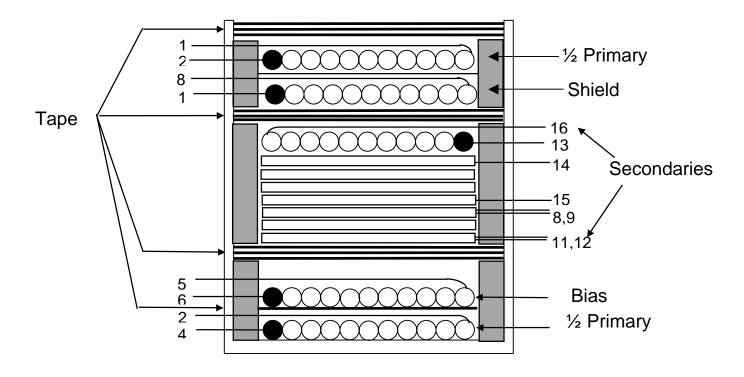


Figure 4 - Transformer Build Diagram.

# 7.5 Transformer Construction

## **WINDING INSTRUCTIONS:**

WINDING INSTRUCTIONS	·
Margin Taping	Apply a 0.24" margin at each side of bobbin using item [9]. Match combined height of primary and bias windings.
½ Primary Winding	Start at pin 4. Wind 30 turns of item [3] in a single layer. Finish at pin
Basic Insulation	Apply one layer of tape [8] for basic insulation.
Bifilar Bias Winding	Start at pin 6. Wind 7 bifilar turns of item [3] uniformly in a single layer, across entire width of bobbin. Finish on pin 5.
Reinforced Insulation	Apply three layers of tape [6] for reinforced insulation.
Margin Taping	Apply a 0.24" margin at each side of bobbin using item [9]. Match combined height of secondary windings.
Secondary Foil Winding	Prepare a cuffed foil assembly using items [4], [5], [7], and [8]. Starting at pin 14, wind 3 turn of foil, finish at pin 15. Wind one turn of foil, finish at pins 9 and 10, Wind three remaining turns, finish at pins 11 and 12.
10 V Bifilar Winding	Starting at pin 13, wind 5 bifilar turns of item [4] directly on top of the foil winding. Space turns evenly across bobbin. Finish at pin 16.
Reinforced Insulation	Apply three layers of tape [6] for reinforced insulation.
Margin Taping	Apply a 0.24" margin at each side of bobbin using item [9]. Match combined height of primary and shield windings.
Shield Winding	Starting at Pin 1, wind 5 bifilar turns of item [3]. Spread turns evenly across bobbin. Finish at pin 8.
Basic Insulation	Apply one layer of tape [9] for basic insulation.
½ Primary Winding	Starting at pin 2, wind 30 turns of item [3] in a single layer. Finish at pin 1.
Outer Insulation	Apply 3 Layers of tape [6] for outer insulation
Varnish	Impregnate transformer using item [10]

# 8 Transformer Spreadsheets

ACDC_TOPGX_Rev1.7_082203 Copyright Power Integrations Inc. 2003 ENTER APPLICATION VARIABLE	INPUT	INFO	INFO	OUTPUT	OUTPUT	UNIT	TOP_GX_FX_082203.xls: TOPSwitch-GX/FX Continuous/Discontinuous Flyback Transformer Design Spreadsheet
VACMIN VACMAX fL VO PO	190 265 50 5					Volts Volts Hertz Volts Watts	Minimum AC Input Voltage Maximum AC Input Voltage AC Mains Frequency Output Voltage Output Power
n Z VB tC	0.8 0.5 12 3					Volts mSeconds	Efficiency Estimate Loss Allocation Factor Bias Voltage Bridge Rectifier Conduction Time Estimate
CIN	100					uFarads	Input Filter Capacitor
ENTER TOPSWITCH-GX VARIAE TOP-GX Chosen Device		TOP245 TOP245	TOP245	Power Out	Power Out	Universal 60W	115 Doubled/230V 85W
KI	0.8			1.296	1 206	Amna	External Ilimit reduction factor (KI=1.0 for default ILIMIT, KI <1.0 for lower ILIMIT)
ILIMITMIN				1.296	1.296	Amps	Use 1% resistor in setting external ILIMIT
ILIMITMAX				1.584	1.584	Amps	Use 1% resistor in setting external ILIMIT
Frequency - (F)=132kHz, (H)=66kHz fS	F 132000			132000	132000	Hertz	Full (F) frequency option - 132kHz TOPSwitch-GX Switching Frequency: Choose between
fSmin				124000	124000	Hertz	132 kHz and 66 kHz TOPSwitch-GX Minimum Switching Frequency
fSmax				140000	140000	Hertz	TOPSwitch-GX Maximum
VOR VDS	110 10					Volts Volts	Switching Frequency Reflected Output Voltage TOPSwitch on-state Drain to Source Voltage
VD	0.5					Volts	Output Winding Diode Forward Voltage Drop
VDB	0.7					Volts	Bias Winding Diode Forward Voltage Drop
KP	0.60						Ripple to Peak Current Ratio (0.4 < KRP < 1.0 : 1.0 < KDP < 6.0)
ENTER TRANSFORMER CORE/OVARIABLES	ONSTRU	ICTION					
Core Type	EER35						
Core Bobbin		EER35_BOBBIN	EER35			P/N: P/N:	PC40EER35-Z BEER-35-1116CPH
AE				1.07	1.07	cm^2	Core Effective Cross Sectional Area
LE AL				9.08 2770		cm nH/T^2	Core Effective Path Length Ungapped Core Effective Inductance
BW				26.1	26.1	mm	Bobbin Physical Winding
М	6					mm	Width Safety Margin Width (Half the Primary to Secondary Creepage Distance)
							5.55pago Distance

L NS	2 3			Number of Primary Layers Number of Secondary Turns
DC INPUT VOLTAGE PARAMETERS VMIN VMAX		251 375	251 Volts 375 Volts	Minimum DC Input Voltage Maximum DC Input Voltage
CURRENT WAVEFORM SHAPE PARAI DMAX IAVG IP IR IRMS		0.31 0.26 1.20 0.72 0.49	0.31 0.26 Amps 1.20 Amps 0.72 Amps 0.49 Amps	Maximum Duty Cycle Average Primary Current Peak Primary Current Primary Ripple Current Primary RMS Current
TRANSFORMER PRIMARY DESIGN P LP NP	ARAMETERS	791 60	791 uHenries 60	Primary Inductance Primary Winding Number of Turns
NB		7	7	Bias Winding Number of
ALG		220	220 nH/T^2	Turns Gapped Core Effective
BM	1	482	1482 Gauss	Inductance Maximum Flux Density at PO,
BP BAC	1	951 445	1951 Gauss 445 Gauss	VMIN (BM<3000) Peak Flux Density (BP<4200) AC Flux Density for Core Loss Curves (0.5 X Peak to Peak)
ur	1	871	1871	Relative Permeability of Ungapped Core
LG		0.56	0.56 mm	Gap Length (Lg > 0.1 mm)
BWE OD		28.2 0.47	28.2 mm 0.47 mm	Effective Bobbin Width Maximum Primary Wire
				Diameter including insulation
INS	•	0.06	0.06 mm	Estimated Total Insulation Thickness (= 2 * film thickness)
DIA	1	0.41	0.41 mm	Bare conductor diameter
AWG		27	27 AWG	Primary Wire Gauge (Rounded to next smaller standard AWG value)
CM		203	203 Cmils	Bare conductor effective area in circular mils
CMA		418	418 Cmils/Amp	Primary Winding Current Capacity (200 < CMA < 500)
TRANSFORMER SECONDARY DESIGI (SINGLE OUTPUT / SINGLE OUTPUT E Lumped parameters	_			
ISP			24.07 Amps	Peak Secondary Current
ISRMS IO			14.38 Amps 10.60 Amps	Secondary RMS Current Power Supply Output Current
IRIPPLE		9.72	9.72 Amps	Output Capacitor RMS Ripple Current
CMS	2	876	2876 Cmils	Secondary Bare Conductor
AWGS		15	15 AWG	minimum circular mils Secondary Wire Gauge (Rounded up to next larger
DIAS		1.45	1.45 mm	standard AWG value) Secondary Minimum Bare Conductor Diameter
ODS		4.70	4.70 mm	Secondary Maximum Outside Diameter for Triple Insulated Wire
INSS		1.62	1.62 mm	Maximum Secondary Insulation Wall Thickness
VOLTAGE STRESS PARAMETERS VDRAIN		626	626 Volts	Maximum Drain Voltage

PIVS		24	24 Volts	Estimate (Includes Effect of Leakage Inductance) Output Rectifier Maximum
PIVB		55	55 Volts	Peak Inverse Voltage Bias Rectifier Maximum Peak
FIVD		55	33 VOIIS	Inverse Voltage
(MULTIPLE OUTPUTS) 1st output	DARY DESIGN PARAMETERS			
VO1 IO1	5.0 2.500		Volts Amps	Output Voltage Output DC Current
PO1 VD1	0.5	12.50	12.50 Watts Volts	Output Power Output Diode Forward Voltage Drop
NS1		3.00	3.00	Output Winding Number of Turns
ISRMS1 IRIPPLE1		3.391 2.29	3.391 Amps 2.29 Amps	Output Winding RMS Current Output Capacitor RMS Ripple Current
PIVS1		24	24 Volts	Output Rectifier Maximum Peak Inverse Voltage
CMS1		678	678 Cmils	Output Winding Bare Conductor minimum circular mils
AWGS1		21	21 AWG	Wire Gauge (Rounded up to next larger standard AWG value)
DIAS1		0.73	0.73 mm	Minimum Bare Conductor Diameter
ODS1		4.70	4.70 mm	Maximum Outside Diameter for Triple Insulated Wire
2nd output VO2 IO2	6.8 1.500	10.00	Volts Amps	Output Voltage Output DC Current
PO2 VD2	0.5	10.20	10.20 Watts Volts	Output Power Output Diode Forward Voltage Drop
NS2		3.98	3.98	Output Winding Number of Turns
ISRMS2 IRIPPLE2		2.035 1.37	2.035 Amps 1.37 Amps	Output Winding RMS Current Output Capacitor RMS Ripple Current
PIVS2		32	32 Volts	Output Rectifier Maximum Peak Inverse Voltage
CMS2		407	407 Cmils	Output Winding Bare Conductor minimum circular mils
AWGS2		24	24 AWG	Wire Gauge (Rounded up to next larger standard AWG value)
DIAS2		0.51	0.51 mm	Minimum Bare Conductor Diameter
ODS2		3.54	3.54 mm	Maximum Outside Diameter for Triple Insulated Wire
3rd output VO3 IO3 PO3 VO3	12.0 2.500	30.00	Volts Amps 30.00 Watts	Output Voltage Output DC Current Output Power Output Diode Forward
VD3	0.7		Volts	Output Diode Forward Voltage Drop

NS3	6.93	6.93	Output Winding Number of Turns
ISRMS3	3.391	3.391 Amps	Output Winding RMS Current
IRIPPLE3	2.29	2.29 Amps	Output Capacitor RMS Ripple
			Current
PIVS3	55	55 Volts	Output Rectifier Maximum
			Peak Inverse Voltage
CMS3	678	678 Cmils	Output Winding Bare
			Conductor minimum circular
			mils
AWGS3	21	21 AWG	Wire Gauge (Rounded up to
			next larger standard AWG
			value)
DIAS3	0.73	0.73 mm	Minimum Bare Conductor
			Diameter
ODS3	2.04	2.04 mm	Maximum Outside Diameter
			for Triple Insulated Wire

#### **Performance Data** 9

All measurements performed at room temperature, 60 Hz input frequency, unless otherwise specified.

#### 9.1 Thermal Performance

Thermal measurements were made with the power supply mounted in the chassis, using a slip-on heat sink on the TOPSwitch. A thermocouple was attached to the heat sink next to the TOPSwitch source tab using solder. Another thermocouple was soldered to a length of adhesive-backed copper tape, which was attached to the transformer. A thermocouple was taped in the center of the chassis, with the junction in free air. This thermocouple was used to measure the ambient air temperature inside the chassis. All holes in chassis were sealed with tape except ventilation holes in chassis and holes used for load and thermocouple wires. A solid cardboard sheet was used as the chassis top lid. The thermal chamber temperature outside the chassis was adjusted until the desired temperature was attained inside the chassis. Due to the limited size of the thermal chamber, the chassis was inserted diagonally into the chamber, with the power supply side tilted up. This may mean that the local ambient temperature of the supply was higher than that that measured by the thermocouple, which was located in the chassis center.

The internal ambient temperature was allowed to rise with the unit running at the worst case power dissipation (e.g. 180VAC) until the unit shutdown (S/D) and the maximum ambient temperature was then recorded. The device was allowed to cool and restart, and the thermals measured using the nominal supply voltage at both normal room ambient and the elevated temperature at which shut down occurred at low line.

Item	180 VAC	230 VAC	230 VAC
Ambient	58	59	23
TOPSwitch (U3)	S/D	122	87
Transformer (T1)	S/D	73	52

### 10 Waveforms

## 10.1 12V Output Turn Off

The waveforms shown below were taken with output loads set to 5V/4A, 6.8V/1.5A, and 12V/0.5A, with a fixed 100 ohm resistor on the -10V output. The 5V and 12V outputs were monitored with an oscilloscope. The oscilloscope was triggered on the falling edge of the 5V output. The waveforms show the rise in the lightly loaded 12V output just before the heavily loaded +5V output goes out of regulation after removal of AC power. Use of a heavy foil on the transformer secondaries, along with a small ferrite bead in series with the 12V rectifier, keeps the 12V overshoot within 5%. The ferrite bead also helps to

center the 12V output.

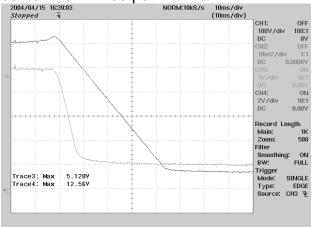


Figure 5 - 180 VAC, 5V/4A, 12V/0.5A, 6.8V/1.5A, 10msec/div

Upper: 12V, 2V / div Lower: 5V, 1V / div

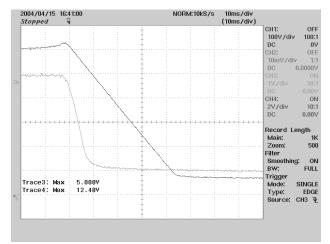


Figure 6 - 230 VAC, 5V/4A, 12V/0.5A, 6.8V/1.5A,

Upper: 12V, 2V / div Lower: 5V, 1V / div

10msec/div

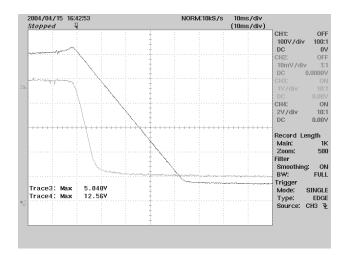


Figure 7 - 180VAC, 5V/4A, 12V/0.5A, 6.8V/1.5A, 10msec/div. Upper: 12V Output, 2V / div

Lower: 5V Output, 1V / div.

## 10.2 5V Transient Response

Transient response measurements were taken for the 5V output using a 1A-2.5A-1A current step, with the 12V output loaded to 0.5A, and the 6.8v output at 1.5A. The cathode terminal of the TL431 error amplifier was loaded to determine its voltage excursion under these transient conditions. As shown below, the cathode excursion of the TL431 does not approach saturation, under these load conditions.

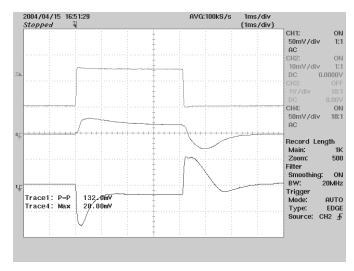


Figure 11 - 230VAC Input, 5V Load Step of 1A-2.5A-1A, 1msec/div. Upper: 5V Load, 1A/div. Middle: TL431 Drain Voltage, 50mV/div. Lower: 5V Output, 50mV/div

# 11 Conducted EMI

Tests were performed in open air with resistive load. The supply was mounted inside the chassis. The secondary return was connected to the chassis at the end of the load cable. The primary ground lead (when used) was connected to the chassis using the fast-on terminal provided at the chassis rear panel. The chassis was hard wired to the LISN ground. The margin at the second harmonic will be 2-3dB better using the TDK choke instead of the Panasonic choke.

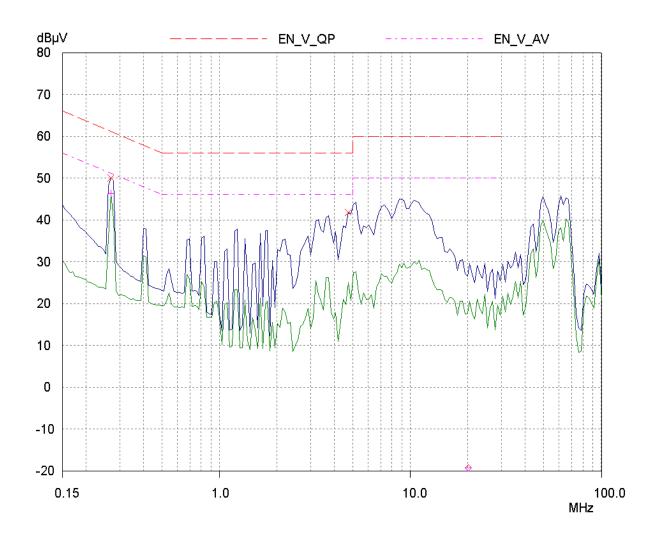
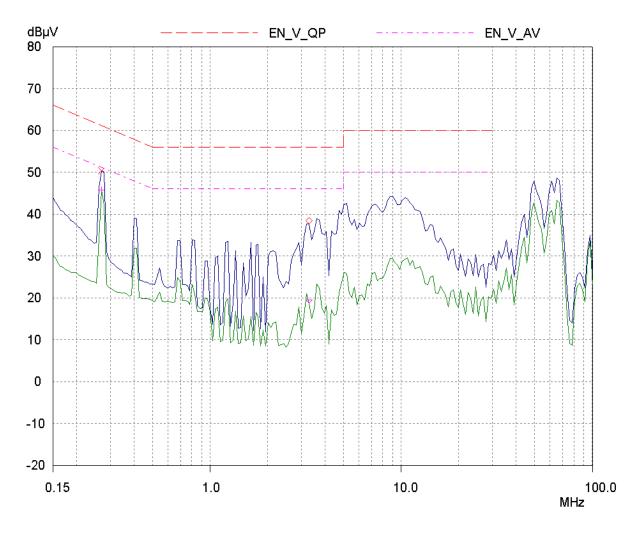


Figure 30 - Conducted EMI, Maximum Steady State Load, 230 VAC, 60 Hz, and EN55022 B Limits, ground wire connected to chassis.



**Figure 30 -** Conducted EMI, Maximum Steady State Load, 230 VAC, 60 Hz, and EN55022 B Limits, ground wire left open.

# **12 Revision History**

<b>Date</b>	<b>Author</b>	Revision	<b>Description &amp; changes</b> First Release	<b>Reviewed</b>
April 27, 2004	RH	1.0		VC

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